



Society of Automotive Engineers, Inc.
400 COMMONWEALTH DRIVE, WARRENDALE, PA. 15096

AEROSPACE MATERIAL SPECIFICATION

AMS 7464 B
Superseding AMS 7464A

Issued 2-15-65
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BOLTS AND SCREWS, STEEL, LOW-ALLOY HEAT-RESISTANT
220,000 psi (1517 MPa) Tensile Strength
Hardened and Tempered, Roll Threaded

1. SCOPE:

1.1 Type: This specification covers premium quality bolts and screws made from a low-alloy, heat-resistant steel and having threads of UNJ (MIL-S-8879) form.

1.2 Application: Primarily for joining parts where a combination of fatigue resistance and high strength is required for applications between -100°F (-73°C) and +1000°F (+538°C) in highly stressed locations. A coating, such as AMS 2416 or AMS 2506, is recommended for corrosion protection.

2. APPLICABLE DOCUMENTS: The following publications form a part of this specification to the extent specified herein. The latest issue of Aerospace Material Specifications (AMS) and Aerospace Standards (AS) shall apply. The applicable issue of other documents shall be as specified in AMS 2350.

2.1 SAE Publications: Available from Society of Automotive Engineers, Inc., 400 Commonwealth Drive, Warrendale, PA 15096.

2.1.1 Aerospace Material Specifications:

AMS 2350 - Standards and Test Methods

AMS 2373 - Quality Assurance Sampling of Bolts and Screws

AMS 6485 - Steel Bars and Forgings, 5.0Cr - 1.3Mo - 0.50V (0.38 - 0.43C)

AMS 6487 - Steel Bars and Forgings, 5.0Cr - 1.3Mo - 0.50V (0.38 - 0.43C), Premium Quality, Consumable Electrode Vacuum Melted

AMS 6488 - Steel Bars and Forgings, 5.0Cr - 1.3Mo - 0.50V (0.38 - 0.43C), Premium Quality

2.1.2 Aerospace Standards:

AS 1132 - Design Parameters for Bolts and Screws, External Wrenching, Unified Thread Inch Series

AS 1177 - Nondestructive Inspection Standards for Bolts and Screws

AS 3062 - Bolts, Screws, and Studs, Screw Thread Requirements

AS 3063 - Bolts, Screws, and Studs, Straightness, Concentricity, and Squareness Requirements

2.2 ASTM Publications: Available from American Society for Testing and Materials, 1916 Race Street, Philadelphia, PA 19103.

ASTM A370 - Mechanical Testing of Steel Products

ASTM E21 - Elevated Temperature Tension Tests of Metallic Materials

ASTM E139 - Conducting Creep, Creep-Rupture, and Stress-Rupture Tests of Metallic Materials

2.3 Government Publications: Available from Commanding Officer, Naval Publications and Forms Center, 5801 Tabor Avenue, Philadelphia, PA 19120.

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2.3.1 Military Standards:

MIL-STD-794 - Parts and Equipment, Procedures for Packaging and Packing of
MIL-STD-1312 - Fasteners, Test Methods

3. TECHNICAL REQUIREMENTS:

Ø 3.1 Material: Shall be AMS 6485, AMS 6487, or AMS 6488 steel.

3.2 Fabrication:

3.2.1 Blanks: Heads shall be formed by either hot or cold forging.

3.2.2 Heat Treatment: Headed blanks shall, before finishing the shank and the bearing surface of the head, cold working the head-to-shank fillet radius, and rolling the threads, be heat treated as follows:

3.2.2.1 Heating Equipment: Furnaces may be any type ensuring uniform temperature throughout the parts being heated and shall be equipped with, and operated by, automatic temperature controllers. The heating medium or atmosphere shall cause neither surface hardening nor decarburization other than that permitted by 3.4.3.2 and 3.4.3.3.

