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**AEROSPACE  
 RECOMMENDED  
 PRACTICE**

**SAE** ARP958

REV.  
**C**

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**ELECTROMAGNETIC INTERFERENCE MEASUREMENT ANTENNAS;  
 STANDARD CALIBRATION METHOD**

**FOREWORD**

Revision C contains a correction to Appendix D, first paragraph, which should read "Appendix C contains....." not "Appendix D".

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**SAE ARP958 Revision C****1. SCOPE:****1.1 Purpose:**

This SAE Aerospace Recommended Practice (ARP) outlines a standard method for the checkout and calibration of electromagnetic interference measurement antennas. Its primary application is for use when measuring a source 1 m from the antenna in a shield room versus a source at a greater distance (far field). This is the typical distance used in performing military EMC testing. Thus, this is a method of calibration. Shield room characteristics are not considered. It does not address an unknown distributed source. Yet it is close to reality since it is based on another antenna that represents a distributed source. This document presents a technique to determine antenna factors for antennas used primarily in performing measurements in accordance with 2.1 and 2.2. The purpose of Revision B is to include the calibration of other antennas, such as small loop antennas that are also specified for use in these same references.

**1.2 Applicable Antennas:**

The intent of Revisions A and B is to make this document applicable to passive and active antennas that may be used to measure signals from a source 1 m distant. Typical antennas being considered are the following:

- a. Biconical
- b. Resonant dipole
- c. Log periodic dipole
- d. Log spiral (200 MHz - 1 GHz)
- e. Log spiral (1 GHz - 10 GHz)
- f. Double ridged horn
- g. Log periodic
- h. Standard gain horns
- i. Loop antennas
- j. Vertical monopole
- k. "RE01/RE101" loop
- l. "RS01/RS101" loop

Most present day "104 cm" (41 in) rod antennas are of the active type and not calibratable per the previous issue of ARP958. The theoretical behavior of rod antennas is well understood. Therefore, the calibration really involves verifying the gain of the electronics in the antenna base. These antennas are calibrated by the use of a signal substitution source as defined in Revision B.

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### 1.3 General Background and Limitations:

This document originally was limited to determining antenna factors for conical logarithmic spiral antennas. It has been expanded to cover other antennas as indicated in 1.2. Antenna factors can be determined and calculated for the far field condition independent of ground reflections. The method, described in this document, of moving from the far field to a 1 m distance results in changes in antenna factors of a few decibels. The primary conditions which influence the antenna factors are the antenna separation, the height of the antenna above the ground plane, the orientation of the antenna relative to the ground plane, and the conductivity of the ground plane.

### 2. REFERENCES:

- 2.1 MIL-STD-461 Requirements for The Control of Electromagnetic Interference Emissions And Susceptibility
- 2.2 MIL-STD-462 Measurement Of Electromagnetic Interference Characteristics
- 2.3 Microwave Antenna Theory and Design by Silver, Vol. 12, Radiation Laboratory Series, McGraw - Hill, 1949, pp. 582-585
- 2.4 Antennas by Kraus, McGraw - Hill, 1950, pp. 455-457
- 2.5 Standard Site Method For Determining Antenna Factors, IEEE EMC Transactions, Vol. EMC-24, No. 3, August 1982, pp 316-322
- 2.6 ANSI C63.5 American National Standard for Electromagnetic Compatibility -- Radiated Emission Measurements in Electromagnetic Interference (EMI) Control -- Calibration of Antennas
- 2.7 IEEE Std 291 Standard Methods For Measuring Electromagnetic Field Strength of Sinusoidal Continuous Waves, 30 Hz to 30 GHz
- 2.8 IEEE Std 149 IEEE Standard Test Procedures For Antennas
- 2.9 SAE J551/5 Performance Levels and Methods of Measurement of Magnetic and Electric Field Strength from Electric Vehicles, Broadband, 9 kHz to 30 Mhz

### 3. RATIONALE FOR APPROACH:

#### 3.1 Antenna Factor:

For an antenna to be useful in measuring EMI, an antenna factor (AF) must be specified which permits converting voltage at the input of a receiver (V) to field strength (E) in volts per meter (V/m) or into units suitable for comparison with radiated emission limits (dB $\mu$ V/m) of reference 2.1. Thus,

$$E = AF \times V \quad (\text{Eq.1})$$

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## 3.1 (Continued):

where:

$$E = V/m$$

$$V = \text{volts}$$

where:

AF is the antenna factor based upon power gain of the antenna (it is derived from the square root of the power density ( $W/m^2$ )). Converting to dB:

$$E = 20 \log_{10} (AF \times V) \quad (\text{Eq.2})$$

where:

$$E = \text{dB}\mu\text{V}/\text{m}$$

$$V = \mu\text{V}$$

AF is the antenna factor based upon an antenna calibration similar to gain, henceforth referred to as 1 m gain, but performed under conditions characteristic of the actual use (1 m from the source) of the antenna for component-level EMC specification compliance testing. Numeric antenna gain (G) and wavelength ( $\lambda$ ) (in meters) in a 50  $\Omega$  system express the antenna factor as follows:

$$AF = \frac{9.73}{\lambda} \cdot \frac{1}{\sqrt{G}} = \frac{9.73}{\lambda\sqrt{G}} \quad (\text{Eq.3})$$

Antenna gain is the ratio of the radiated power density in a certain direction to the average radiated power density.

The average radiated power density is the isotropic radiation intercepted by a surface area of a sphere of unit radius (see 2.3 and 2.4).

## 3.2 General Antenna Gain:

Antenna gain may be obtained by antenna pattern measurements which satisfy the following expression of antenna gain in integral form:

$$G = \frac{\Phi(\theta, \phi)}{\frac{1}{4\pi} \int_0^\pi \int_0^{2\pi} \Phi(\theta, \phi) \, d\phi \, \sin \theta \, d\theta} \quad (\text{Eq.4})$$

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## 3.2 (Continued):

where:

$\theta, \phi$  = spherical coordinates in radians

$\Phi$  = power radiated per unit solid angle in a given direction

## 3.3 Using Two Identical Antennas:

The term "1 m gain" has been selected in lieu of "apparent gain," since "1 m" defines the conditions under which "apparent" applies. The 1 m gain determination can be calculated by the antenna gain equation. This method uses two identical antennas aligned on axis with polarization matched. The relationship for power received is:

$$P_R = \frac{P_T G_T}{4\pi r^2} \cdot \frac{\lambda^2}{4\pi} \cdot G_R \quad (\text{Eq.5})$$

where:

$G_T$  and  $G_R$  = numeric power gain of the transmitting and receiving antennas respectively

$P_R$  = power received in watts

$P_T$  = power transmitted in watts

$r$  = distance between antennas in meters

$\lambda$  = wavelength in meters

$$\text{If } G_T = G_R, \text{ then } G^2 = \left( \frac{4\pi r}{\lambda} \right)^2 \frac{P_R}{P_T} \quad (\text{Eq.6})$$

If both receiving and transmitting systems are matched ( $50 \Omega$ ), voltage measurements may be made in lieu of power measurements so that:

$$G = \frac{4\pi r}{\lambda} \cdot \frac{V_R}{V_T} \quad (\text{Eq.7})$$

where:

$V_R$  = voltage across the receive antenna terminals

$V_T$  = voltage across the transmit antenna terminals

(It should be noted that  $G$  is the numeric power gain even though it is determined by two voltage measurements since these are used to form a ratio which is dimensionless.)

