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**Acoustics — Description,  
measurement and assessment of  
environmental noise —**

**Part 3:  
Objective method for the  
measurement of prominence of  
impulsive sounds and for adjustment  
of  $L_{Aeq}$**

*Acoustique — Description, mesurage et évaluation du bruit de  
l'environnement —*

*Partie 3: Méthode objective pour le mesurage de l'émergence des  
bruits impulsifs et pour l'ajustement du  $L_{Aeq}$*

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## Foreword

ISO (the International Organization for Standardization) is a worldwide federation of national standards bodies (ISO member bodies). The work of preparing International Standards is normally carried out through ISO technical committees. Each member body interested in a subject for which a technical committee has been established has the right to be represented on that committee. International organizations, governmental and non-governmental, in liaison with ISO, also take part in the work. ISO collaborates closely with the International Electrotechnical Commission (IEC) on all matters of electrotechnical standardization.

The procedures used to develop this document and those intended for its further maintenance are described in the ISO/IEC Directives, Part 1. In particular, the different approval criteria needed for the different types of ISO documents should be noted. This document was drafted in accordance with the editorial rules of the ISO/IEC Directives, Part 2 (see [www.iso.org/directives](http://www.iso.org/directives)).

Attention is drawn to the possibility that some of the elements of this document may be the subject of patent rights. ISO shall not be held responsible for identifying any or all such patent rights. Details of any patent rights identified during the development of the document will be in the Introduction and/or on the ISO list of patent declarations received (see [www.iso.org/patents](http://www.iso.org/patents)).

Any trade name used in this document is information given for the convenience of users and does not constitute an endorsement.

For an explanation of the voluntary nature of standards, the meaning of ISO specific terms and expressions related to conformity assessment, as well as information about ISO's adherence to the World Trade Organization (WTO) principles in the Technical Barriers to Trade (TBT), see [www.iso.org/iso/foreword.html](http://www.iso.org/iso/foreword.html).

This document was prepared by Technical Committee ISO/TC 43, *Acoustics*, Subcommittee SC 1, *Noise*.

A list of all parts in the ISO 1996 series can be found on the ISO website.

Any feedback or questions on this document should be directed to the user's national standards body. A complete listing of these bodies can be found at [www.iso.org/members.html](http://www.iso.org/members.html).

## Introduction

Noise with prominent impulsive sound is more annoying than continuous types of noise (without impulses or tones) with the same equivalent sound pressure level. Therefore, an adjustment is commonly added to the measured  $L_{Aeq}$  if prominent impulsive sound is present.

In ISO 1996, three categories of impulsive sound have been found to correlate best with community response, and adjustments are given for each. Sources of impulsive sound are listed for each category. However, the list is not exhaustive.

This method objectively categorises sources by determining the prominence of impulsive sound at the receiver point, with the aim of correlating to human response. The resulting adjustments can be used to categorise the sources or be applied directly. It describes specific methodology for this purpose and provides guidance to cognizant authorities for categorising sources and their adjustments. It is intended to complement the ISO 1996-2 measurement method for general purpose environmental noise assessment.

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# Acoustics — Description, measurement and assessment of environmental noise —

## Part 3:

# Objective method for the measurement of prominence of impulsive sounds and for adjustment of $L_{Aeq}$

## 1 Scope

This method objectively categorises sources by determination of the prominence of impulsive sound, with the aim of correlating to community response. This method for measuring the prominence of impulsive sounds is intended for sources not identified as gunfire or high-energy impulsive sound. It typically produces adjustments in the range 0,0 dB to 9,0 dB. These adjustments are intended to be used to categorise the sources as either regular impulsive or highly impulsive sound sources and apply the penalty indicated in ISO 1996-1. However, the adjustments may be applied directly, as is done in NT ACOU 112<sup>[2]</sup>, and BS 4142<sup>[3]</sup>. ISO 1996-2 provides additional guidance for performing these measurements.

The method is intended for use on sources with impulsive characteristics that are not already categorised in ISO 1996-1. A non-exhaustive list of examples includes compressed air release, scrap handling, goods delivery, fork lifts with rattling forks, skateboard ramps, industrial shearing, gas discharges, percussive tools in demolition, powered riveting, etc.