3.2.2.2 Annealing: Blanks shall be annealed by heating to a temperature within the range 1500° - 1650° F (815.6° - 898.9° C), holding at the selected temperature within $\pm 25^\circ$ F ($\pm 14^\circ$ C) for 2 hr ± 5 min., and cooling at a rate not greater than 50 F (28 C) deg per hr to 1000° F (538° C) or below, and then cooling as desired.

3.2.2.3 Hardening: Annealed blanks shall be uniformly heated to 1850° F ± 25 (1010° C ± 14), held at heat for 15 - 45 min., and cooled in air; preheating of blanks to 1450° F (788° C) before transferring to the austenitizing furnace at 1850° F (1010° C) is permissible.

3.2.2.4 Tempering: Hardened blanks shall be tempered three times by heating uniformly to the respective tempering temperature, holding at heat for 2 - 3 hr, and cooling in air; the temperature for the first and second tempering operations shall be not lower than 1060° F (571° C) and the temperature for the third tempering operation shall be not more than 25 F (14 C) deg below that of the second tempering operation.

3.2.2.5 Stress-Relief: After removal of oxide and decarburization but before cold working the fillet radius and rolling the threads, blanks shall be stress relieved by heating to a temperature not more than 25 F (14 C) deg below that of the final tempering temperature, holding at heat for 2 - 3 hr, and cooling in air.

3.2.3 Oxide and Decarburization Removal: The heat treated blanks, before cold working the fillet radius and rolling the threads, shall have all surfaces free from surface oxide, oxide penetration, and decarburization except as permitted in 3.4.3.3. The removal process shall produce no intergranular attack or corrosion of the blanks. The metal removed from the bearing surface of the head and the full body diameter of the shank shall be as little as practicable to obtain a clean, smooth surface and in no case shall be so great as to produce more cutting of flow lines in the head-to-shank junction than shown in Fig. 1B.

- 3.2.4 **Cold Working of Fillet Radius:** After removal of oxide and decarburization as in 3.2.3, the head-to-shank fillet radius of parts having the radius complete throughout the circumference of the part shall be cold worked sufficiently to remove all visual evidence of grinding or tool marks and to produce the fatigue strength of 3.3.5. Distortion due to cold working shall not raise metal more than 0.002 in. (0.05 mm) above the contour at "A" or depress metal more than 0.002 in. (0.05 mm) below the contour at "B" as shown in Fig. 2; distorted areas shall not extend beyond "C" as shown in Fig. 2. In configurations having an undercut associated with the fillet radius, the cold working will be required only for 90 deg (1.57 rad) of fillet arc, starting at the point of tangency of the fillet radius and the bearing surface of the head.
- 3.2.5 **Thread Rolling:** Threads shall be formed on the heat treated and finished blanks by a single rolling process.
- 3.3 **Properties:** Parts shall conform to the requirements of 3.3.1, 3.3.2, 3.3.3, 3.3.4, and 3.3.5. Threaded members of gripping fixtures for tensile tests shall be of sufficient size and strength to develop the full strength of the part without stripping the thread. Finished parts shall be tested in accordance with the following applicable test methods of MIL-STD-1312:

| Property | Test Method |
|------------------------------|-------------|
| Hardness | No. 6 |
| Room Temperature Tensile | No. 8 |
| Stress Rupture | No. 10 |
| Fatigue | No. 11 |
| Elevated Temperature Tensile | No. 18 |

3.3.1 **Tensile Properties at Room Temperature:**

- 3.3.1.1 **Finished Parts:** Parts having hardness within the range 46 - 50 HRC shall have breaking load not lower than that specified in Table II. If the size or shape of the part is such that failure would occur outside the threaded section but the part can be tested satisfactorily, such as parts having a shank diameter equal to or less than the minimum pitch diameter or having an undercut, parts shall conform to only the tensile strength requirement of 3.3.1.2; for such parts, the diameter on which stress is based shall be the actual measured minimum diameter of the part. Tension fasteners with either standard double hexagon or hexagon type heads having a minimum metal condition in the head equal to the design parameters specified in AS 1132 shall not fracture in the head-to-shank fillet radius except when this radius is associated with an undercut.
- 3.3.1.2 **Machined Test Specimens:** If the size or shape of the part is such that a tensile test cannot be made on the part, tensile tests shall be conducted in accordance with ASTM A370 on specimens machined from finished parts or from coupons of the same heat of steel heat treated with the parts. Specimens shall conform to the following requirements:

| | |
|--|------------------------|
| Tensile Strength, min | 220,000 psi (1517 MPa) |
| Elongation in 2 in. (50.8 mm) or 4D, min | 12% |
| Reduction of Area, min | 43% |

