

# AEROSPACE MATERIAL SPECIFICATIONS

## AMS 7460A

SOCIETY OF AUTOMOTIVE ENGINEERS, Inc. 485 Lexington Ave., New York 17, N.Y.

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### BOLTS AND SCREWS, TITANIUM ALLOY

6Al - 4V

Heat Treated, Roll Threaded

1. ACKNOWLEDGMENT: A vendor shall mention this specification number and its revision letter in all quotations and when acknowledging purchase orders.
2. APPLICATION: High quality bolts and screws for use up to 600 F (315 C) where a high strength lightweight fastener is required.
3. MATERIAL: Shall be AMS 4928 titanium alloy.
4. FABRICATION:
  - Ø 4.1 Blanks: Heads shall be formed by hot upsetting or by machining.
  - 4.2 Heat Treatment:
    - 4.2.1 Heating Equipment: Furnaces may be any type ensuring uniform temperature throughout the parts being heated and shall be equipped with, and operated by, automatic temperature controllers. The heating medium or atmosphere shall cause neither surface hardening nor embrittlement unless blanks are machined, after heat treatment, to remove surface hardening.
    - 4.2.2 Solution Heat Treatment: Blanks shall be heated to a temperature approximately 50 F (28 C) below the beta transus as determined on the heat of material from which Ø blanks are made, held at the selected temperature within  $\pm 15$  F ( $\pm 8.3$  C) for 30 - 60 min., and quenched in water.
    - 4.2.3 Precipitation Heat Treatment: Solution heat treated blanks shall be heated to a temperature within the range of 900 - 1100 F (482.2 - 593.3 C), held at the selected temperature within  $\pm 10$  F ( $\pm 5.6$  C) for 4 - 8 hr, and cooled in air.
  - 4.3 Contamination Removal: The solution and precipitation heat treated blanks, before rolling the threads, shall be free from all surface contamination and contamination penetration caused by prior heat treatment. The contamination removal process shall produce no intergranular attack, corrosion, or changes of structure of the blanks. The metal removed from the bearing surface of the head shall be as little as practicable to obtain a clean, smooth surface and in no case shall be greater than 0.010 inch. Ø
  - 4.4 Thread Rolling: Threads shall be formed by a single rolling process after removal of contamination as in 4.3.

Section 8.3 of the SAE Technical Board rules provides that: "All technical reports including standards approved and practices recommended, are advisory only. Their use by anyone engaged in industry or trade is entirely voluntary. There is no obligation to conform to or be guided by any technical report. In formulating and applying technical reports, the Board and its Committees will not investigate or consider patents which may apply to the subject matter. Prospective users of the report are responsible for protecting themselves against liability for infringement of patents."

## 5. TECHNICAL REQUIREMENTS:

- 5.1 Flow Lines: Flow lines of upset heads shall conform to the general arrangement shown in Fig. 1A, 1B, or 1C. The intersection of the longitudinal axis of the part and the approximate transverse axis of the flow lines shall be not less than  $D/4$  in. from the bearing surface for hexagonal, round, and square head parts and not less than  $D/6$  in. from the bearing surface for 12 point head parts where  $D$  is the nominal diameter of the shank after heading.
- 5.2 Threads:
- 5.2.1 Flow lines at threads shall be continuous, shall follow the general thread contour, and shall be of maximum density at root of thread (See Fig. 2).
- 5.2.2 Root defects such as notches, slivers, folds, roughness, or oxide scale are not permissible (See Fig. 3).
- 5.2.3 Multiple laps on the sides of threads are not permissible regardless of location. Single laps on the sides of threads that extend toward the root are not permissible (See Figs. 4 and 5).
- 5.2.4 A single lap is permissible along the side of the thread below the pitch diameter on the non-pressure side provided the lap does not originate closer than 20% of the basic thread height from the root and extends toward the crest and generally parallel to the side (See Fig. 6). A single lap is permissible along the side of the thread above the pitch diameter on either the pressure or non-pressure side (one lap per thread) provided it extends toward the crest and generally parallel to the side (See Fig. 7). Basic thread height is defined as being equivalent to 0.650 times the pitch (See Table I).
- 5.2.5 Crest craters, crest laps, or a crest lap in combination with a crest crater are permissible, provided the imperfections do not extend deeper than 20% of the basic thread height (See Table I) as measured from the thread crest when the thread major diameter is at minimum size (See Fig. 8). The major diameter of the thread shall be measured prior to sectioning. As the major diameter of the thread approaches maximum size, values for crest crater or crest lap imperfections listed in Table I may be increased by 1/2 the difference between the minimum major diameter and the actual major diameter as measured on the part.
- 5.2.6 Slight deviations from thread contour are permissible at the crest of the thread within the major diameter limits as shown in Fig. 9 and at the incomplete thread at each end of the threaded section.
- 5.2.7 Parts having holes for locking devices are permitted to have slight ovalization of the hole and the countersink and slight flattening of the crest of the thread at the countersink, provided the diameter of the hole is within specified tolerances.