The method is not intended for use on sounds from firearms. Although the measurements of prominence may give relevant results, research has shown the response to these sources is influenced by factors outside of the scope of this document. In addition, the method is not intended to use for high-energy impulsive sound sources as specified in ISO 1996-1.

NOTE This method is not intended for occupational hearing loss, which is outside the scope of this document.

See [Annex A](#) for recommended additional research.

## 2 Normative references

The following documents are referred to in the text in such a way that some or all of their content constitutes requirements of this document. For dated references, only the edition cited applies. For undated references, the latest edition of the referenced document (including any amendments) applies.

ISO 1996-1, *Acoustics — Description, measurement and assessment of environmental noise — Part 1: Basic quantities and assessment procedures*

IEC 61672-1, *Electroacoustics — Sound level meters — Part 1: Specifications*

## 3 Terms and definitions

For the purposes of this document, the following terms and definitions apply.

ISO and IEC maintain terminology databases for use in standardization at the following addresses:

- ISO Online browsing platform: available at <https://www.iso.org/obp>
- IEC Electropedia: available at <https://www.electropedia.org/>

**3.1**  
**sound pressure level**

$L_{pAF}$   
A frequency-weighted and F time-weighted sound pressure level

Note 1 to entry: The sound pressure level is as defined in ISO 1996-1.

**3.2**  
**impulsive sound**  
sound with a sudden onset

Note 1 to entry: The definition includes only the onset of a sound, not the sound as a whole. "Sudden" is based on an auditive judgement, which is expressed in terms of physical measurements in this method.

Note 2 to entry: The perceived characteristics and prominence of an impulsive sound at the immission point depends on the character of the emitted sound, the distance and propagation path from the sound source and the residual sound. Therefore, the onset parameters characterize the impulse independent of the category of the sound source.

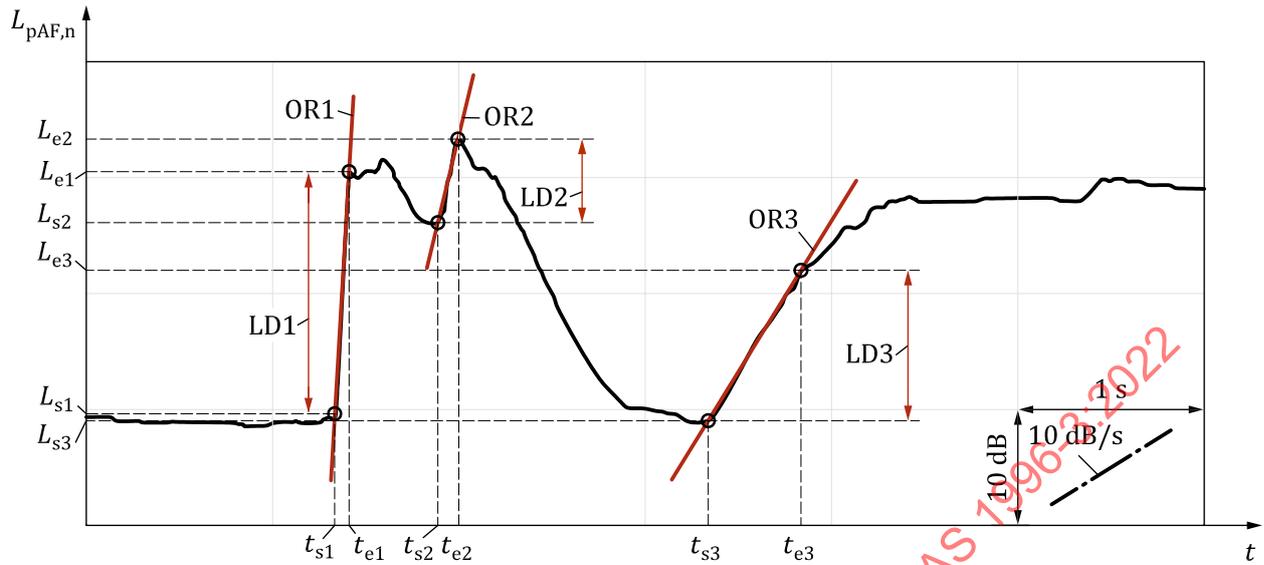
**3.3**  
**onset**  
contiguous part of the positive slope of the time history of  $L_{pAF}$  where the gradient exceeds 10 dB/s

Note 1 to entry: The starting point of an onset is the point where the gradient first exceeds 10 dB/s. The end point of an onset is the first point after the starting point where the gradient decreases to less than 10 dB/s. Irregularities (on the onset) shorter than 50 ms are excluded.