- 3.3.1.2.1 When permitted by purchaser, hardness tests on the end of parts may be substituted for tensile tests of machined specimens.

3.3.2 **Tensile Properties at 900° F (482.2° C):**

- 3.3.2.1 **Finished Parts:** Parts heated to 900° F ± 3 (482.2° C ± 1.7), held at heat for 30 min. ± 3 before testing, and tested at 900° F ± 3 (482.2° C ± 1.7) shall have breaking load not lower than that specified in Table II. If the size or shape of the part is such that failure would occur outside the threaded section but the part can be tested satisfactorily, such as parts having a shank diameter equal to or less than the minimum pitch diameter or having an undercut, parts shall conform to only the tensile strength requirement of 3.3.2.2; for such parts, the diameter on which stress is based shall be the actual measured minimum diameter of the part.
- 3.3.2.2 **Machined Test Specimens:** If the size or shape of the part is such that a tensile test cannot be made on the part, specimens prepared as in 3.3.1.2, heated to 900° F ± 3 (482.2° C ± 1.7), held at heat for 30 min. ± 3 before testing, and tested in accordance with ASTM E21 at 900° F ± 3 (482.2° C ± 1.7) shall conform to the following requirements:
- | | |
|--|-------------------------|
| Tensile Strength, min | 170, 000 psi (1172 MPa) |
| Elongation in 2 in. (50.8 mm) or 4D, min | 15% |
| Reduction of Area, min | 50% |
- 3.3.3 **Hardness:** Shall be uniform and within the range 46 - 50 HRC or equivalent but hardness of the threaded section and of the head-to-shank fillet area may be higher as a result of the cold working operations.
- 3.3.4 **Stress-Rupture Properties at 900° F (482.2° C)**
- 3.3.4.1 **Finished Parts:** Parts, maintained at 900° F ± 3 (482.2° C ± 1.7) while the load specified in Table II is applied continuously, shall not rupture in less than 100 hours. If the shank diameter of the part is less than the minimum pitch diameter of the thread but the part can be tested satisfactorily, parts shall conform to the requirements of 3.3.4.1.1.
- 3.3.4.1.1 Parts having a shank diameter less than the minimum pitch diameter of the part shall be tested as in 3.3.4.1 except that the load shall be as specified in 3.3.4.2. The diameter on which stress is based shall be the actual measured minimum diameter of the part.
- 3.3.4.2 **Machined Test Specimens:** If the size or shape of the part is such that a stress-rupture test cannot be made on the part, a test specimen, maintained at 900° F ± 3 (482.2° C ± 1.7) while a load sufficient to produce an initial axial stress of 130,000 psi (896 MPa) is applied continuously, shall not rupture in less than 100 hours. Specimens shall be machined from finished parts, or from coupons of the same heat of steel heat treated with the parts, to the dimensions shown in ASTM A370. Tests shall be conducted in accordance with ASTM E139.
- 3.3.5 **Fatigue Strength:** Parts tested in tension-tension fatigue at room temperature with maximum load as specified in Table II and minimum load equal to 10% of maximum load shall have average life of not less than 65, 000 cycles with no part having life less than 45, 000 cycles. Tests need not be run beyond 130, 000 cycles. Life of parts which do not fail in 130, 000 cycles shall be taken as 130, 000 cycles for purposes of computing average life. If the shank diameter of the part is less than the minimum pitch diameter of the part, parts shall withstand fatigue testing as above using loads sufficient to produce a maximum stress of 106, 000 psi (731 MPa) and a minimum stress of 10, 600 psi (73.1 MPa). The above requirements apply only to parts 0.138 in. (3.51 mm) and larger in nominal thread size with round, square, hexagonal, or double hexagonal heads designed for tension applications and not having an undercut.
- 3.4 **Quality:** Parts shall be uniform in quality and condition, clean, sound, smooth, and free from burrs and foreign materials and from internal and external imperfections detrimental to their performance. Parts shall conform to AS 1177.

