
**Guidelines for specifying Charpy
V-notch impact prescriptions in steel
specifications**

*Lignes directrices pour la spécification des prescriptions d'énergie de
rupture sur éprouvette Charpy à entaille en V dans les normes d'acier*

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Foreword

ISO (the International Organization for Standardization) is a worldwide federation of national standards bodies (ISO member bodies). The work of preparing International Standards is normally carried out through ISO technical committees. Each member body interested in a subject for which a technical committee has been established has the right to be represented on that committee. International organizations, governmental and non-governmental, in liaison with ISO, also take part in the work. ISO collaborates closely with the International Electrotechnical Commission (IEC) on all matters of electrotechnical standardization.

The procedures used to develop this document and those intended for its further maintenance are described in the ISO/IEC Directives, Part 1. In particular the different approval criteria needed for the different types of ISO documents should be noted. This document was drafted in accordance with the editorial rules of the ISO/IEC Directives, Part 2 (see www.iso.org/directives).

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For an explanation on the voluntary nature of standards, the meaning of ISO specific terms and expressions related to conformity assessment, as well as information about ISO's adherence to the World Trade Organization (WTO) principles in the Technical Barriers to Trade (TBT) see the following URL: www.iso.org/iso/foreword.html.

This document was prepared by Technical Committee ISO/TC 17, *Steel*, Subcommittee SC 20, *General technical delivery conditions, sampling and mechanical testing methods*.

This first edition of ISO/TS 7705 cancels and replaces ISO/TR 7705:1991, which has been technically revised.

Guidelines for specifying Charpy V-notch impact prescriptions in steel specifications

1 Scope

This document gives guidelines for specifying Charpy V-notch impact prescriptions in steel specifications.

2 Normative references

There are no normative references in this document.

3 Terms and definitions

No terms and definitions are listed in this document.

ISO and IEC maintain terminological databases for use in standardization at the following addresses:

- ISO Online browsing platform: available at <http://www.iso.org/obp>
- IEC Electropedia: available at <http://www.electropedia.org/>

4 General features of Charpy V-notch impact test

4.1 Toughness testing methods in design codes and in steel specifications

Tests for evaluating the toughness of steel can be divided into two categories: notch toughness tests and fracture toughness tests based on fracture mechanics.

Notch toughness tests are used to measure the ability of a material to absorb energy and deform plastically in the presence of a mechanical notch. The Charpy V-notch impact test and the drop weight test are typical examples of small scale tests which are used for evaluations of notch toughness. They are often used to determine the ductile to brittle transition temperature of a material and to give a qualitative estimate of the material's toughness. Due to relatively good reproducibility and low cost these methods are highly suitable for use as delivery tests for steel consignments.

Fracture toughness tests such as the crack-tip opening displacement (CTOD) test (see ISO 12135) are fracture mechanics tests which are generally concerned with the determination of critical crack sizes which can appear without causing fracture in a material loaded to a specific stress level. Fracture mechanics tests are very complicated and expensive to carry out. They are primarily used to examine the behaviour of pressurized or structural components with respect to safety rules, etc. Therefore, fracture mechanics testing is primarily connected with design codes and not with steel specifications.

For these reasons, only notch toughness tests are dealt with in these guidelines for steel specifications.

4.2 Historical background to the Charpy V-notch impact test

When welded structures, especially heavy ones such as bridges and ships, were first developed on an industrial scale, and especially when the fabrication methods called for joining heavy segments by welding, problems with brittle fractures became more common. This was especially evident during the Second World War when the USA began to produce welded ships of the Liberty and Victory type, where a large number of failures occurred due to brittle fractures.

An empirical relationship based on many tests was found between the Charpy V-notch impact energy and service fractures. The work initiated by the USA was continued by the International Institute of Welding (IIW) who provide recommendations and a classification system for steels according to their susceptibility to brittle fracture after welding.

Originally the USA required an impact energy value of 15 footpounds (ft lb) for a standard 10 mm x 10 mm V-notch impact test piece. This was later increased to 20 ft lb. The IIW converted these figures into metric units and referred the impact energy value to the cross-section under the notch, which gave a figure of 3,5 kg m/cm² corresponding to 20 ft lb. Later the units were transformed into SI units. This gave the value of 27 J (20 ft lb).

In 1953 Pellini compared the Charpy V-notch impact test with an explosion crack starter test intended to simulate the service performance of higher quality steels. Pellini recommended impact energy of 20 ft lb (27 J) instead of the earlier used 15 ft lb.

Wells also simulated service conditions at the starting point of a brittle fracture crack by using a wide plate test. The intention of this test, which could not be used as an acceptance test for a steel consignment, was to include in a big plate specimen the stresses existing in a weld, the influence of plate thickness, the type of defect, etc. The results of wide plate tests were also compared with Charpy V-notch impact values.