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## 3.4 Gain and 1 m Gain:

- 3.4.1 **Need for Gain and 1 m Gain:** Because the antenna may be used to make field strength measurements and specification compliance measurements, the gain, as well as the 1 m gain, is often needed. Accordingly, gain measurements are discussed in this document and a recommended measurement method is presented as an appendix to this document. However, the procedure specified in the document is only for determining the 1 m gain.
- 3.4.2 **Distance for Gain Measurements:** The gain is measured using the three identical antenna technique (see Appendix C). The distance between the antennas is 3 m. (See Figure 2 of this document.)
- 3.4.3 **Distance for 1 m Gain Measurements:** Measure the 1 m gain using the two identical antenna technique at a 1 m distance between the antennas. This is equal to that required between the antenna and the test sample for EMC specification compliance testing of components and subsystems. Some antennas have an "electrical" center that is used as the antenna position for theoretical calculations and measurements. Antennas, such as the log spiral, where the electrical center is not defined or is a function of frequency use the "nearest" point approach. (See Figure 2 of this document.)
- 3.4.4 **Necessary Number of Measurements:** Measurements should be made at a sufficient number of frequencies to describe their 1 m gain within the specified operating bandwidth of the antenna. A 1 m gain should be measured at frequencies as specified in 4.3(g). Such additional measurement frequencies should be chosen to precisely identify and define any anomalies in the 1 m gain characteristics.

## 3.5 Determining Antenna Factors:

- 3.5.1 **Antenna Factor For Gain (AF<sub>1</sub>):** The AF for gain in the far field (referred to as gain and defined as AF<sub>1</sub>) is calculated from Equation 3 where G was determined per 3.4.2.
- 3.5.2 **Antenna Factor for 1 m Gain (AF<sub>2</sub>):** The antenna factor for 1 m measurements (defined as AF<sub>2</sub>) is calculated from Equation 3 where G was determined per 3.4.3.
- 3.5.3 **Calculation:** The antenna factors AF<sub>1</sub> and AF<sub>2</sub> are calculated by the same method and by Equation 3 by using either the value G<sub>1</sub> or G<sub>2</sub> in the equation. To simplify the calculation it may be performed in logarithmic form. For this reason, Figure 1 was plotted which is a plot of  $20 \log_{10} 9.73/\lambda$  as a function of frequency.

When the 1 m gain, G<sub>2</sub>, is a numeric, AF<sub>2</sub> in decibels may be found by the following expression:

$$AF \text{ (db)} = 20 \log_{10} \frac{9.73}{\lambda} - 10 \log_{10} G \quad (\text{Eq.8})$$

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## 3.5.3 (Continued):

where:

$\lambda$  = meters

When the 1 m gain,  $G_2$ , is in decibels,  $AF_2$  may be found by:

$$AF \text{ (db)} = 20 \log_{10} \frac{9.73}{\lambda} - G$$

For example, at 200 MHz the 1 m gain was 10 dB. What is the antenna factor  $AF_2$ ?

From Figure 1,  $20 \log (9.73/\lambda) = 16$

Therefore,  $AF_2 = 16 - 10 = 6$  dB.

## 3.6 Use of Antenna Factor:

- 3.6.1 Correction of Signal Levels: The appropriate antenna factor is added to the voltage at the receiver input which is indicated in decibels above 1  $\mu$ V, along with cable-loss factors to obtain field intensity in decibels above 1  $\mu$ V/m.

$$E \text{ (dB}\mu\text{V/m)} = V \text{ (dB}\mu\text{V)} + AF \text{ (dB)} + \text{Cable Loss (dB)} \quad (\text{Eq.9})$$

- 3.6.2 Polarization Considerations: Section 4 outlines the procedure for obtaining gain of the antenna utilizing the two identical antenna technique. If the conical logarithmic spiral antenna is used, the gain so determined is that for a circularly polarized wave (see 3.3). When making field intensity measurements with linearly polarized received waves, the gain used to calculate the antenna correction factor,  $AF_1$ , must be decreased by 3 dB (which means the antenna factor goes up by 3 dB. See Appendix B). The 1 m antenna factor,  $AF_2$ , should also be based on the gain for linearly polarized signals.

## 4. PROCEDURE FOR TWO IDENTICAL ANTENNA 1 m GAIN MEASUREMENTS:

## 4.1 Apparatus:

- a. Signal generators with 50  $\Omega$  output impedance capable of generating test levels over the frequency range specified for the antenna type
- b. Two 6 dB, 50  $\Omega$  attenuators
- c. Calibrated receiver (or spectrum analyzer) tuning over the frequency range specified for the antenna type. The receiver input impedance should be 50  $\Omega$  and a VSWR  $\leq 1.25$ . An isolating attenuator can be used at the receiver input to achieve 1.25 VSWR.
- d. Coaxial cables of 50  $\Omega$  characteristic impedance and appropriate connectors for mating with antennas, 6 dB attenuator, signal generators, and receivers

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## 4.1 (Continued):

- e. Adapter for connecting two coaxial cables

## 4.2 Setup:

The basic setup is shown in Figure 3. The area in which the setup is situated should be clear of obstructions to achieve a free-space environment. A chamber permitting the 1 m spacing between antennas is acceptable if the chamber is anechoic, except for the floor, at all measurement frequencies. It also needs to maintain a ground plane to simulate open field sites. The antenna height above the ground influences the results and should be standard. A 3 m height for the center of the antenna is defined.

## 4.3 Measurement:

At each measurement frequency using the receiver as a transfer device the following operations shall be performed.

- a. Adjust signal generator output to obtain a receiver indication. Be sure the receiver is tuned for maximum response to the signal.
- b. Make fine adjustment of the alignment of the antennas for maximum indication and record the signal generator setting. ( $V_T$ )
- c. Disconnect the receiver and signal generator cables from their respective antennas and connect the signal generator and the receiver to each other using the same cables with the addition of a 50  $\Omega$ , calibrated coupling adapter.
- d. Reduce the signal generator output to obtain the same receiver output meter indication as obtained in step (b). Record the signal generator setting. ( $V_R$ )
- e. Solve for gain with 1 m spacing between antennas utilizing Equation 7 in which  $V_R$  and  $V_T$  are equivalent to the signal generator readings recorded in steps (d) and (b), respectively.
- f. Compute the antenna factor using the equation of 3.5.3 (Equation 8) or Equation A7 of Appendix A.
- g. Measurements should be taken as a minimum at frequency increments as follows:
  - (1) 20 kHz - 200 kHz: 10 kHz
  - (2) 200 kHz - 2 MHz: 100 kHz
  - (3) 2 MHz - 20 MHz: 1 MHz
  - (4) 20 MHz - 200 MHz: 10 MHz
  - (5) 200 MHz - 1.0 GHz: 100 MHz
  - (6) 1.0 GHz - 40 GHz: 1.0 GHz

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## 5. THE ROD ANTENNA:

## 5.1 Rod Antenna Theory:

The most significant characteristic of a rod antenna is its effective height ( $h_e$ ). This is usually given in meters. With the rod antenna vertically oriented, it is perpendicular to a ground plane of infinite length ( $h_e = \ell/2$ ). ( $\ell$  = physical length of antenna.) With the antenna oriented vertically,  $h_e$  expresses the relationship between the voltage induced in the antenna and the vertical components of the incident field  $E$ . The effective height expression of  $\ell/2$  applies exactly for most practical situations, within the limits of experimental measurements. Thus, the rod is mounted above a counterpoise that simulates this ground plane.