**3.4**  
**level difference**  
**LD**  
difference in decibels of  $L_{pAF}$  between the level of the end point  $L_e$  and the level of the starting point  $L_s$  of the onset (3.3)

**3.5**  
**onset rate**  
**OR**  
slope in decibels per second of the straight line that gives the best approximation to the onset (3.3) between the starting point and the end point

Note 1 to entry: For pass-bys of, e.g. road vehicles, trains or aircraft the onset rates shall be found from the level range  $L_e - (L_e - L_s)/2$  to  $L_e$ , i.e. over the upper half of the slope, see [Figure 1](#) illustrating the onset rate (OR) and the level difference (LD) based on the time history of the A frequency-weighted and F time-weighted sound pressure levels.



### Key

- LD level difference, in decibels
- $L_s$  level at the starting point, in decibels
- $L_e$  level at the end point, in decibels
- OR onset rate, in decibels per second
- $t_s$  starting point, in seconds
- $t_e$  end point, in seconds

NOTE Gradients of 10 dB/s or more are indicated with short line segments.

**Figure 1 — Analysis of the time history of the A frequency-weighted and F time-weighted sound pressure levels**

### 3.6

#### assessment time interval

time interval in which any adjustment is applied

Note 1 to entry: This is typically different than the reference time interval, the measurement time interval and the observation time interval.

## 4 Measurements

Measurements shall be made with instruments conforming with Class 1 as specified in IEC 61672-1 with the additional logging of  $L_{pAF}$ , the A frequency-weighted and F time-weighted sound pressure level, at the intervals identified below.

The A frequency-weighted and F time-weighted sound pressure level shall be sampled with time intervals in the range 10-25 ms (incl.). Alternatively, measurements made on the basis of short-term  $L_{Aeq}$  values (e.g. 10 ms) may be used and, if so, shall (e.g. by computation) be approximated to time weighting F before the readings are taken.

NOTE 1 Direct measurements of  $L_{pAF}$  are preferred to those based on short-term  $L_{Aeq}$  values.

NOTE 2 Measurements based on a series of short-term  $L_{Aeq}$  values can be converted to a series of  $L_{pAF}$  values by the following [Formula \(1\)](#):

$$L_{pAF,n} = 10 \cdot \lg \left[ \left[ \left( \frac{\tau}{\Delta t} - 1 \right) \cdot 10^{\frac{L_{pAF,n-1}}{10}} + 10^{\frac{L_{Aeq,n}}{10}} \right] / \left( \frac{\tau}{\Delta t} \right) \right] \text{ dB} \quad (1)$$

where

$L_{Aeq,n}$   $n$ 'th short-term  $L_{Aeq}$  value, in decibels;

$L_{pAF,n}$  A frequency-weighted and F time-weighted sound pressure level at the time of the  $n$ 'th  $L_{Aeq}$  value,  $L_{Aeq,n}$ ;  $L_{pAF,0} = L_{Aeq,0}$ , in decibels;

$\tau$  time constant for the time weighting, in ms. For F:  $\tau = 125$  ms;

$\Delta t$  time between the  $L_{Aeq}$  values (and the integration time), in ms.

Measurements based on samples with time intervals of 100 ms may be used for surveys and screening, as many modern sound level meters can do this while recording the audio in sufficient detail for later analysis. Using this method, a higher uncertainty is associated to the results.

NOTE 3 Using time intervals of 100 ms means that it is not possible to observe two impulsive sound events occurring within 50 ms.

The measurement is to be made where possible at such times that impulses from sources of residual sound are not present as these can impact the assessment of the source of specific sound under investigation. Where not possible, the influence of the sources of residual sound on the measurement is to be reported. When unattended measurements are used, ancillary data such as audio recording or other methods of source identification are recommended. It is recommended that impulses that are suspected of being caused by sources of residual sound are excluded from analysis.