- 5.2.8 Parts shall have a minimum thread run-out of one thread and a maximum of two threads. The run-out shall fair onto the shank eliminating any abrupt change in cross sectional area. Bottom and sides of threads contained in run-out shall be filleted, smooth, and devoid of abrupt tool stop marks.
- 5.2.9 All thread elements shall be within specified limits starting at a length 2 times the pitch from the end, including chamfer, and extending for the specified full thread length.
- 5.3 Straightness, Concentricity, and Squareness: For purposes of these inspections, shank and threads shall be included but shall be considered as separate elements of the part.
- 5.3.1 Straightness of Shank and Threads: Shank and threads shall be straight within the limits specified on the drawing for the total length (L) of the part under the head (See Fig. 10). Visibly abrupt changes in diameter or shape of the shank and threads which might cause stress concentrations are not permissible.
- 5.3.2 Concentricity of Thread Pitch Diameter: The concentricity of thread pitch diameter in relation to shank diameter shall be within the limits specified on the drawing for a distance of not less than 1.5 times the nominal part diameter away from the last full thread along the shank (See Fig. 11). For parts having a shank length less than 1.5 times the nominal part diameter, the concentricity of the shank diameter over its full length in relation to the thread pitch diameter shall be within the limits specified on the drawing.
- 5.3.3 Concentricity of Head: The concentricity of the head in relation to the shank diameter shall be within the limits specified on the drawing for a distance of not less than 1.5 times the nominal part diameter away from the washer face along the shank (See Fig. 12). For parts threaded to the head and for parts having shank length less than 1.5 times the nominal part diameter, concentricity of head shall be measured in relation to thread pitch diameter in lieu of shank diameter.
- 5.3.4 Squareness of Washer Face: The squareness of the washer face with the shank diameter shall be within the limits specified on the drawing for a distance of not less than 1.5 times the nominal part diameter away from the washer face along the shank (See Fig. 12). For parts threaded to the head and for parts having a shank length less than 1.5 times the nominal part diameter, squareness of washer face shall be measured in relation to thread pitch diameter in lieu of shank diameter.
- 5.4 Structure: Parts shall show microstructure free from indications of overheating resulting from heating above the beta transus without subsequent working in the alpha-beta temperature range. Slight overheating on and adjacent to the top of the head is permissible provided that the depth of overheating is not greater than 0.003 in.; measurements shall be made normal to the top of the head. A structure showing outlines of equiaxed beta grains and no primary alpha grains will be cause for rejection.
- 5.5 Surface Hardening: Parts shall have no surface hardening except as produced during rolling of threads. Determinations of surface hardening may be made by microscopic method or by a sensitive hardness testing instrument.

5.6 Properties:

5.6.1 Hardness: Shall be uniform and within the range of Rockwell C 36 - 42 or equivalent but hardness of the threaded portion may be higher as a result of the thread rolling.