The factor 2 appears in  $h_e = \ell/2$  and exists because of the effect of the proximity of a perfect ground and may be explained by the theory of images. The vertical rod and ground behave electrically as though a mirror image of the actual rod were located below the surface of the ground, and the ground removed. The antenna as a transmitter develops a field strength ( $E$ ) having a peak value double that of the isolated rod, for the same voltage input to the antenna. By reciprocity, the incident field on the antenna as a receiver induces a voltage  $E_a$  equal to one-half that for the isolated rod. From the definition  $h_e$  for effective height, the value for the rod in the presence of ground is, therefore,  $\ell/2$ . Thus, for example, a rod 1 m in length has an effective height in the presence of ground of 0.5 m.

The value of  $h_e = \ell/2$  for effective height is valid so long as  $\ell < \lambda/8$  where  $\lambda$  is the wavelength. Thus, for 1 m physical length the frequency is 37.5 MHz. Therefore, the 1 m rod antenna is usually calibrated to 30 MHz. The rod has an internal impedance ( $Z_a$ ).

$$Z_a = [R_a + 1/j\omega C_a] \quad (\text{Eq.10})$$

where:

$R_a$  = radiation resistance

$C_a$  = electrostatic capacitance of the rod and ground plane

Typical values of capacitance are 10 pF for a 1 m rod. Thus, for example, the maximum frequency for a 1 m rod (37.5 MHz) the capacitive reactance is 425  $\Omega$ , and it increases with decreasing frequency. Since the impedance of the rod antenna is quite high, most rod antennas have a coupling network or an amplifier to match the high impedance to the 50  $\Omega$  input impedance of the EMI meter. This coupling network or amplifier requires calibration.

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## 5.2 Rod Antenna Calibration:

The antenna factor for the rod antenna shall be determined by measuring the signal transfer characteristics of the matching device and assuming that the antenna is a short monopole with an infinite ground plane. The Thevenin equivalent of the rod element becomes an ideal voltage source equal to the electric field strength multiplied by the 0.5 m effective height of the antenna in series with a capacitor (typically 10 pF) representing the rod impedance. Figure 4 presents the general test setup and procedure for determining the antenna factor. Since some antenna assemblies include items such as the 10 pF capacitor or bandswitching mechanisms, details on the implementation of this technique for a particular antenna should be obtained from the manufacturer. Additional details can be found in reference 2.9.

## 6. LOOP ANTENNAS:

## 6.1 Operating Theory:

This test method is not meant to experimentally determine the magnetic fields. In most cases, for a controlled situation like this, they can be more accurately calculated than measured. This method is to set up a standard by which it can be determined that the antennas are functioning correctly. Thus, a failure such as a cold solder joint, broken wire, etc. can be detected.

## 6.1.1 Calculation for RE01/RE101 Loop:

## 6.1.1.1 The RS01 loop generates a field at 12 cm for 1 A of current as follows:

$$\begin{aligned}\beta &= \mu H = \mu I N R^2 / 2 (R^2 + Z^2)^{3/2} \\ &= 4\pi \times 10^{-7} \times [1 \times 10 \times (.06)^2] / 2[(.06)^2 + (.12)^2]^{3/2} \\ &= 9.366 \times 10^{-6} \text{ Tesla} = 139.4 \text{ dBpT}\end{aligned}$$

The RE01/RE101 loop reading of this field at 300 Hz is:

$$\begin{aligned}V &= 2\pi f N A \beta \\ V &= 2\pi \times 300 \times 36 \times \pi (6.65 \times 10^{-2})^2 \times 9.366 \times 10^{-6} \\ V &= 8.83 \times 10^{-3} \text{ V} = 78.9 \text{ dB}\mu\text{V}\end{aligned}$$

At 12 cm the RS01 field is 139.4 dBpT. The RE01 loop reads 78.9 dB $\mu$ V. The difference is the factor that needs to be added to the RE01 loop reading to indicate the correct dBpT reading.

i.e., 139.4 - 78.9 - 60.5 dB = antenna factor for (unloaded) RE01 loop

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6.1.1.2 The RS101 loop (with 20 turns) generates a field at 12 cm as follows:

$$\begin{aligned}\beta &= \mu H = \mu I N R^2 / 2 (R^2 + s Z^2)^{3/2} \\ &= 4\pi \times 10^{-7} \times [1 \times 20 \times (.06)^2] / 2[(.06)^2 + (.12)^2]^{3/2} \\ &= 18.332 \times 10^{-6} \text{ Tesla} = 145.4 \text{ dBpT}\end{aligned}$$

The field generated by the RS101 loop is higher than for the RS01 loop, and the reading by the RE01/101 loop increases accordingly to 84.9 dB $\mu$ V. Therefore, 145.4 - 84.9 = 60.5 dB = antenna factor for (unloaded) RE01 loop.

6.1.2 Calculation for 4 cm Calibration Loop: The 4 cm loop is used to measure the level generated by the RS101 loop.

The RS101 loop generates a field at 5 cm as follows:

$$\begin{aligned}\beta &= \mu H = \mu I N R^2 / 2 (R^2 + Z^2)^{3/2} \\ &= 4\pi \times 10^{-7} \times [1 \times 20 \times (.06)^2] / 2[(.06)^2 + (.05)^2]^{3/2} \\ &= 9.4955 \times 10^{-5} \text{ Tesla} = 9.4955 \times 10^7 \text{ pT} = 159.6 \text{ dBpT}\end{aligned}$$

The 4 cm loop reading of this field at 300 Hz is:

$$\begin{aligned}V &= 2\pi f N A \beta \\ V &= 2\pi \times 300 \times 51 \times \pi (2 \times 10^{-2})^2 \times 9.4955 \times 10^{-5} \\ V &= 1.1471 \times 10^{-2} \text{ V} = 81.2 \text{ dB}\mu\text{V}\end{aligned}$$

At 5 cm the RS01 field is 159.6 dBpT. The 4 cm loop reads 81.2 dB $\mu$ V. The difference is the factor that needs to be added to the 4 cm loop reading to indicate the correct dBpT reading.

i.e., 159.6 - 81.2 = 78.4 dB = antenna factor for (unloaded) 4 cm loop

6.1.3 Loading Effect on the Loops: The calculations of 6.1.1 and 6.1.2 (for simplicity) are for the condition in which the loop is open circuited or sees a high impedance, such as 100 k $\Omega$ . When a 50  $\Omega$  receiver is used, the loading of the loop must be considered. Tables 1 and 2 have been developed using the 50  $\Omega$  load. The equation in general is:

$$V = 2\pi f N A \beta / [(1 + R_w/R_L)^2 + (2\pi f L_w/R_L)^2]^{1/2} \quad (\text{Eq.11})$$

For the RE01/RE101 loop

$$\begin{aligned}V &= 2\pi 36\pi (6.65 \times 10^{-2})^2 \times 9.366 \times 10^{-6} f / \\ &\quad [(1 + 10/50)^2 + (2\pi f 340 \times 10^{-6} / 50)^2]^{1.2} \\ @ 300 \text{ Hz: } V &= 77.3 \text{ dB} \\ \text{and the antenna factor is } &139.4 - 77.3 = 62.1 \text{ dB}\end{aligned}$$

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TABLE 1 - Antenna Factor<sup>1</sup> for RE01/RE101 Loop

Frequency (Hz)	Reading ( $\pm 2$ dB tolerance)
30	82.1
60	76.0
100	71.6
300	62.1
600	56.0
1 000	51.6
3 000	42.1
6 000	36.2
10 000	32.1
20 000	27.4
30 000	25.4
50 000	23.8
100 000	23.0

<sup>1</sup> To be added to loop reading in dB $\mu$ V to yield magnetic field level in dBpT. Factors are for the loops when loaded by a 50  $\Omega$  system.