From a successive series of A frequency-weighted and F time-weighted sound pressure levels,  $L_{pAF,n}$ , the starting point  $s$  and the end point  $e$  of an onset are defined from the procedures a) to d). The symbols used are defined below. Points a) to c) refer to [Figure 1](#). Point d) refers to [Figure 2](#).

- a) The starting point,  $s_1$ , is the first point where the slope is larger than 10 dB/s:  

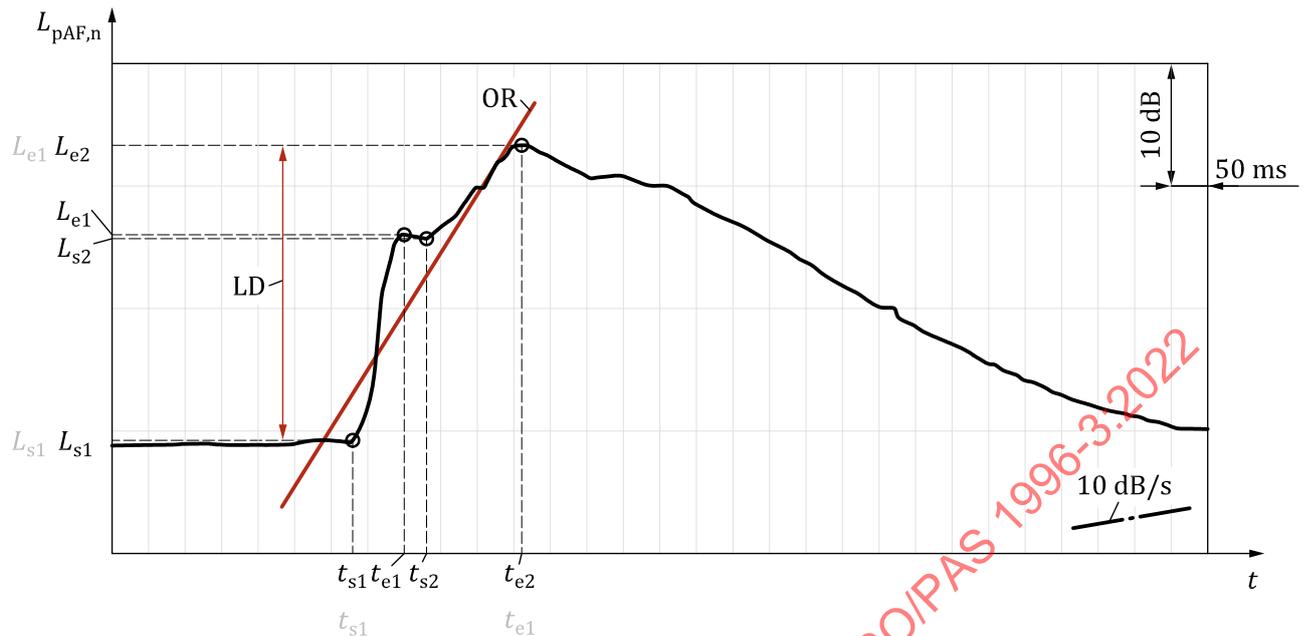
$$\frac{(L_{s_{1+1}} - L_{s_1})}{(t_{s_{1+1}} - t_{s_1})} > 10 \text{ dB/s}.$$
- b) The end point,  $e_1$ , is the first point after the starting point where the slope is less than 10 dB/s:  

$$\frac{(L_{e_{1+1}} - L_{e_1})}{(t_{e_{1+1}} - t_{e_1})} < 10 \text{ dB/s}.$$
- c) A new starting point,  $s_2$ , in [Figure 1](#), occurs when condition a) is met again.
- d) If a new starting point,  $s_2$ , occurs within a period of 50 ms after the end point,  $e_1$ , see [Figure 2](#), then end point,  $e_1$ , and starting point,  $s_2$ , become unnamed intermediate points if the following conditions are met:

$$\frac{(L_{e_2} - L_{e_1})}{(t_{e_2} - t_{e_1})} > 10 \text{ dB/s} \text{ and } \frac{(L_{s_2} - L_{s_1})}{(t_{s_2} - t_{s_1})} > 10 \text{ dB/s}$$

$e_2$  is the end point after the new starting point,  $s_2$ . If point,  $e_1$  and  $s_2$ , become unnamed, point  $e_2$  takes over the name  $e_1$  (illustrated in grey in [Figure 2](#)).