Today 27 J is generally used for unalloyed steels. In some cases, for instance for fine grain steels or quenched and tempered steel grades, this level can be 27 J or alternatively fixed to a higher level (40 J) according to the requirements for specific steels and intended applications. Impact test requirements are included in the product standard.

4.3 The Charpy V-notch impact test in relation to other tests

Originally the Charpy impact test was performed with a "keyhole" or U-notch test bar. Its purpose was to check that the material was sound as to cleanliness, rolling and heat treatment. In the 1950s interest was concentrated on the risk of brittle fracture in welded structures and the V-notch test bar was introduced as the V-notch test indicates transition behaviour more clearly than the U-notch test.

In addition to the Charpy impact test other impact test methods (e.g. Mesnager, Izod, Schnadt) have also been used.

The drop weight test is a material test which is intended to measure the highest temperature at which steel exhibits brittle fracture. This test can be an alternative or can be required in addition to the Charpy V-notch impact test.

4.4 Factors influencing impact properties

The behaviour of a steel structure subject to impact is not only dependent on the material. It is also dependent on the following:

- material thickness;
- stress state;
- temperature;
- steel type;
- loading rate;
- surface conditions;
- residual stresses;
- yield strength.

In addition, the Charpy V-notch test result is influenced by the following:

- orientation of test piece;
- orientation of notch;
- sharpness of notch;
- specimen position in the product;
- steel type;
- type of impact machine striker.

For these and other reasons the impact energies or transition temperatures determined under the well-defined conditions of an impact test cannot, without any further considerations, be regarded as determinant with respect to temperature and/or thickness for the application of the material.

4.5 The Charpy V-notch impact test as a powerful tool for delivery control in steel specifications

The Charpy V-notch impact test can be used as a means of expressing, in a specification, the susceptibility of a steel to brittle fracture. It is an inexpensive and easily reproducible test method which is empirically related to the susceptibility to brittle fracture and therefore to the weldability of a steel.

Impact test requirements are included in many ISO steel specifications.

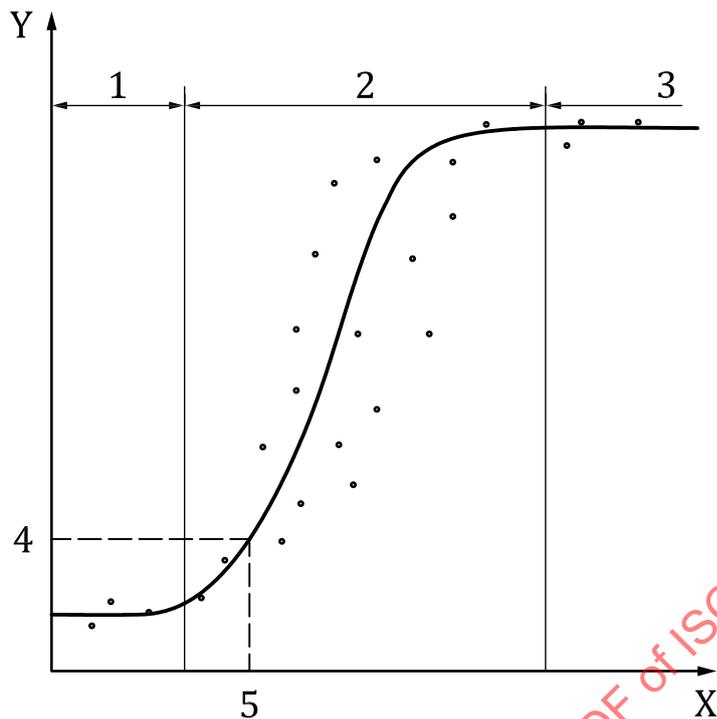
For specimen and notch orientation consult the relevant product standard.

5 Information to be gained from the impact test

Independent of the size of the test piece, the thickness of the material and the type of notch, the impact test carried out for a specified steel of given thickness at different temperatures gives a curve of absorbed energy versus temperature (see [Figure 1](#)). This curve can be separated into three parts: one part at higher temperatures and higher energies (upper shelf); one part at lower temperatures and lower energies (lower shelf); and a transition range in between. The scatter of results on the upper and lower shelves is relatively small but the scatter in the transition part of the curve is relatively large. Because of this scatter, the requirement of testing three test pieces and calculating their mean value was chosen.

Austenitic stainless steels are also ductile at very low temperatures, and consequently the impact curve does not show a transition range even at very low temperatures (see [Figure 2](#)).