5.6.2 Room Temperature Notched Stress-Rupture Test: Parts shall be capable of meeting the following requirement:

5.6.2.1 A part, maintained at room temperature while the axial load specified in Table II is applied continuously, shall not rupture in less than 5 hours. The initial load may be less than that specified in Table II and increased in the increments specified in Table II at intervals of not less than 5 hours.

5.6.2.1.1 If the size or shape of the part is such that the part cannot be tested satisfactorily, a test may be made on a specimen machined from the stock to the dimensions given in AMS 4928 and heat treated in the same manner as the parts. Such specimens shall withstand an axial stress of 170,000 psi applied continuously for not less than 5 hours. The initial stress may be less than 170,000 psi and increased to 170,000 psi in increments of 10,000 psi at intervals of not less than 5 hours.

6. QUALITY: Parts shall be uniform in quality and condition, clean, sound, smooth, and free from burrs and foreign materials and from internal and external imperfections detrimental to their performance.

6.1 Parts subject to fluorescent penetrant inspection shall conform to the following standards.

6.1.1 Discontinuities transverse to grainflow, such as pipes, grinding checks, and quench cracks, shall be cause for rejection.

6.1.2 Longitudinal indications of surface seams and forming laps parallel to grainflow are acceptable within the following limits, provided the separation between indications is not less than 1/16 in. in all directions.

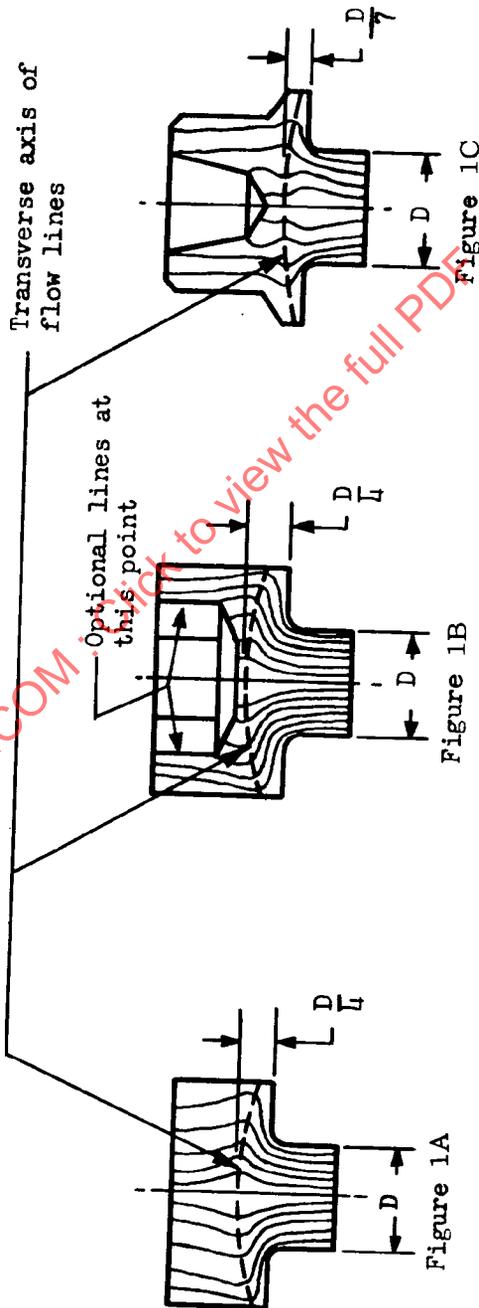
6.1.2.1 Sides of Head: A maximum of 3 surface indications per head is permitted and the length of each indication may be the full height of the surface. No indication shall break over either edge to a depth greater than 1/32 in. or the equivalent of the basic thread height (See Table I), whichever is less.

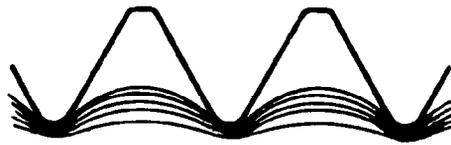
6.1.2.2 Top of Head and End of Stem: A maximum of 3 surface indications in each area is permitted provided the length or diameter of any individual indication does not exceed 1/32 in. or the equivalent of the basic thread height (See Table I), whichever is less.

