

	SURFACE VEHICLE INFORMATION REPORT	SAE	J2052 JAN2011
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		Superseding	J2052 DEC2005
Test Device Head Contact Duration Analysis			

A technically equivalent version of SAE J2052 is included in ISO Technical Report 12351.

RATIONALE

The committee reviewed this information report and determined that no substantial changes were needed. The reference section was reformatted and updated.

FOREWORD

A technique has been established for determining head impact contact duration called the "Force Difference Method." This technique allows calculation of Head Injury Criterion (HIC) only during head contact.

1. SCOPE

This methodology can be used for all calculations of HIC, with all test devices having an upper neck triaxial load cell mounted rigidly to the head, and head triaxial accelerometers.

1.1 Purpose

The purpose of this SAE Information Report is to describe a computer-adaptable technique for determining head engagement and disengagement times for use in the calculation of the HIC without reliance on contact switches or photography.

2. REFERENCES

2.1 Applicable Documents

The following publications form a part of this specification to the extent specified herein. Unless otherwise indicated, the latest issue of SAE publications shall apply.

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2.1.1 SAE Publication

Available from SAE International, 400 Commonwealth Drive, Warrendale, PA 15096-0001, Tel: 877-606-7323 (inside USA and Canada) or 724-776-4970 (outside USA), www.sae.org.

SAE J211-1 JUL 2007 Instrumentation for Impact Test

2.1.2 Federal Publication

Available from the Superintendent of Documents, U.S. Government Printing Office, Mail Stop: SSOP, Washington, DC 20402-9320.

49 CFR Part 572, Subpart E Occupant Crash Protection, revised as of April, 1997

2.1.3 ISO Publication

Available from American National Standards Institute, 25 West 43rd Street, New York, NY 10036-8002, Tel: 212-642-4900, www.ansi.org.

ISO Technical Report 12351 Determination of head contact and duration in impact tests—ISO/TC22/SC12/WG3N355

3. DEFINITIONS

3.1 HIC

The HIC is one of the "injury criteria" prescribed by S6 of the Federal Motor Vehicle Safety Standard (FMVSS) 208. It is the maximum value calculable from the head c.g. resultant acceleration-time profile in accordance with Equation 1:

$$\text{HIC} = \left[\frac{1}{(t_2 - t_1)} \int_{t_1}^{t_2} a \cdot dt \right]^{2.5} (t_2 - t_1) \quad (\text{Eq. 1})$$

where:

a is the resultant acceleration expressed as multiples of *G* (the acceleration of gravity), and *t*₁ and *t*₂ are any two points in time during the crash.

NOTE: Although a HIC window of 36 ms maximum was subsequently mandated by NHTSA, it is not utilized with this document.

3.2 Contact HIC

HIC values calculated only during the periods of each head contact.

3.3 *t*_e, *t*_d

The head engagement and disengagement times, *t*_e and *t*_d respectively, are determined by the method given in Section 5. These are the starting and ending times, i.e., the windows for the iterative HIC calculations for each head contact.

NOTE: The maximum contact HIC for each *t*_e, *t*_d interval will have associated with it times *t*₁, *t*₂ which may be equal to, or less than the *t*_e, *t*_d interval.

3.4 Accelerometers (a_x , a_y , a_z)

The triaxial accelerometer(s) in the head of the test device will be referred to as an accelerometer, omitting the triaxial classification as defined in SAE J211-1; $+a_x$ is forward, $+a_y$ is to the right, and $+a_z$ is downward. These orientations are shown in Figure 1.

3.5 Load Cell

The triaxial force load cell (attached rigidly to the base of the skull portion of the test device to which the neck is attached) will be referred to as a load cell, omitting the triaxial and upper neck classification. Load cells with additional outputs can also be used.

3.6 Head Mass (M)

The mass of the head including the masses of the head accelerometers and mounting brackets and the mass of the load cell above the gage plane.

NOTE: Caution should be exercised to minimize the effect of elements external to the neck, such as neck skins or wires, which might carry load or modify the head mass.

3.7 Inertial Head Forces (Ma_x , Ma_y , Ma_z)

The inertial head forces are calculated from the triaxial accelerometers which are inside the head of the test device. The accelerations are multiplied by the M of the test device to determine the inertial head forces. The directions of these inertial forces are the same as the directions of their corresponding acceleration vectors.

3.8 Neck Forces (F_x , F_y , F_z)

The neck forces are determined directly from the load cell, per 3.5, which reads the forces acting on the neck at the location of the load cell (the base of the skull in this case). F_x is longitudinal shear, F_y is lateral shear, and F_z is axial force. Forces (F_x , F_y , F_z) are applied to the neck in this paper (see Figure 1). A positive F_x output from the load cell means head rearward motion relative to neck; positive F_y output is head left motion relative to neck; and positive F_z output is tensile force or head upward motion relative to the neck. Conventions are per SAE J211-1.