TABLE 2 - Antenna Factor<sup>1</sup> for 4 cm Calibrating Loop

Frequency (Hz)	Reading ( $\pm 2$ dB tolerance)
30	99.1
60	93.1
100	88.6
300	79.1
600	73.1
1 000	68.6
3 000	59.1
6 000	53.1
10 000	48.6
20 000	42.6
30 000	39.1
50 000	34.6
100 000	28.6

<sup>1</sup> To be added to loop reading in dB $\mu$ V to yield magnetic field level in dBpT. Factors are for the loops when loaded by a 50  $\Omega$  system.

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## 6.1.3 (Continued):

For the 4 cm calibrating loop

$$V = 2\pi 51\pi (2 \times 10^{-2})^2 \times 9.496 \times 10^{-5} f / [(1 + 4/50)^2 + (2\pi f 2 \times 10^{-6} / 50)^2]^{1/2}$$

@ 300 Hz:  $V = 80.5$  dB

and the antenna factor is  $159.6 - 80.5 = 79.1$  dB

## 6.2 Calibration:

## 6.2.1 Test Equipment Specification:

Equipment and critical specifications

Calibrator/Oscillator (1)

parameter: AC flatness

ranges: 30 Hz to 50 kHz

resolution: .01%

acceptable uncertainty:  $\pm 0.4\%$

Meter (2)

parameter: rms voltage/dBm

range: dBm, 30 Hz to 50 kHz

resolution: NA

uncertainty of standard:  $\pm 5\%$  of full scale

acceptable uncertainty:  $\pm 0.5$  dB

Meter (3)

parameter: rms voltage

range: 1 V, 30 Hz to 50 kHz

resolution: NA

uncertainty of standard:  $\pm 5\%$  of full scale

acceptable uncertainty:  $\pm 0.5$  dB

Audio Amplifier (4)

Load:  $50 \Omega$  (5)

Precision Resistor:  $1 \Omega \pm 1\%$  (6)

The RS01/RS101 and RE01/RE101 loop antennas are calibrated at a distance of 12 cm as a pair. Both transmit and receive loop antennas must have structures on or attached to them to allow them to be placed against each other and still have the required 12 cm loop separation.

The dB $\mu$ V calculations obtained from the receive loop antenna shall be subtracted from 139.4 dBpT (pico Tesla), which was calculated for the 12 cm distance and is the constant used to determine the antenna factor.

The loop antenna shall be considered calibrated when the levels have been compared to the values of Table 1 and found to be within  $\pm 2$  dB of those values.

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## 6.2.1 (Continued):

If the transmit loop has a series resistor on the input (approximately 10  $\Omega$ ), measure its value and include this information on the data sheet. Bypass the resistor for this calibration.

6.2.2 RS101 (4 cm) Calibration Loop: The 4 cm loop antenna is mounted at 5 cm from the RS101 loop. The dB $\mu$ V calculations obtained from the receive (4 cm) loop antenna shall be subtracted from 159.6 dBpT, which was calculated for the 5 cm distance and is the constant used to determine the antenna factor.

The loop antennas shall be considered calibrated when the levels have been compared to the values of Table 2 and found to be within  $\pm 2$  dB of those values.

6.2.3 Procedure: See Figure 5 for the test arrangement:

- a. Using the meter (3), verify the value of the 1  $\Omega$  precision resistor. (6)
- b. Set up the equipment as shown in Figure 5.
- c. Using meter (3), establish a 1 V rms, 30 Hz signal across the 1  $\Omega$  series resistor.
- d. Record the level measured by the meter (2)
- e. Calculate the antenna factor.

Example if the reading is in dBm

meter (2) reading	-30 dBm
$107 + (-30) =$	77 dB $\mu$ V
$139.4$ (from 6.1) - 77 dB $\mu$ V =	62.4 antenna factor

Example if the reading is in mV

meter (2) reading	7.3 mV
$20 \log 7.3 \text{ mV}/1 \mu\text{V} =$	77.3 dB $\mu$ V
$139.4 - 77.3 =$	62.1 antenna factor

- f. The results should be within the limits as shown in Table 1.
- g. Repeat steps c through f for the remaining frequencies in Table 1.
- h. If the calibration fails, replace the receive antenna with another and repeat the procedure.
- i. If the calibration fails again, the transmit loop is at fault. Replace the defective loop and repeat the calibration procedure.

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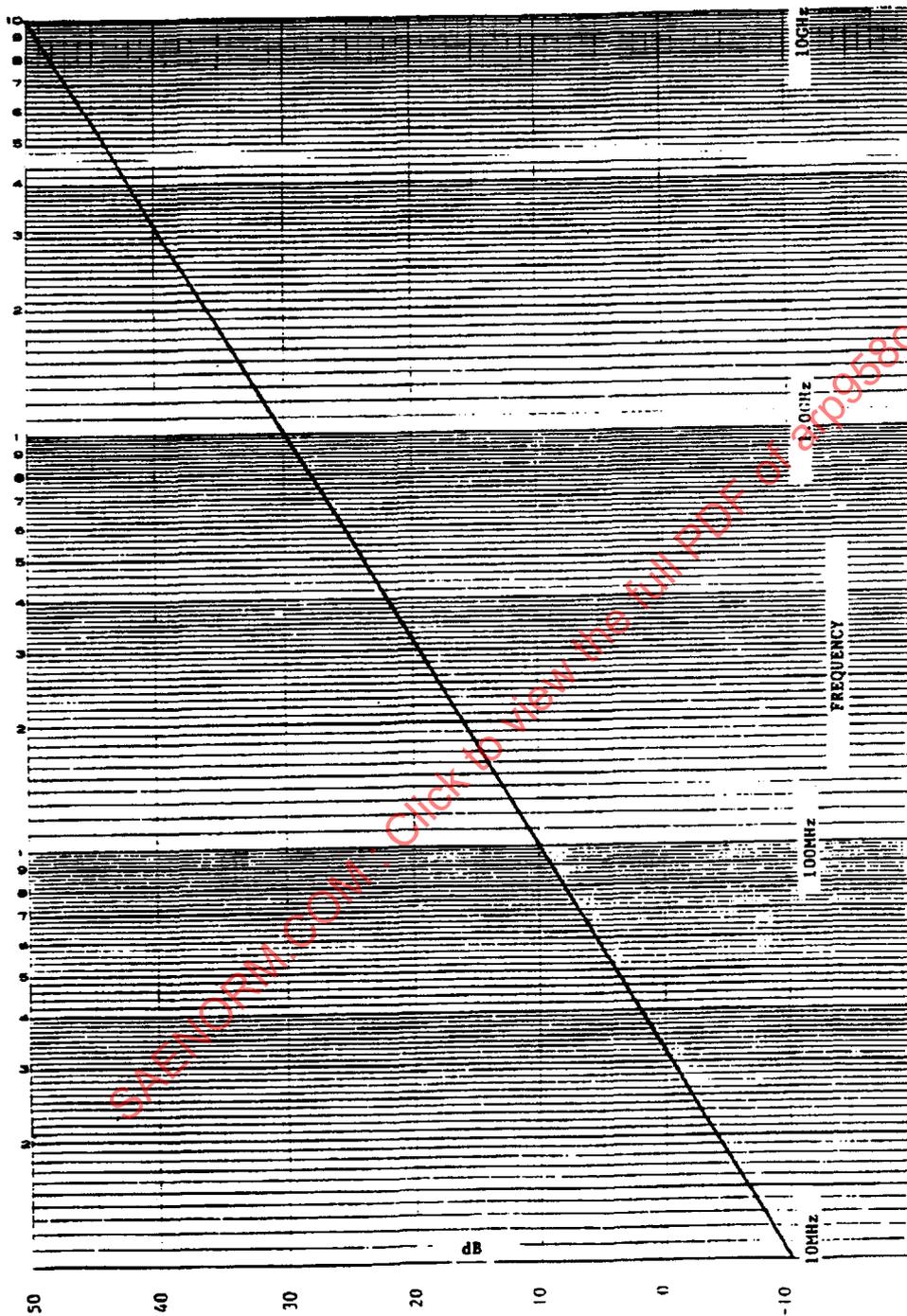