6.1.2.3 Shank or Stem: A maximum of 5 indications is permitted. The length of any one indication may be the full length of the surface but the total length of all indications shall not exceed twice the length of the surface. No indication shall break into a fillet or over an edge.

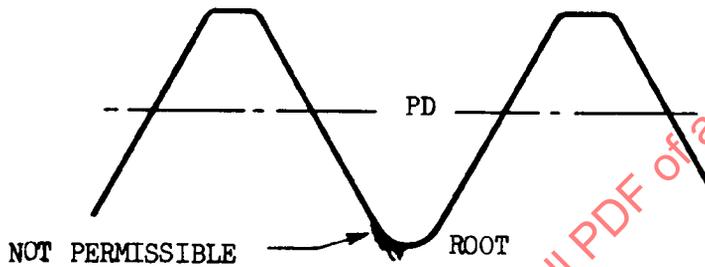
6.1.2.4 **Threads:** There shall be no indications of cracks, seams, pipes, or rolling laps in threads as shown by Figs. 3, 4, and 5 except that indications of slight laps as shown by Figs. 6, 7, and 8 will be permitted.

7. **REJECTIONS:** Parts not conforming to this specification or to authorized modifications will be subject to rejection.

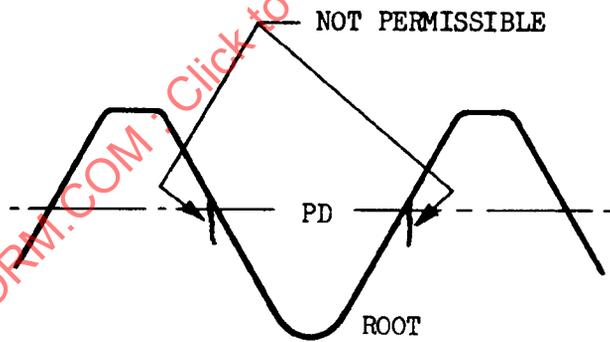




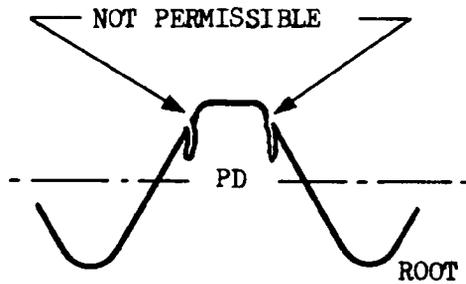
FLOW LINES - ROLLED THREAD  
Figure 2



ROLLED THREAD  
Figure 3

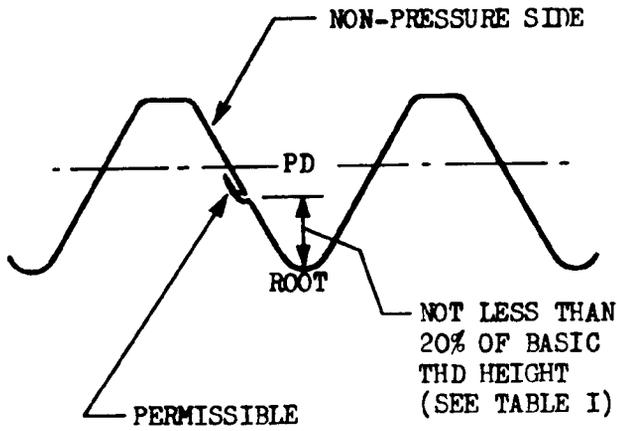


ROLLED THREAD  
Figure 4

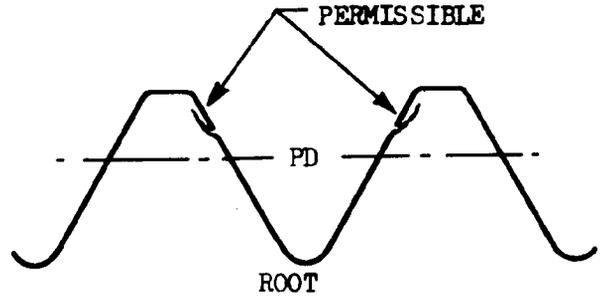


ROLLED THREAD  
Figure 5

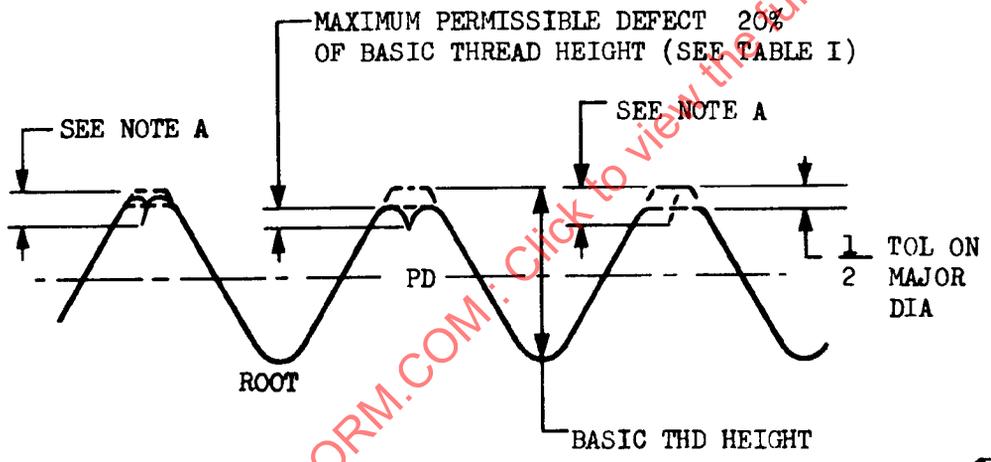
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ROLLED THREAD  
Figure 6

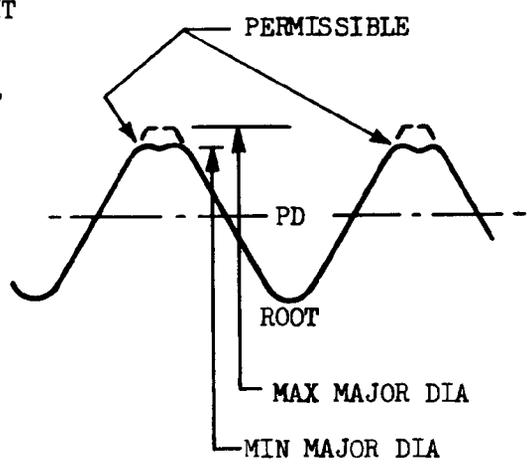


ROLLED THREAD  
Figure 7



NOTE A. DEPTH OF DEFECT EQUALS 20% OF BASIC THREAD HEIGHT PLUS 1/2 THE DIFFERENCE OF THE ACTUAL MAJOR DIAMETER AND MINIMUM MAJOR DIAMETER.