- 3.4.1 Dimensional Examination: Parts shall conform to the following:
- 3.4.1.1 Straightness, Concentricity, and Squareness: Parts shall be within the limits of the drawing, determined in accordance with AS 3063.
- 3.4.1.2 Threads: Shall be as specified on the drawing and shall conform to AS 3062.
- 3.4.2 Macroscopic Examination: Parts or sections of parts, as applicable, shall be etched in a solution of approximately 50% hydrochloric acid (sp gr 1.19) and 50% water for sufficient time to reveal flow lines but not longer than 15 min. and examined at approximately 20X magnification to determine conformance to the following requirements, except that examination for the thread imperfections of 3.4.2.3 may be made by microscopic examination of specimens polished and etched as in 3.4.3.
- 3.4.2.1 Flow Lines:
- 3.4.2.1.1 Examination of a longitudinal section through the part shall show flow lines in the shank, head-to-shank fillet, and bearing surface which follow the contour of the part as shown in Fig. 1A, except that slight cutting of flow lines by the oxide and decarburization removal process of 3.2.3 is permissible, as shown in Fig. 1B; excessive cutting of flow lines in the shank, head-to-shank fillet, and bearing surface, as shown in Fig. 1C, is not permissible except when an undercut is associated with the fillet radius. The head style shown in Figs. 1A through 1C is for illustrative purposes only but other symmetrical head styles shall conform to the above requirements. Flow lines in upset heads on parts having special heads, such as Dee- or Tee-shaped heads or particularly thin heads, shall be as agreed upon by purchaser and vendor.
- 3.4.2.1.2 Flow lines in threads shall be continuous, shall follow the general thread contour, and shall be of maximum density at root of thread (See Fig. 3).
- 3.4.2.2 Internal Defects: Examination of longitudinal sections of the head and shank and of the threads shall reveal no cracks or other injurious imperfections. The head and shank section shall extend not less than $D/2$ from the bearing surface of the head and the threaded section shall extend not less than $D/2$ beyond the thread runout where "D" is the nominal diameter of the shank after heading. If the two sections would overlap, the entire length of the part shall be sectioned and examined as a whole.
- 3.4.2.3 Threads:
- 3.4.2.3.1 Root defects such as notches, slivers, folds, roughness, and oxide scale are not permissible (See Fig. 4).
- 3.4.2.3.2 Multiple laps on the flanks of threads are not permissible regardless of location. Single laps on the flanks of threads that extend toward the root are not permissible (See Figs. 5 and 6).
- 3.4.2.3.3 There shall be no laps along the flank of the thread below the pitch diameter (See Fig. 7). A single lap is permissible along the flank of the thread above the pitch diameter on either the pressure or nonpressure flank (one lap at any cross section through the thread) provided it extends toward the crest and generally parallel to the flank (See Fig. 7).
- 3.4.2.3.4 Crest craters, crest laps, or a crest lap in combination with a crest crater are permissible provided that the imperfections do not extend deeper than 20% of the basic thread height (See Table I) as measured from the thread crest when the thread major diameter is at minimum size (See Fig. 8). The major diameter of the thread shall be measured prior to sectioning. As the major diameter of the thread approaches maximum size, values for depth of crest crater and crest lap imperfections listed in Table I may be increased by 1/2 of the difference between the minimum major diameter and the actual major diameter as measured on the part.

3.4.3 Microscopic Examination: Specimens cut from parts shall be polished, etched in 2% Nital, and examined at not lower than 100X magnification to determine conformance to the following requirements.