FIGURE 1 - Plot of  $20 \log_{10} \frac{9.73}{\lambda}$  as a Function of Frequency Use for Calculating Antenna Factors  $AF_1$  and  $AF_2$

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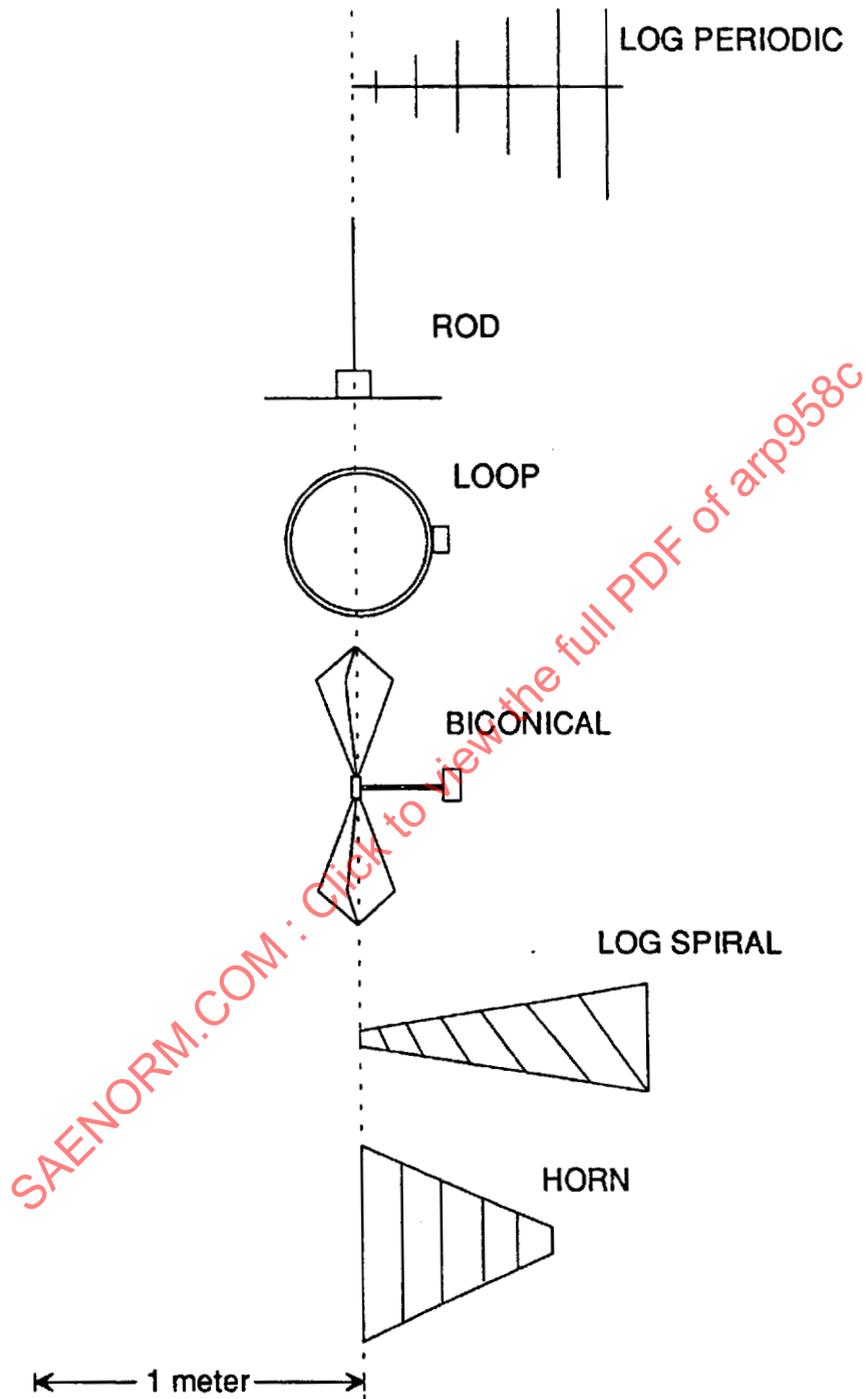