3.9 Test Device

Any full, partial, or simulated anthropomorphic dummy equipped with head accelerometers and load cell per 3.4 and 3.5 is defined as the test device. For example, the 50th percentile male Hybrid III dummy specified in 49 CFR Part 572, Subpart E, can be used, as can any derivative of that dummy with proper instrumentation.

4. DATA ACQUISITION AND PROCESSING SYSTEM

The data acquisition and processing system must be capable of supplying transducer data per SAE J211-1 which recommends that both head acceleration and neck force utilize channel class 1000, and that any multiple recording devices are time-referenced per 4.4.2 of SAE J211-1.

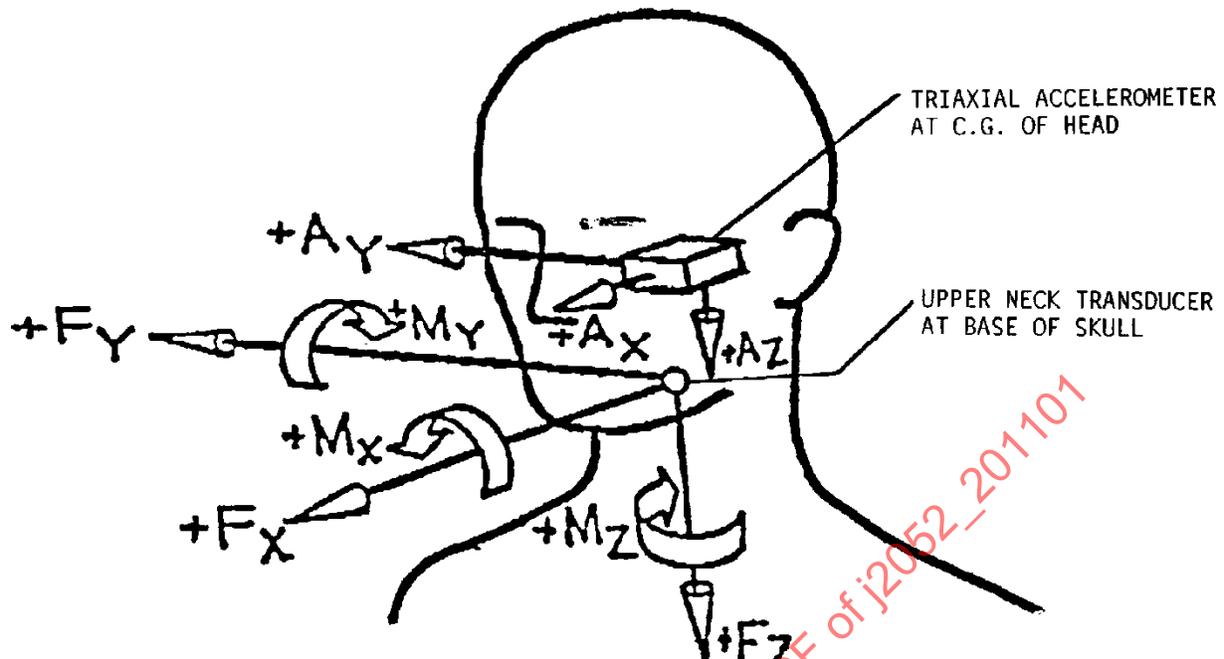


FIGURE 1 - HEAD CONTACT DURATION ANALYSIS - ACCELERATION AND FORCE

5. PROCEDURE FOR DETERMINING HEAD CONTACT DURATION (t_e , t_d)

The subject method uses Equation 2:

$$F = \sqrt{[(Ma_x - F_x)^2 + (Ma_y - F_y)^2 + (Ma_z - F_z)^2]} \quad (\text{Eq. 2})$$

The acceleration components (a_x , a_y , a_z) of the head are multiplied by the M to produce the components of inertial head force. Each neck force component (F_x , F_y , F_z) is subtracted from the corresponding calculated inertial head force component. The aforementioned subtractions produce three force-differences. The external resultant head force (F) is calculated by taking the root sum square of the force-differences, and is plotted as a function of time. This plot represents the resultant contact force acting on the head.

In order to establish consistent engagement (t_e) and disengagement (t_d) times for each contact, the following method is established: A contact is assumed to have occurred when the force level has reached 500 N. The t_e for this contact is obtained by tracing backwards in time from the 500 N point on the force versus time curve until 200 N is first reached. The t_d for this contact is determined by tracking forward in time until the curve crosses the 200 N force level.

A subsequent contact is assumed to have occurred when the force level again has reached 500 N after the first time t_d . The t_e and t_d for this second contact are determined in the same manner used for determining t_e and t_d in the previous contact. This process is repeated for each subsequent contact, and is illustrated in Figure 2.