3.4.3.1 Microstructure: Parts shall have microstructure of tempered martensite.

3.4.3.2 Surface Hardening: Parts shall have no surface hardening except as produced during cold working of the head-to-shank fillet radius and during rolling of threads. There shall be no evidence of carburization, carbon restoration, or nitriding. In case of dispute over results of the microscopic examination, microhardness testing shall be used as a referee method; a Vickers hardness reading within 0.003 in. (0.08 mm) of the surface more than 30 points higher than the reading in the core will be evidence of nonconformance to this requirement.

3.4.3.3 Decarburization:

3.4.3.3.1 The bearing surface of the head, the head-to-shank fillet radius, the shank, and the threads shall be free from decarburization.

3.4.3.3.2 Depth of decarburization on those surfaces of the head which are the original surfaces of the bar shall be not greater than that permitted by the applicable material specification.

3.4.3.3.3 Depth of decarburization on the OD of the head of cylindrical head parts made by upsetting is not restricted.

3.4.3.3.4 Depth of decarburization at any point on any surface not covered by 3.4.3.3.1, 3.4.3.3.2, or 3.4.3.3.3, shall not exceed 0.002 in. (0.05 mm).

4. QUALITY ASSURANCE PROVISIONS:

4.1 Responsibility for Inspection: The vendor of parts shall supply all samples and shall be responsible for performing all required tests. Results of such tests shall be reported to the purchaser as required by 4.4. Purchaser reserves the right to perform such confirmatory testing as he deems necessary to ensure that the parts conform to the requirements of this specification.

4.2 Classification of Tests:

4.2.1 Acceptance Tests: Tests to determine conformance to tensile properties at room temperature (3.3.1) and hardness (3.3.3) requirements are classified as acceptance or routine control tests.

4.2.2 Qualification Tests: Tests to determine conformance to tensile properties at 900° F (482.2° C) (3.3.2), stress rupture (3.3.4), and fatigue strength (3.3.5) requirements are classified as qualification or periodic control tests.

4.2.2.1 For direct U. S. Military procurement, qualification test material and supporting test data shall be submitted to the cognizant qualification agency as directed by the request for procurement, the procuring activity, or the contracting officer.

4.3 Sampling: Shall be in accordance with AMS 2373.

4.4 Reports: The vendor of parts shall furnish with each shipment three copies of a report stating that the chemical composition of the parts conforms to the applicable material specification, showing the results of tests to determine conformance to the hardness and room temperature tensile strength requirements, and stating that the parts conform to the other technical requirements of this specification. This report shall include the purchase order number, this specification number and its revision letter, contractor or other direct supplier of material, part number, and quantity.

4.5 Resampling and Retesting: If any part or specimen used in the above tests fails to meet the specified requirements, disposition of the parts may be based on the results of testing three additional parts or specimens for each original nonconforming specimen. Failure of any retest part or specimen to meet the specified requirements shall be cause for rejection of the parts represented and no additional testing shall be permitted. Results of all tests shall be reported.

5. PREPARATION FOR DELIVERY:

5.1 Identification: Each different part number shall be packed in a separate container. Each container shall be marked to show the following information:

BOLTS (OR SCREWS) LOW-ALLOY HEAT-RESISTANT STEEL
AMS 7464B
PART NUMBER _____
PURCHASE ORDER NUMBER _____
QUANTITY _____
MANUFACTURER'S IDENTIFICATION _____

5.2 Packaging:

5.2.1 Containers of parts shall be prepared for shipment in accordance with commercial practice to ensure carrier acceptance and safe transportation to the point of delivery. Packaging shall conform to carrier rules and regulations applicable to the mode of transportation.

5.2.2 For direct U. S. Military procurement, packaging shall be in accordance with MIL-STD-794, Level Ø A or Level C, as specified in the request for procurement. Commercial packaging as in 5.2.1 will be acceptable if it meets the requirements of Level C.

