



SURFACE VEHICLE STANDARD	J1792™-2	NOV2015
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Superseding J1792-2 APR2007		
Self-Propelled Sweepers - Air Flow Performance - Part 2: Suction/Blower Fan Performance		

RATIONALE

The document has been revised to update the referenced documents.

1. SCOPE

This SAE Standard establishes a test method and a definition for disclosing the performance of suction/blower fans when applied to self-propelled sweepers that solely use a pneumatic conveyance means for the collection and transfer of “sweepings” into a collection hopper.

1.1 Purpose

The purpose of the document describes a test practice for measuring the performance of suction/blower fans used in vacuum and regenerative air street sweepers described in SAE J2130-1. The measured performance considers the air volume movement versus the static depression developed by the fan across a spectrum of different operating conditions. The document also sets-out to propose a format for the presentation of the test results. The method in this document can be used to disclose or compare particular operating performance criteria under similar conditions.

2. REFERENCE

2.1 Applicable Documents

The following publications form a part of this specification to the extent specified herein. Unless otherwise indicated, the latest issue of SAE publications shall apply.

2.1.1 SAE Publication

Available from SAE International, 400 Commonwealth Drive, Warrendale, PA 15096-0001, Tel: 877-606-7323 (inside USA and Canada) or +1 724-776-4970 (outside USA), www.sae.org.

SAE J2130-1 Identification of Self-Propelled Sweepers and Cleaning Equipment Part 1 - Machines with a Gross Vehicle Mass Greater than 5000 kg

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3. DEFINITIONS

3.1 SWEEPER

A self-propelled vacuum or regenerative air street sweeper that is primarily designed to sweep material from highways, parking lots, airport complexes, industrial and construction sites, and during road maintenance work. The sweeper may use broom means to dislodge and direct material into a pneumatic collection mechanism that is the sole means to convey the swept material into a collection hopper.

3.2 SUCTION/BLOWER FAN

Centrifugal fan means for developing the required air movement/pressure employed in the sweeper's pneumatic conveyance mechanism.

4. TECHNICAL REQUIREMENTS

4.1 Recommended Apparatus

Manometer - Pitot tube - Tachometer - Thermometer - Barometer - Hygrometer (see note in 4.4) - test duct.

4.2 Method

The machine shall be set up in its optimum running condition according to the recommendations given in its operator's instruction manual. The hopper filter meshes shall be clean or may be removed. All air ducts shall be clean and free from debris. Wander hoses, drain off hoses, etc., shall be sealed and blanked-off. The suction pick-up nozzle and flexible conduit shall be removed and substituted with a test duct, a suggested test duct and blanking mechanism is shown in Figures 1 and 2.

It is important to monitor the engine and suction/blower fan speed during the test in order that it always runs at a constant speed. Ideally a digital tachometer connected to the engine or actual fan itself shall be used. An instrument giving a precise speed to the nearest revolution per minute is preferred. The running speed of the fan shall be set to a predetermined level for the test and recorded in the results.

The manometer and pitot tube used in the tests measurements shall be checked to ensure the pitot tube is clean and that the manometer and connecting tubes are perfectly sealed with no leakage to atmosphere. If an electronic manometer is used, first ensure that it is calibrated to zero pressure in the inert state. Two small holes shall be provided at 90 degrees to each other in the test duct large enough to permit the insertion of the pitot tube. These holes shall be located mid-way along the test duct to ensure minimum turbulence within the air-stream.

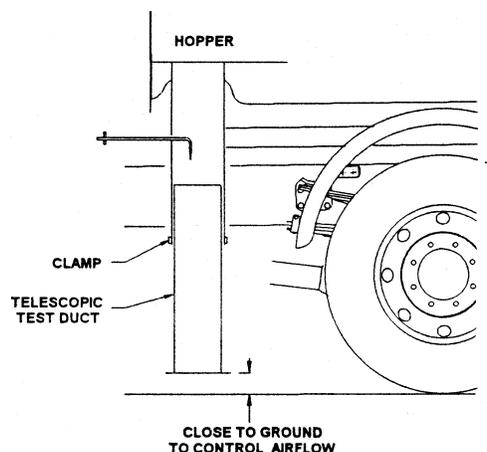


Figure 1 - Suggested test duct

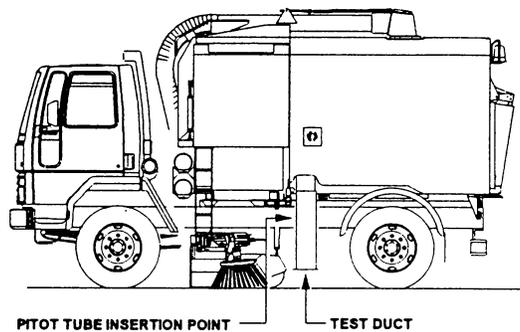


Figure 2 - Test duct set-up

The ambient temperature shall be recorded before and after the tests in order that results may be corrected to a standard of 20 °C (68 °F). Barometric pressure shall also be recorded so that corrections may be made to a standard of 760 mm Hg or 1013 mb (norm at sea level). Corrections for temperature and barometric pressure will ensure that quantifiable comparative data is available to a common standard.

The pitot tube shall have a calibrated scale marked with six positions - refer to Figure 3, according to the internal size of the test duct being used. The pitot tube is then inserted into the test duct with the probe pointing into the air-stream within 5 degrees of the duct axis. Velocity head pressure readings are then read from the manometer at each of the twelve positions, six for each pass (or hole). Readings taken are the total velocity head (in millimeters water gauge), shown on the manometer. From these twelve results, the average velocity head and hence air flow velocity and volume shall be calculated based on the duct's cross-sectional area. Prior to and after the test pass, the static pressure within the 'eye' of the fan shall be recorded.