FIGURE 2 - Reference Plane for Antenna Distance

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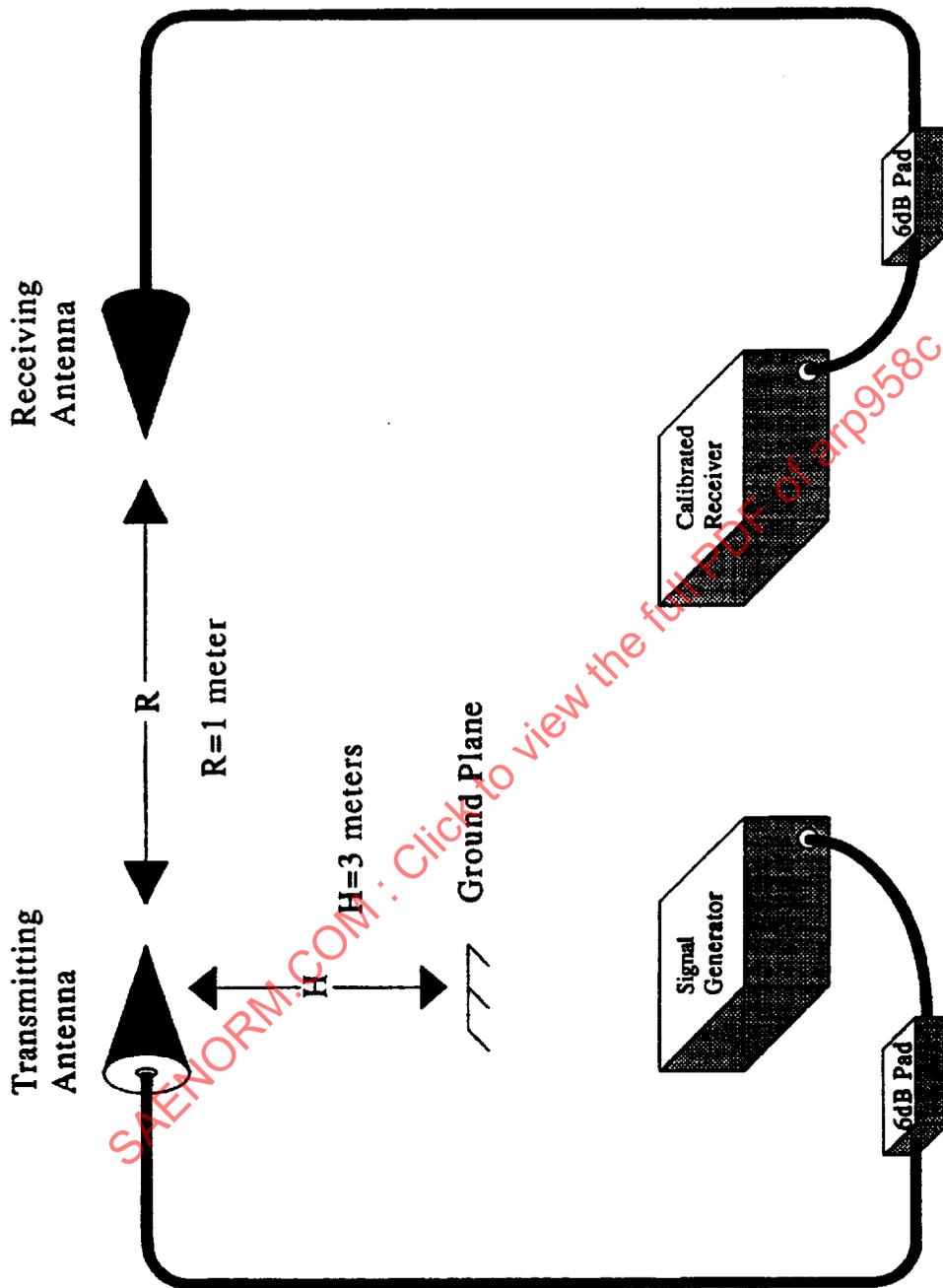
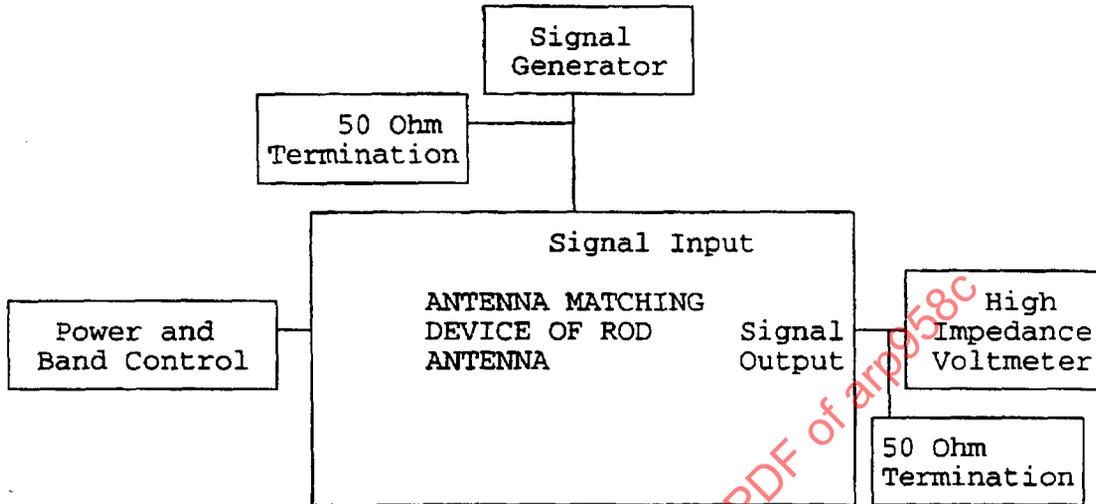


FIGURE 3 - Test Set-Up for Determining 1 m Gain Utilizing Two Identical-Antenna Technique

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NOTES:

1. At selected frequencies (4.3(g)) adjust the signal generator for a level which is sufficient for an accurate reading on the voltmeter. Insure that the level is below over-load.
2. Calculate the antenna factor (AF) where  

$$AF = 20 \text{ Log (Input Voltage / Output Voltage) } + 6 \text{ dB}$$
3. Repeat at the frequencies of 4.3(g).
4. Manufacturers should be consulted on implementation of this technique for a particular antenna due to variations between antennas.
5. All cables except for power and band control are 50  $\Omega$  coaxial cables.

FIGURE 4 - Rod Antenna Calibration Setup

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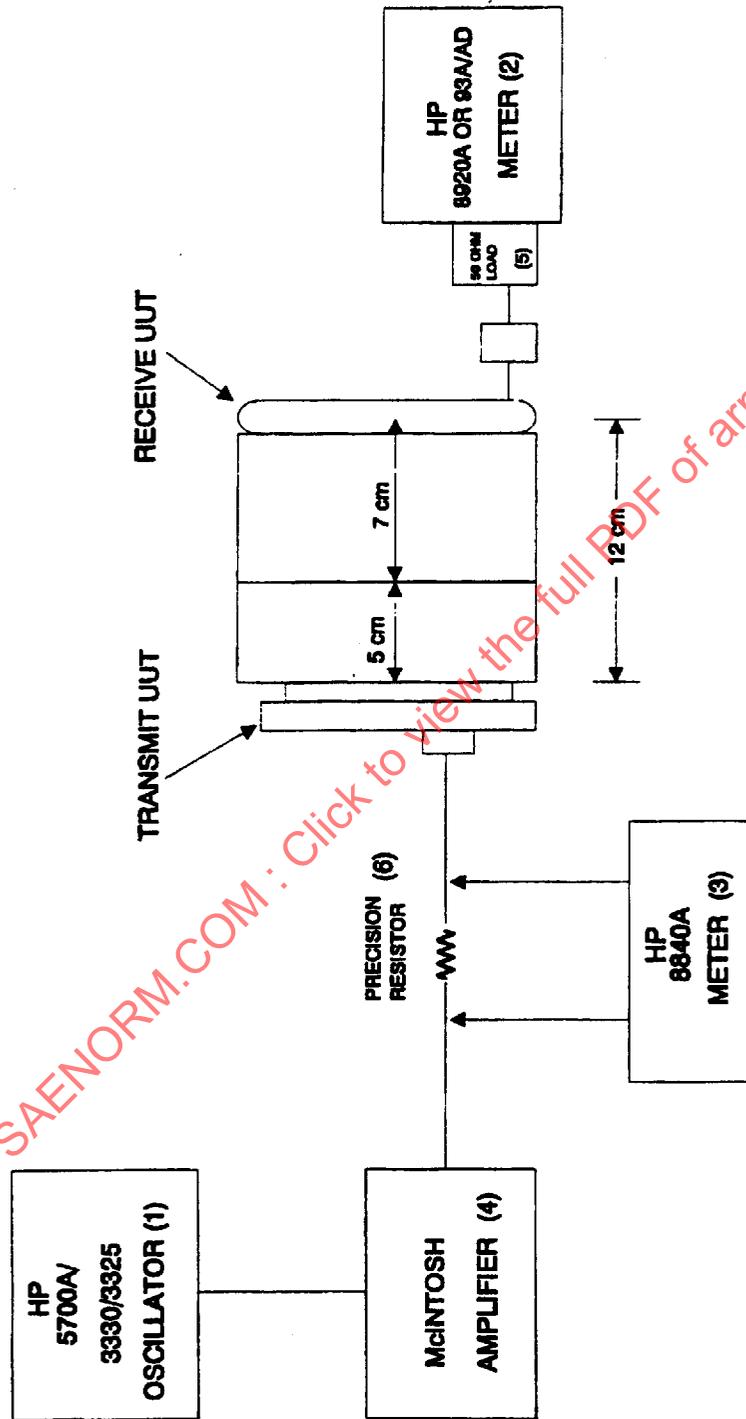