6. ACKNOWLEDGMENT: A vendor shall mention this specification number and its revision letter in all quotations and when acknowledging purchase orders.

7. REJECTIONS: Parts not conforming to this specification or to authorized modifications will be subject to rejection.

8. NOTES:

8.1 Marginal Indicia: The phi (Ø) symbol is used to indicate technical changes from the previous issue of this specification.

8.2 For direct U. S. Military procurement, purchase documents should specify the following:

- Title, number, and date of this specification
- Part number or size of parts desired
- Quantity of parts desired
- Applicable level of packaging (See 5.2.2).

TABLE I

| Thread Per Inch | Basic Thread Height Ref (See Note 1) | | 20% Basic Thread Height | |
|--------------------|---|--------------|-------------------------------|--------------|
| | Inch | (Millimeter) | Inch | (Millimeter) |
| 80 | 0.0081 | (0.206) | 0.0016 | (0.041) |
| 72 | 0.0090 | (0.229) | 0.0018 | (0.046) |
| 64 | 0.0102 | (0.259) | 0.0020 | (0.051) |
| 56 | 0.0116 | (0.295) | 0.0023 | (0.058) |
| 48 | 0.0135 | (0.343) | 0.0027 | (0.069) |
| 44 | 0.0148 | (0.376) | 0.0030 | (0.076) |
| 40 | 0.0162 | (0.411) | 0.0032 | (0.081) |
| 36 | 0.0180 | (0.457) | 0.0036 | (0.091) |
| 32 | 0.0203 | (0.516) | 0.0041 | (0.104) |
| 28 | 0.0232 | (0.589) | 0.0046 | (0.117) |
| 24 | 0.0271 | (0.688) | 0.0054 | (0.137) |
| 20 | 0.0325 | (0.826) | 0.0065 | (0.165) |
| 18 | 0.0361 | (0.917) | 0.0072 | (0.183) |
| 16 | 0.0406 | (1.031) | 0.0081 | (0.206) |
| 14 | 0.0464 | (1.179) | 0.0093 | (0.236) |
| 13 | 0.0500 | (1.270) | 0.0100 | (0.254) |
| 12 | 0.0541 | (1.374) | 0.0108 | (0.274) |
| 11 | 0.0590 | (1.499) | 0.0118 | (0.300) |
| 10 | 0.0650 | (1.651) | 0.0130 | (0.330) |
| 9 | 0.0722 | (1.834) | 0.0144 | (0.366) |
| 8 | 0.0812 | (2.062) | 0.0163 | (0.414) |

Note 1. Basic thread height is defined as being equivalent to 0.650 times the pitch.

TABLE II

| Thread Size | Tensile Breaking Load lb, min | | Maximum Fatigue Test Load, lb | Stress Rupture Test Load, lb |
|-------------|----------------------------------|----------|-------------------------------------|------------------------------------|
| | Room Temperature | 900° F | | |
| 0.112 -40 | 1, 520 | 1, 170 | -- | 897 |
| 0.112 -48 | 1, 610 | 1, 240 | -- | 949 |
| 0.138 -32 | 2, 290 | 1, 770 | 1, 100 | 1, 350 |
| 0.138 -40 | 2, 460 | 1, 900 | 1, 180 | 1, 460 |
| 0.164 -32 | 3, 430 | 2, 650 | 1, 650 | 2, 030 |
| 0.164 -36 | 3, 540 | 2, 740 | 1, 700 | 2, 090 |
| 0.190 -32 | 4, 770 | 3, 690 | 2, 290 | 2, 820 |
| 0.250 -28 | 8, 540 | 6, 600 | 4, 100 | 5, 040 |
| 0.3125 -24 | 13, 500 | 10, 400 | 6, 480 | 7, 980 |
| 0.375 -24 | 20, 900 | 16, 200 | 10, 000 | 12, 400 |
| 0.4375 -20 | 28, 300 | 21, 900 | 13, 600 | 16, 700 |
| 0.500 -20 | 37, 800 | 29, 200 | 18, 100 | 22, 300 |
| 0.5625 -18 | 47, 900 | 37, 000 | 23, 000 | 28, 300 |
| 0.625 -18 | 59, 900 | 46, 300 | 28, 800 | 35, 400 |
| 0.750 -16 | 87, 000 | 67, 200 | 41, 700 | 51, 400 |
| 0.875 -14 | 119, 000 | 91, 700 | 57, 100 | 70, 100 |
| 1.000 -12 | 155, 000 | 119, 000 | 74, 400 | 91, 400 |