ROLLED THREAD  
Figure 8



ROLLED THREAD  
Figure 9

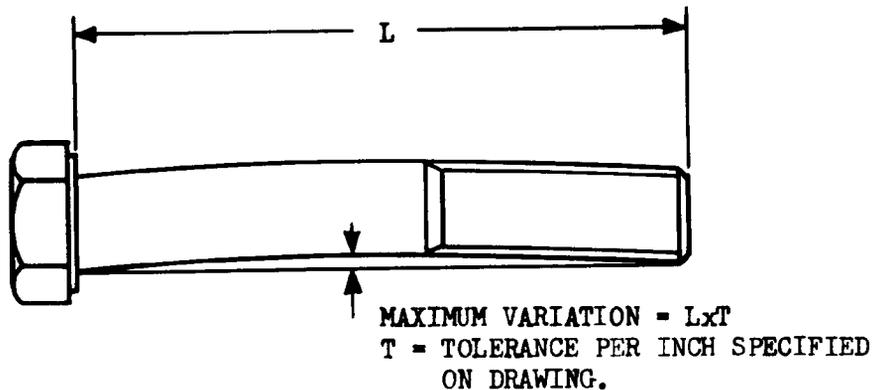


Figure 10

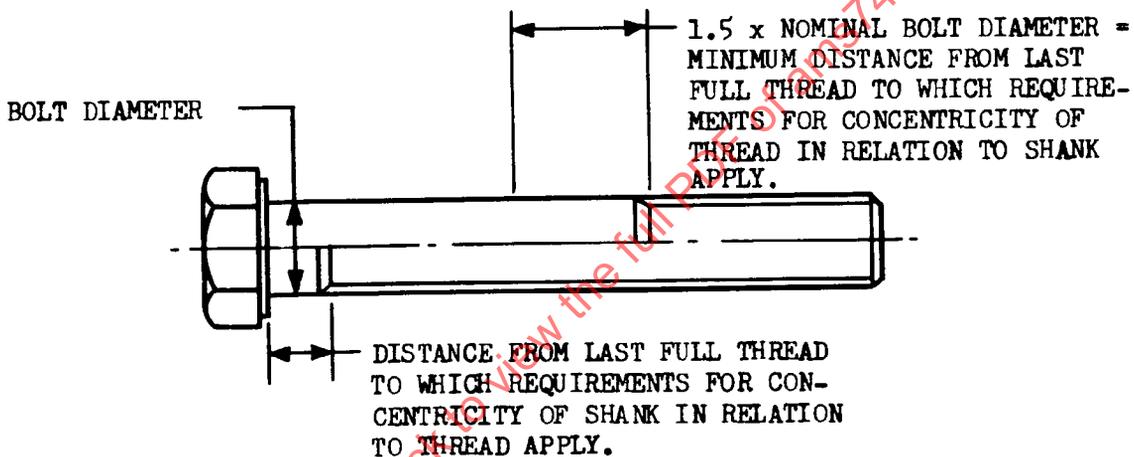


Figure 11

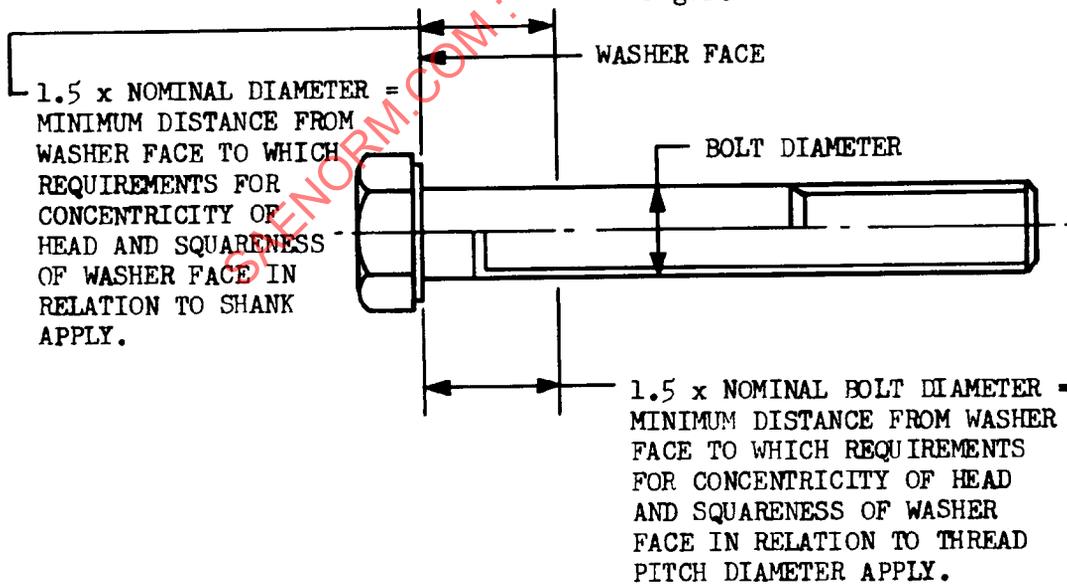


Figure 12