Since the test result depends upon the geometry of the test piece, the thickness, etc., the test is carried out on a standardized test bar and it is irrelevant to refer the impact energy to a cross-sectional area. The energy level should therefore be given in Joules only.



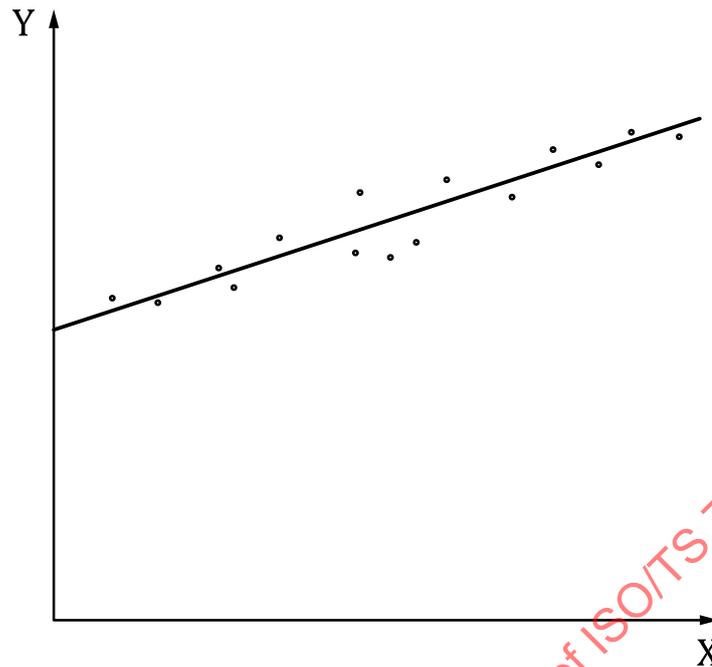
Key

X test temperature, in °C
 Y absorbed energy, in J

- 1 lower shelf
- 2 transition range
- 3 upper shelf
- 4 specified energy
- 5 specified temperature

Figure 1 — Example of an impact test curve

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**Key**

- X test temperature, in °C
Y absorbed energy, in J

Figure 2 — Example of an impact test curve for material without transition range

The impact test is prescribed in material specifications for the following two reasons.

- To determine indirectly whether the cleanliness, manufacturing process and heat treatment, etc. have been appropriately controlled.
- To classify a steel according to its susceptibility to brittle fracture.

In this case the result of interest is whether the test result reaches the upper or the lower shelf of the curve and, especially, where the transition range is located on the temperature scale. If the test result corresponds to the upper part of the curve, the conclusion can be drawn that the toughness of the material is considerably better than if the result corresponds to the lower part of the curve. Furthermore, if the transition range of the curve for one steel occurs at a considerably lower temperature than that for another steel, impact test results for the first steel will lie on the upper part of the curve down to lower temperatures than for the other steel and hence the conclusion can be drawn that the first steel has a higher toughness and is more suitable for constructions that are fabricated and/or used at lower temperatures.

The most important information obtained is therefore the temperature range where the change from ductile to brittle fracture occurs, i.e. the transition temperature. There are several methods for determining the transition temperature depending on the material and on the intended use (level of energy or defining the inflexion point of the transition curve or based upon the percentage of brittle zone on the fracture surface).

Other information from the test can also be of importance, such as the fracture appearance and lateral expansion measured after fracture.

It should be observed that as the impact energy is not a material property, a high value only indicates a tougher material, when the comparison is made with the same material having the same thickness and the test is carried out with the same size of test pieces at the same temperature.

6 Subsize test pieces

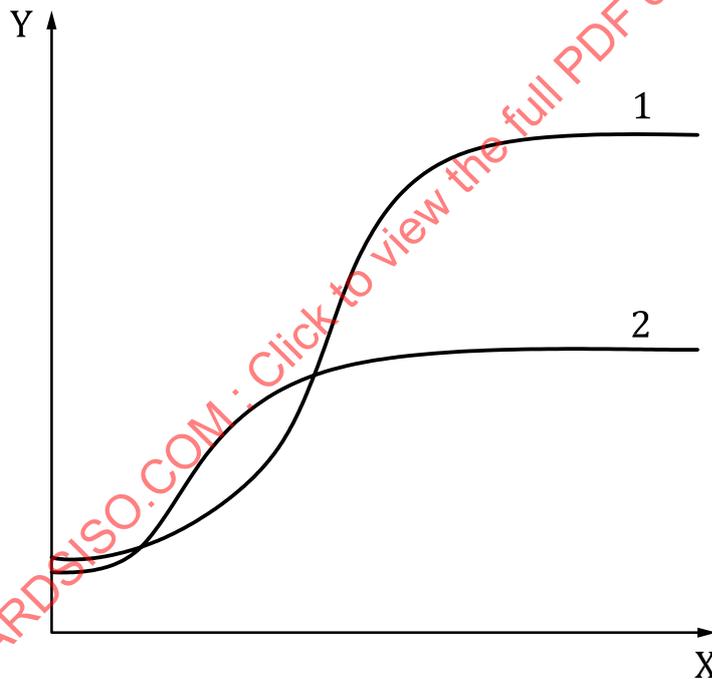
The standard V-notch test piece has a cross-section of 10 mm x 10 mm.