TABLE II (SI)

| Thread Size | Tensile Breaking Load N, min | | Maximum Fatigue Test Load, N | Stress Rupture Test Load, N |
|-------------|---------------------------------|----------|------------------------------------|-----------------------------------|
| | Room Temperature | 482.2° C | | |
| 0.112 -40 | 6, 760 | 5, 200 | -- | 3, 990 |
| 0.112 -48 | 7, 160 | 5, 520 | -- | 4, 220 |
| 0.138 -32 | 10, 200 | 7, 870 | 4, 890 | 6, 000 |
| 0.138 -40 | 10, 900 | 8, 450 | 5, 250 | 6, 490 |
| 0.164 -32 | 15, 300 | 11, 800 | 7, 340 | 9, 030 |
| 0.164 -36 | 15, 700 | 12, 200 | 7, 560 | 9, 300 |
| 0.190 -32 | 21, 200 | 16, 400 | 10, 200 | 12, 500 |
| 0.250 -28 | 38, 000 | 29, 400 | 18, 200 | 22, 400 |
| 0.3125 -24 | 60, 000 | 46, 300 | 28, 800 | 35, 500 |
| 0.375 -24 | 93, 000 | 72, 100 | 44, 500 | 55, 200 |
| 0.4375 -20 | 126, 000 | 97, 400 | 60, 500 | 74, 300 |
| 0.500 -20 | 168, 000 | 130, 000 | 80, 500 | 99, 200 |
| 0.5625 -18 | 213, 000 | 165, 000 | 102, 000 | 126, 000 |
| 0.625 -18 | 266, 000 | 206, 000 | 128, 000 | 157, 000 |
| 0.750 -16 | 387, 000 | 299, 000 | 185, 000 | 229, 000 |
| 0.875 -14 | 529, 000 | 408, 000 | 254, 000 | 312, 000 |
| 1.000 -12 | 689, 000 | 529, 000 | 331, 000 | 407, 000 |

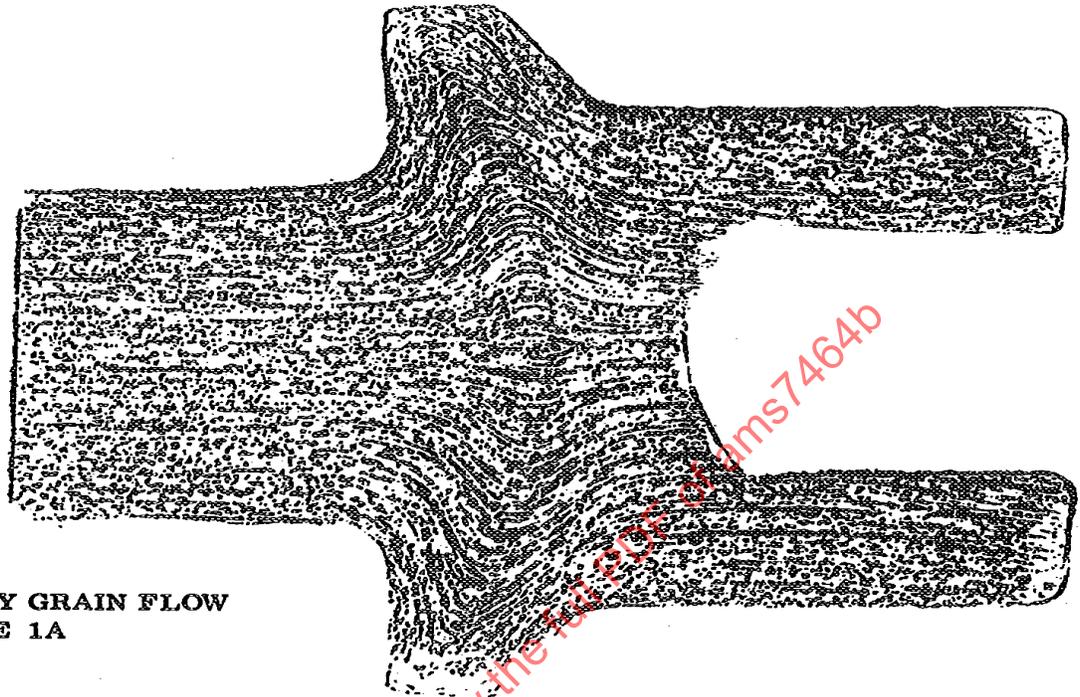
Note 1. Area upon which stress for tensile breaking load requirements and stress-rupture test load requirements is based is 98% of basic pitch diameter for nominal thread major diameters up to 0.3125 in. (7.938 mm), incl, and the basic pitch diameter for larger sizes.