FIGURE 5 - Test Setup for Small Loop Calibration

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APPENDIX A  
ANTENNA FACTOR DERIVATION

The factor associated with any antenna of a given gain can be calculated as follows:

$$V = h_{\text{eff}} E/2 \quad (\text{Eq.A1})$$

where:

- V = voltage at input to a 50  $\Omega$  receiver
- E = field intensity in volts/meter
- $h_{\text{eff}}$  = effective height of antenna in meters

The factor of one half assumes that the voltage appearing at antenna terminals divides by one half when the 50  $\Omega$  receiver is placed across the antenna terminals.

$$h_{\text{eff}} = 2 (A_{\text{em}} R_r / Z)^{1/2} \quad (\text{Eq.A2})$$

$$A_{\text{em}} = \frac{D\lambda^2}{4\pi} \quad (\text{Eq.A3})$$

where:

- $A_{\text{em}}$  = maximum effective aperture in square meters (aperture which would deliver maximum power to a matched load)
- $R_r$  = 50  $\Omega$
- Z = 120 $\pi$  = 377  $\Omega$
- D = directivity of the antenna

Substituting (Eq.A3) into (Eq.A2):

$$h_{\text{eff}} = \lambda(Dr_r / \pi Z)^{1/2} \quad (\text{Eq.A4})$$

If a zero loss 50  $\Omega$  transmission line is assumed between the antenna and the receiver and a zero mismatch is assumed, D = G. Therefore:

$$V = \frac{E\lambda}{2} (G50 / \pi 377)^{1/2} = E \frac{\lambda}{9.73} \sqrt{G} \quad (\text{Eq.A5})$$

where:

- G = numeric power gain
- $\lambda$  = wavelength in meters

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If a conversion from V to E is now desired, it can be seen from Equation A5 that:

$$V \frac{9.73}{\lambda\sqrt{G}} = E \quad (\text{Eq.A6})$$

The antenna correction factor in going from a meter reading in volts to field intensity is then:

$$AF = \frac{9.73}{\lambda\sqrt{G}} \quad (\text{Eq.A7})$$

NOTE: If field intensity is derived from antenna induced voltage or a voltage across open circuit antenna terminals, the factors is  $\frac{4.87}{\lambda\sqrt{G}}$ .

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APPENDIX B  
CIRCULAR/LINEAR POLARIZATION

A circularly polarized wave can be represented as two E vectors in space quadrature and separated in time phase by 90° as shown below.

V is  $1/\sqrt{2}$  and P is 1/2 for linear polarization relative to circular polarization. Therefore, if an antenna is calibrated with a circularly polarized source

TABLE B1

Signal Being Measured	Gain	Correction Factor
circular	G	X
linear	G/2	2X (or add a 3 dB factor)

If an antenna is calibrated with a linear source

TABLE B2

Signal Being Measured	Gain	Correction Factor
linear	G	Y
circular	2G	Y/2 (or subtract 3 dB from the correction factor since the antenna will be reading twice as high as it should)

NOTE:  $2X = Y$ , so that final results are independent of the method of calibration.

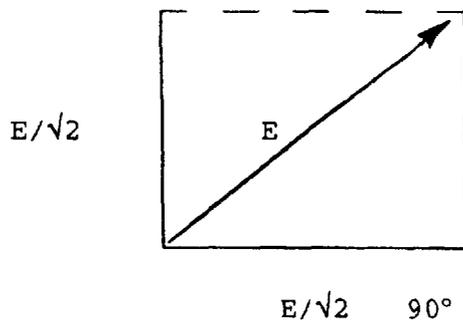


FIGURE B1

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APPENDIX C  
THREE ANTENNA DETERMINATION

The three antenna method is for calibrating antennas from site attenuation measurements made on an open field site. Reference 2.5 describes the method. Reference 2.8 also provides details on the method. This method uses three antennas taken two at a time: Antennas 1 and 2, antennas 1 and 3, and antennas 2 and 3. These are placed 1 m above the ground plane at a separation of 3 m. The receiving antenna is varied in height between 1 and 4 m to determine the maximum reception level. With the three antennas used, the results provide three equations and three unknowns. This removes source and reflection variations leaving a good far field antenna factor.

$$\begin{aligned}
 AF_1 \text{ (dB)} &= 10 \log_{10} (f_M) - 24.46 + .5 \times (E_D^{\max} + A_1 + A_2 - A_3) \\
 AF_2 \text{ (dB)} &= 10 \log_{10} (f_M) - 24.46 + .5 \times (E_D^{\max} + A_1 + A_3 - A_2) \\
 AF_3 \text{ (dB)} &= 10 \log_{10} (f_M) - 24.46 + .5 \times (E_D^{\max} + A_2 + A_3 - A_1)
 \end{aligned}
 \tag{Eq.C1}$$

where:

- A (dB) = 20 log<sub>10</sub> (V<sub>T</sub>/V<sub>R</sub>) for each of the three tests
- V<sub>T</sub> = voltage applied to transmitting antenna
- V<sub>R</sub> = voltage out of receiving antenna
- f<sub>M</sub> = frequency in MHz
- E<sub>D</sub><sup>max</sup> (dBμV/m) = calculated maximum

E<sub>D</sub><sup>max</sup> is tabulated in Table C1.

TABLE C1

F <sub>M</sub> (MHz)	E <sub>D</sub> <sup>max</sup> (dBμV/m)	F <sub>M</sub> (MHz)	E <sub>D</sub> <sup>max</sup> (dBμV/m)
25	2.3	150	12.1
30	3.5	160	12.2
35	4.6	175	12.3
40	5.6	175	12.3
45	6.4	180	12.4
50	7.1	200	12.5
60	8.3	250	12.6
70	9.2	300	12.1
80	10.0	400	11.7
90	10.5	500	12.2
100	10.9	600	12.4
120	11.6	700	12.6
125	11.7	900	12.3
140	11.9	1000	12.4

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APPENDIX D  
EXPECTED RESULTS

Appendix D contains a partial list of commercially manufactured antennas which include the frequency range and typical antenna factors. The value of the antenna factors were derived from manufacturer's data and these data are provided as typical calibration data and are not valid for all antennas. They can serve as "typical" results when using this ARP and indicate an approximate value that should be obtained when using this calibration method. They are included here to serve as a check that results obtained by this method are close to the expected results.