The test process shall be repeated a number of times, each time with the test duct inlet progressively blanked by moving it nearer to the ground to reduce and inhibit air flow into it. Each time the negative pressure within the 'eye' of the fan shall be recorded before and after each test pass.

Care must be taken while measuring the velocity head readings to ensure that the pitot tube is held parallel to the walls of the duct. This may be checked by reference to the direction pointer on the tail of the pitot tube (this points in the same direction to the pitot probe).

The static depression shall also be measured within the duct in order to make a correction for air density by connecting the side holes in the pitot tube only to the manometer, leaving the other side open to atmosphere. The total deflection (in millimeters water gauge) shall again then be read from the manometer. Note that in this application the reading will be a negative pressure and shall be used as such when applying the formulae for correction of duct depression.

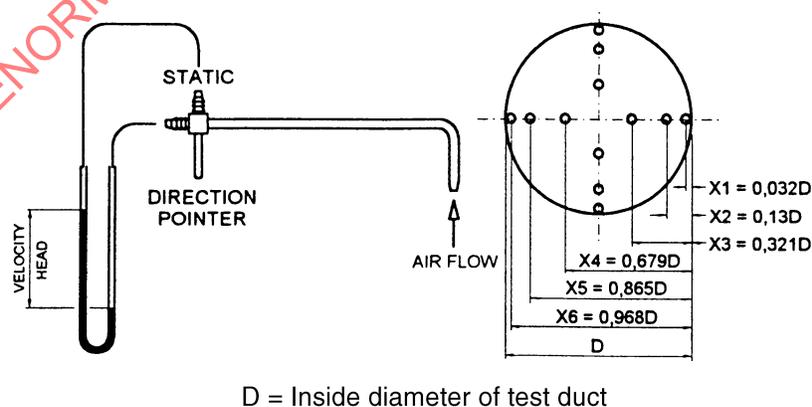


Figure 3 - Pitot tube positions for a six-point pass in circular ducts

4.3 Results Tabulation

The test results can be typically recorded in the format shown in Figure 4, the corrected values would be derived by the calculation methods given in 4.4.

Test No.	Fan Speed (rpm)	Uncorrected Pitot Velocity Head Readings (mm H ₂ O)												Corrected Values (20 °C/1013mb)				
		First Pass (first hole)						Second Pass (second hole)						Fan Inlet Pressure (mm H ₂ O)	Average Vel. Head (mm H ₂ O)	Test Duct Air Vel. (m/sec)	Test Duct Air Vol. (m ³ /sec)	Fan Inlet Pressure (mm H ₂ O)
		X ₁	X ₂	X ₃	X ₄	X ₅	X ₆	X ₇	X ₈	X ₉	X ₁₀	X ₁₁	X ₁₂					
1																		
2																		
3																		
4																		
5																		
6																		
7																		
8																		
9																		
10																		
11																		
12																		

Figure 4 - RESULTS CALCULATION

4.4 Calculations

See Equations 1 to 6.

$$\text{Average velocity head (in mm H}_2\text{O)} = \sqrt{\frac{\sum x^2}{n}} \quad (\text{Eq. 1})$$

$$\text{Correction for temperature (correct to 20 °C)} = \frac{\text{ambient temp. (°C)} + 273}{293} \quad (\text{Eq. 2})$$

$$\text{Correction for barometric pressure (correct to 1013 mb - sea level)} = \frac{1013}{\text{barometric pressure (mb)}} \quad (\text{Eq. 3})$$

$$\text{Correction for duct depression (correct to std. density)} = \frac{10363}{10363 + \text{static depression (mm H}_2\text{O) in test duct}} \quad (\text{Eq. 4})$$

$$\text{Air velocity in duct (m/s)} = 4.032 \times \sqrt{(1) \times (2) \times (3) \times (4)} \quad (\text{multiply by 196.8 to convert m/s to ft/min}) \quad (\text{Eq. 5})$$

$$\text{Volume of conveying air (m}^3\text{/s)} = (5) \times \text{duct cross section (m}^2\text{)} \quad (\text{multiply by 2118.9 to convert m}^3\text{/s to cfm}) \quad (\text{Eq. 6})$$

NOTE: Corrections may also be made for relative humidity conditions. Usually the results shall be specified at 50% humidity. High humidity will result in lower air volume recordings due to lower density. The effect is often small and can therefore be ignored.

4.5 Typical Test Summary Format

The calculated results for corrected air flow volume versus the negative air pressure (static pressure) within the fan eye may be shown graphically and presented together with the operational criteria in the format in Figure 5:

**SAE 1792 PART 2
SELF-PROPELLED SWEEPERS
SUCTION/BLOWER FAN PERFORMANCE**

Testing Agency:

Machine Make.....
 Type.....
 Serial No.....

Blower Fan: Designation/Size:.....
 Rotational Speed:.....

Ambient Conditions: Temperature:.....
 Barometric Pressure:.....
 Humidity:

Static Pressure (mb) ↑

↓ Air Volume (m³/sec) →

NOTE— Performance corrected to 20 °C, 1013 mb and 50% relative humidity

Remarks:.....
.....
.....

Test Ref. No:.....

Test Engineer:.....

Date:

Figure 5 - Typical test summary format