As the test pieces are machined to a good surface finish, it is not possible to take 10 mm x 10 mm test pieces from plates, strip and sections ≤ 12 mm or from round bars with a diameter of less than 16 mm. Especially for plates, customers often require impact tests on material with thickness < 12 mm and therefore three subsize V-notch test pieces have been standardized: 10 mm x 2,5 mm, 10 mm x 5 mm and 10 mm x 7,5 mm. When test pieces with reduced width are used, the largest obtainable width should be taken.

When testing a material with subsize test pieces (see [Figure 3](#)), it should be noted that

- a) the transition range moves to lower temperatures compared with the 10 mm x 10 mm test pieces, i.e. subsize test pieces will show inherently more ductile behaviour, and
- b) the upper energy level is reduced compared to the 10 mm x 10 mm test piece.

Furthermore, there is no simple mathematical connection between the test results obtained from 10 mm x 10 mm test pieces and those from subsize test pieces. Therefore, rules to reduce the impact values for subsize test pieces in relation to the values for 10 mm x 10 mm test pieces are empirical, and scientifically doubtful, but are accepted for practical reasons.



Key

- | | | | |
|---|-------------------------|---|--------------------------|
| X | test temperature, in °C | 1 | test piece 10 mm x 10 mm |
| Y | absorbed energy, in J | 2 | test piece 5 mm x 10 mm |

Figure 3 — Example of an impact test curve for a material with subsize test pieces

The following points should, however, be observed.

- c) The difference between a correct reduced impact energy and an energy related to the reduction in thickness is very small in comparison to the normal scatter. In the case of the 7,5 mm thick test piece the 75 % value becomes 80 % which means, referred to a minimum value of 27 J for the normal test piece, a difference of 1,4 J.

- d) Except for the temperature range at a high energy level, no simple formula for the dependency of the impact energy from the test piece thickness exists for the transition range. This means that the calculation of the minimum energy values for the subsize test pieces as a proportional function of the test piece thickness is a simplification.
- e) With decreasing product thickness, the danger of brittle fracture decreases under otherwise comparable conditions, so that the calculation with 75 % and 50 %, instead of for example 80 % and 60 %, will not be critical.

For material thickness where the standardized test piece of 10 mm x 10 mm cannot be used, i.e. plates \leq 12 mm and round bars with a diameter of less than 16 mm, the following rules should apply.

- f) The standardized subsize test pieces of 10 mm x 7,5 mm and 10 mm x 5 mm should be used wherever possible. The test piece should be of the maximum standard size that can be obtained consistent with removing the scale from the surface.
- g) Minimum values included in steel specifications should refer to tests with the standardized test piece of 10 mm x 10 mm.
- h) Plates and tubes with thicknesses of 5 mm to 10 mm should be referred to the relevant product standard.
- i) For practical reasons minimum impact values in steel specifications for standardized subsize test pieces should be 75 % of the full-size test piece value for the 10 mm x 7,5 mm test piece and 50 % of the full-size piece value for the 10 mm x 5 mm test piece.

7 Recommendations for specifying impact strength requirements in steel specifications

7.1 Selection and preparation of samples and test pieces

7.1.1 Selection and preparation of samples

Apart from machining, the sample should not undergo any processing and treatment, unless specified by the product standard.

7.1.2 Cutting and machining

Cutting should be carried out cold with precautions taken to avoid superficial work hardening and overheating of the steel which could change the mechanical characteristics.

After machining, any marks left by the tool which might interfere with the results of the test should be removed, either by grinding (with ample coolant supply) or by polishing, provided that the chosen method of finishing maintains the dimensions and shape of the test piece within the tolerances stipulated in the standard for the test.

The tolerances of the dimensions of the test pieces should be as stipulated in the appropriate standards for the test methods.

7.2 Number of test pieces to be taken per sample and specific requirements

The average value of three test pieces should meet the specified requirement. Unless otherwise specified by the product standard, one individual value may be below the specified value, provided that it is not less than 70 % of that value.

7.3 Location of test pieces

Impact test pieces should be located in steel products according to ISO 377.