Load requirements are based on:

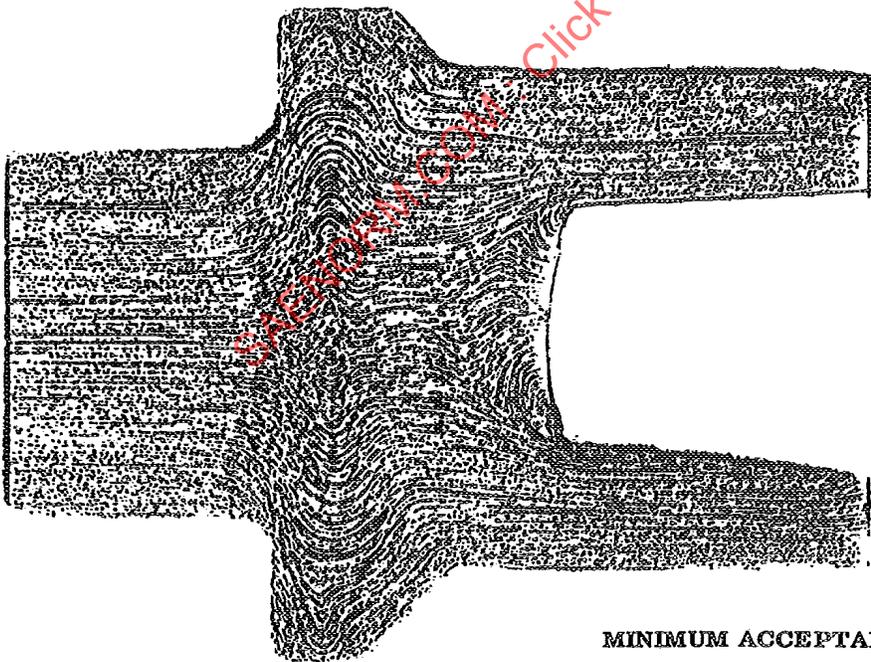
220, 000 psi (1517 MPa) for tensile breaking loads at room temperature
170, 000 psi (1172 MPa) for tensile breaking loads at 900° F (482.2° C)
48% of the tensile breaking loads at room temperature for maximum
fatigue test loads
130, 000 psi (896 MPa) for stress-rupture test loads

Note 2. For sizes not shown, tensile breaking loads, maximum fatigue test loads, and stress-rupture test loads for parts tested as parts, not as specimens machined from parts or from coupons of the stock, shall be based upon the respective areas and stresses given in Note 1 above.

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**SATISFACTORY GRAIN FLOW
FIGURE 1A**



MINIMUM ACCEPTABLE STANDARD

Showing maximum permissible cutting of flow lines after machining to remove oxide and decarburization as in 3.2.3.

FIGURE 1B