NOTE: Some of these antennas are no longer available and some newer ones may not be included.

## TABLE OF CONTENTS

## ANTENNA FACTORS (See Figure D1)

Fairchild PEF-10 Electric Field Probe  
 Fairchild ALP-10, 20 Hz to 50 kHz, Loop  
 Empire LG-105, 14 kHz to 150 kHz, Loop  
 Empire VR-3-105, 14 kHz to 150 kHz, Vertical  
 Empire VR-1-105, 14 kHz to 150 kHz, Vertical  
 Empire VX-105, 14 kHz to 150 kHz, 41" Vertical  
 Fairchild ALR-25, 14 kHz to 25 MHz, Magnetic Loop  
 Fairchild RVR-25, 14 kHz to 25 MHz, 41" Vertical  
 Empire LP-105, .15 MHz to 30 MHz, Loop  
 Empire VA-105, .150 Mhz to 30 MHz, 41" Vertical  
 EMCO 3104, 20 MHz - 200 MHz, Biconical  
 (S/N 2139 and S/N 2140)  
 Fairchild BDA-25, 20 MHz to 55 MHz Broadband Dipole  
 Double Extension  
 Honeywell 7833, 20 MHz to 300 MHz Bi-Conical  
 Fairchild BIA-25, 20 MHz to 200 MHz  
 Bi-Conical  
 CDI B100 Bi-Conical, 20 MHz to 200 MHz  
 Fairchild BDA-25, 24 MHz to 210 MHz, Broadband  
 Dipole. No Extension  
 Empire DM-105-T1, 25 MHz to 200 MHz, Dipole  
 Honeywell 7826, 200 MHz to 1000 MHz Conical-Log Spiral  
 Fairchild BDA-25, 45 MHz to 120 MHz, Broadband Dipole, Single  
 Extension  
 Roberts Antenna TM Dipole, 30 MHz to 1.0 GHz  
 CDI B300 Bi-Conical, 400 MHz to 1.0 GHz  
 CDI B200 Bi-Conical, 175 MHz to 400 MHz  
 Empire DM-105-T2, 190 MHz - 400 MHz, Dipole  
 Fairchild LCA-25, 200 MHz - 1000 MHz  
 Conical Log Spiral

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TABLE OF CONTENTS (Continued)

Honeywell 7828, 1 GHz to 10 GHz  
Conical-Log Spiral  
Stoddart 93490-1, 200 MHz to 1000 MHz  
Conical Log Spiral  
Empire DM-105-T3, 400 MHz - 1000 MHz, Dipole  
EMCO CLP-1 B, 1 GHz - 10 GHz Conical Log Spiral  
Singer EMA 910 Series, 1 GHz to 10.5 GHz, Horns  
Polarad CA Series, 1 GHz - 10 GHz, Horns  
EMCO 3105, 1 to 12.4 GHz  
Stoddart 93491-1, 1 GHz to 10 GHz, Conical Log Spiral

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#### FAIRCHILD PEF-10, ELECTRIC FIELD PROBE

Add 32dB to meter reading to obtain accurate volts/meter reading when E-Field measurements are made according to section 3.14.4 of the EMC-10 instrumentation manual.

FAIRCHILD ALP-10, 20 Hz to 50 kHz, LOOP				EMPIRE LG-105, 14 kHz to 150 kHz, LOOP		
FREQUENCY (Hz)	AF (dB)	FREQUENCY (Hz)	AF (dB)	NF-105 BAND	FREQUENCY (kHz)	AF (dB)
20	62	1000	26	1	14	7
30	56	1200	25		16	6
40	54	1400	24		20	5
50	52	1600	22		24	4
60	50	2000	21		25	4
70	49	2400	19			
80	48	2800	18	2	25	4
90	47	3200	16		30	3
100	46	3600	15		35	2
120	45	4000	14		40	1
140	43	4800	13		45	0
170	42	5600	12		50	1
200	40	6200	11		60	1
230	39	7000	10			
260	38	8000	9	3	62	0
300	37	9000	8		70	-3
350	36	10,000	7		80	-5
400	35	13,000	6		120	-6
450	33	20,000	5		140	-4
500	32	30,000	4		150	-5
550	31	50,000	.3			
600	30					
700	29					
800	28					
900	27					

Note 1: Meter reading (dBμV) + Antenna factor (dB) = Field Intensity (dBμA/m).

Note 2: To read the E-field (Far Field), add 51.5 dB to the dBμA/m value to get dBμV/m.

Note 1: These factors apply for a non-sensitized calibration of the receivers.

Note 2: Meter reading (dBμV) + Antenna factor (dB) = Field Intensity (dBμA/m).

Note 3: To read the E-field (Far Field), add 51.5 dB to the dBμA/m value to get dBμV/m.

#### EMPIRE VR-3-105, 14 kHz to 150 kHz, VERTICAL

FREQUENCY (kHz)	AF (dB)
14	44
20	44
25	42
35	41
60	41
100	41
150	41

Note 1: These values apply to a non-sensitized calibration of the NR-150 receiver.

Note 2: Meter reading (dBμV) + Antenna Factor (dB) = Field intensity (dBμV/m).

#### EMPIRE VR-1-105, 14 kHz to 150 kHz, VERTICAL

FREQUENCY (kHz)	AF (dB)
14	52
20	50
25	48
35	47
60	46
100	46
150	46

Note 1: These values apply to a non-sensitized calibration of the NF-150 receiver

Note 2: Meter reading (dBμV) + Antenna factor (dB) = Field intensity (dBμV/m).

FIGURE D1

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EMPIRE VX-105, 14 kHz to 150 kHz, 41" VERTICAL			FAIRCHILD ALR-25, 14 kHz TO 25 MHz, MAGNETIC LOOP					
NF-105 BAND	FREQUENCY (kHz)	AF (dB)	EMC-25 BAND	FREQUENCY (MHz)	AF (dB)			
1	14	47	1	.014	15			
	15	46		.018	14			
	16	45		.024	13			
	18	44		.030	13			
	20	43		2	.030	11		
	25	45			.038	10		
	2	25			51	.162	10	
		30			49	3	.060	8
		35			48		.076	7
		40		46	.124		7	
45		44	4	.120	-3			
50		43		.140	2			
55		42		.180	3			
60		40		.260	3			
62		47		5	.240	-1		
75		46	.280		-2			
80	45	.520	-2					
90	42	6	.5		-3			
100	40		1.1		-3			
110	39		7	1.1	-6			
120	38			1.4	-7			
130	37			1.6	-6			
140	37	2.2		-7				
150	36	2.4		-7				
3			8	2.3	-9			
				2.5	-10			
				5.3	-10			
				9	5	-11		
					10	-12		
11	-13							
12	-13							
10	11	-17						
	18	-18						
	20	-19						
	22	-20						
	24	-22						
			25	-22				

Note 1: These values apply to a non-sensitized calibration of the receiver.  
 Note 2: Meter reading (dBμV) - Antenna factor (dB) - Field intensity (dBμV/m).

Note 1: Meter reading (dBμV) + Antenna factor (dB) = Field intensity (dBμV/m).  
 Note 2: To read the E-field (Far Field), add 51.5 dB to the dBμV/m

FIGURE D1 (Continued)