$s_{1+1}$  denotes the point one sample after point  $s_1$ .  $L_{s_1}$  is the level of point  $s_1$ , and  $t_{s_1}$  is the time of sampling;  $L_{e_1}$  is the level of point  $e_1$ , and  $t_{e_1}$  is the time of sampling, and so on.

**Key**

LD level difference, in decibels

 $L_s$  level at the starting point, in decibels $L_e$  level at the end point, in decibels

OR onset rate, in decibels per second

 $t_s$  starting point, in seconds $t_e$  end point, in seconds

NOTE The red line is the least squares fit.

**Figure 2 — Analysis example of two impulsive sound events observed within 50 ms**

For each onset,  $n$ , the level difference is  $L_{en} - L_{sn}$ , and the onset rate is found from the “least-squares method” (linear regression analysis) of the points from  $s_n$  to  $e_n$  (inclusive and also including any now unnamed points from step d).

NOTE 4 In some measuring systems, the onset rate can be determined from the  $F$  time-weighted samples as  $60/T$ , where  $T$  is the reverberation time measured directly on the onset of the sound. Other systems can require that the sound samples are reversed before such a measurement can be performed.

**5 Prominence,  $P$** 

In assessment time intervals, a number of impulses with the apparently highest onset rates and level differences shall be selected. The default assessment time interval is 30 min. For each selected impulse the prominence,  $P$ , is calculated from [Formula \(2\)](#):

$$P = 3 \lg \left[ \frac{r}{(\text{dB/s})} \right] + 2 \lg \left( \frac{d}{\text{dB}} \right) \quad (2)$$

where

$r$  is the onset rate (OR) as defined in [3.4](#), expressed in dB/s;

$d$  is the level difference (LD) as defined in [3.5](#), expressed in dB.

The impulse with the highest value of  $P$  gives the final result.

NOTE The general form of the expression for  $P$  is:  $P = k_1 \cdot \lg(\text{onset rate}) + k_2 \cdot \lg(\text{level difference})$ . The constants  $k_1$  and  $k_2$  have been estimated from the results of listening tests. It is also taken into account that the relation between  $P$  for very sudden and loud impulses and  $P$  for slow level changes is large.  $P$  was furthermore designed to give a maximum around 15. With the constants given in [Formula \(2\)](#) the prominence explains 73 % of the variance in the answers from the listening test mentioned in Reference [\[4\]](#).

## 6 Identification of adjustment to $L_{Aeq}$

For sounds with onset rates larger than 10 dB/s, the adjustment  $K_I$ , based on the prominence  $P$ , is calculated as given by the following [Formula \(3\)](#):

$$K_I = 1,8 \cdot (P - 5) \text{ dB, for } P > 5$$

$$K_I = 0 \text{ dB, for } P \leq 5 \tag{3}$$

where

$K_I$  is the adjustment, expressed in dB;

$P$  is the prominence, in dB.

During an assessment time interval of 30 min, the adjustment for the one event with the highest value of  $P$  occurring during this time is assessed. For reference time intervals of less than 30 min, the assessment time interval should be aligned with this reference time interval and reported. The rating level for a reference time interval is determined as the energy-average of the rating level of each assessment time interval.

NOTE 1 According to this proposal the rating level  $L_{Ar,T}$  over the reference time interval,  $T$ , related to the impulsive sound is found from:

$$L_{Ar,T} = 10 \lg \left( \frac{1}{T} \sum_N \Delta t_N 10^{\frac{L_{Aeq,N} + K_{I,N}}{10}} \right)$$

where

$T$  duration of the reference time interval, in minutes;

$\Delta t_N$  duration of each assessment time interval, in minutes, nominally 30 min;

$L_{Aeq,N}$  equivalent noise level of the assessment time interval  $\Delta t_N$ , in decibels;

$K_{I,N}$  adjustment to  $L_{Aeq,N}$ , in decibels.

The assessment time interval of 30 min for adjustment of  $L_{Aeq}$  is a preliminary choice based on considerations of reasonableness and ease of measurement and administration. There are no systematic investigations behind this choice of assessment time interval, and the principle should be considered in more detail when investigations of the relevant assessment time interval are made. The assessment time interval for the adjustment of  $L_{Aeq}$  should be less than or equal to the reference time interval, and it may be advantageous to make the assessment time interval a divisor of the reference time interval – for example, using a 5 min assessment time interval for a reference time interval of 30 min.

NOTE 2 The longer the assessment time interval, the greater the impact that energy-averaging has on the adjustment for the reference time interval.

## 7 Categorisation of impulsive sound

Sounds with adjustment  $K_1 = 0$  at the receiver location are not impulsive.

For sounds with adjustment  $0 < K_1 \leq 5$  at the receiver location, categorise these as regular impulsive.

For sounds with adjustment  $K_1 > 5$  at the receiver location, categorise these as highly impulsive.

Either apply the adjustment to the rating level, based on the categorisation of the source, as indicated in ISO 1996-1, or apply the adjustment  $K_1$  directly to the rating level.

## 8 Accuracy

The information about the measurements shall be given in terms of sound pressure levels, although the method for determination of the adjustment,  $K$ , is not sensitive to the absolute calibration of the measuring equipment.

The working conditions of the source may affect impulsive sound measurements to a greater extent than long-term averaging measurements of, for example,  $L_{Aeq}$ .

In Reference [12] it was found that the mean standard deviations of the results of 16 different noise examples from 4 laboratories using 4 different measuring set-ups was 0,3 on the prominence  $P$  and 0,6 dB on the adjustment  $K_1$ .

## 9 Test report

The test report shall contain the information required by the relevant guidelines for the noise measurements. Additionally, the following information shall be given:

- a) Recording and analysis equipment, type, make and model;
- b) A reference to this document, i.e. ISO 1996-3:2022;
- c) Sampling rate for  $L_{pAF}$ , and whether estimated from short-term  $L_{Aeq}$ , see [Clause 4](#);
- d) Procedure used for the measurement of level difference and onset rate;
- e) The working conditions that cause the impulsive sound and the time of the specific measurements;
- f) Weather conditions as required in the ISO 1996 series;
- g) Measured values of level differences and onset rates;
- h) Calculation results of the prominence,  $P$ , and the adjustment,  $K_1$ , and associated uncertainties;
- i) Assessment time interval.

## Annex A (informative)

### Research topics

Within the context of ISO 1996, adjustments are added to assessments of  $L_{Aeq}$  from various sound sources to be able to rate these with respect to expected community response. These adjustments are based on research in which the experienced annoyance of those sounds is often compared with equally annoying road traffic noise.

In this document it is mentioned that the herein described method, meant to objectively categorize sources by determining how prominently the impulsive sound from these sources is perceived by determining the prominence  $P$ , can also be used to directly determine the annoyance relevant adjustment to the measured or calculated  $L_{Aeq}$ .

Research in the late 1980s (Fourth CEC Programme on Human Responses to impulsive noise, listed in the last section of the bibliography) concluded that the predictability of assumed annoyance based on such a prominence of impulsiveness was inconclusive using methods available at that time.

Research listed in the first and second parts of the bibliography have resulted in national standards and legislation, and subsequently, the method contained in this document. Compared to the amount of research on community annoyance from road traffic, aircraft and rail noise, the amount of research on annoyance from impulsive sound is limited.

Further research on relevant sources is recommended to support the development of the PAS into a full ISO standard. Such research should among other things take into account:

- The use of sound signals as would be experienced/assessed:
  - At real-world (large) distances;
  - As influenced by propagation aspects;
  - In both outdoor- and indoor living conditions;
  - With real-world signal to (residual) noise ratios;
- The correlation of  $K_1$  with prominence for impulses with very high onset rate;
- The use of a sufficiently large number of participating listening subjects;
- Rating of annoyance based on comparison with equally annoying traffic noise;
- Surveys of real communities exposed to the actual noise source to develop a dose-response relationship, such as those used for adjustments to road rail and aircraft noise, e.g. CTL.
- The statistical relevance of various ways of considering the prominence of impulses in dose response relations, for instance using maximum prominence within a given time interval versus using an average(d) prominence over an assessment relevant period or other physical aspects of the sound signal.