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**Textile machinery and accessories —  
Beams for winding —**

Part 4:

**Test methods and quality classification of  
flanges for weaver's beams, warper's  
beams and sectional beams**

*Matériel pour l'industrie textile — Ensembles pour enroulement —*

*Partie 4: Méthodes d'essai et classes de qualité pour les joues  
d'ensembles de tissage, d'ourdissiers et sectionnelles*

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## Foreword

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International Standards are drafted in accordance with the rules given in the ISO/IEC Directives, Part 2.

The main task of technical committees is to prepare International Standards. Draft International Standards adopted by the technical committees are circulated to the member bodies for voting. Publication as an International Standard requires approval by at least 75 % of the member bodies casting a vote.

Attention is drawn to the possibility that some of the elements of this document may be the subject of patent rights. ISO shall not be held responsible for identifying any or all such patent rights.

ISO 8116-4 was prepared by Technical Committee ISO/TC 72, *Textile machinery and accessories*, Subcommittee SC 3, *Machinery for fabric manufacturing including preparatory machinery and accessories*.

This third edition cancels and replaces the second edition (ISO 8116-4:1995), which has been technically revised.

ISO 8116 consists of the following parts, under the general title *Textile machinery and accessories — Beams for winding*:

- *Part 1: General vocabulary*
- *Part 2: Warper's beams*
- *Part 3: Weaver's beams*
- *Part 4: Test methods and quality classification of flanges for weaver's beams, warper's beams and sectional beams*
- *Part 5: Sectional beams for warp knitting machines*
- *Part 6: Beams for ribbon weaving and ribbon knitting*
- *Part 7: Beams for dyeing slivers, rovings and yarns*
- *Part 8: Definitions of run-out tolerances and methods of measurement*
- *Part 9: Dyeing beams for textile fabrics*

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# Textile machinery and accessories — Beams for winding —

## Part 4:

# Test methods and quality classification of flanges for weaver's beams, warper's beams and sectional beams

## 1 Scope

This part of ISO 8116 specifies the test procedure for flanges for weaver's beams, warper's beams and sectional beams and the quality classes in this respect.

## 2 Normative references

The following referenced documents are indispensable for the application of this document. For dated references, only the edition cited applies. For undated references, the latest edition of the referenced document (including any amendments) applies.

ISO 8116-1, *Textile machinery and accessories — Beams for winding — Part 1: General vocabulary*

ISO 8116-2:2008, *Textile machinery and accessories — Beams for winding — Part 2: Warper's beams*

ISO 8116-3, *Textile machinery and accessories — Beams for winding — Part 3: Weaver's beams*

ISO 8116-5:2008, *Textile machinery and accessories — Beams for winding — Part 5: Sectional beams for warp knitting machines*

## 3 Terms and definitions

For the purposes of this document, the terms and definitions given in ISO 8116-1 and the following apply.

### 3.1

#### **quality class**

classification of beam flanges according to their deformation behaviour under load

### 3.2

#### **maximum test load**

$F_{\max}$

maximum value of load applied to the beam flange during testing according to its quality class

## 4 Quality classification

Beam flanges are classified according to four quality classes. The designation of the quality classes is Q1, Q2, Q3 or Q4.

Depending on the quality class, the beam flanges are loaded with different ultimate loads. These limit values are given in Clause 6.

For examples of application by quality class, see Annex A.

## 5 Test methods

### 5.1 Principle

The beam flange is subjected to a test load and the resulting deformation is measured.

For weaver's beams, the test load is applied to the flange via a beam barrel. For warper's beams and sectional beams, the load is applied to the beam flange via a pressure plate. A pressure ring with a defined inner diameter is used as an anvil.

The permanent deformation and the plastic deformation of the flange shall not exceed the defined limit values when the maximum load is applied.

### 5.2 Apparatus

**5.2.1 Press device**, with indications for the application of the test load.

**5.2.2 Three dial gauges**, for determination of deformation of the flange with an accuracy of 0,01 mm.

**5.2.3 Measurement device**, for joint installation of the three dial gauges on the bearing device, in an angle of 120° each.

**5.2.4 Steel pressure ring**.

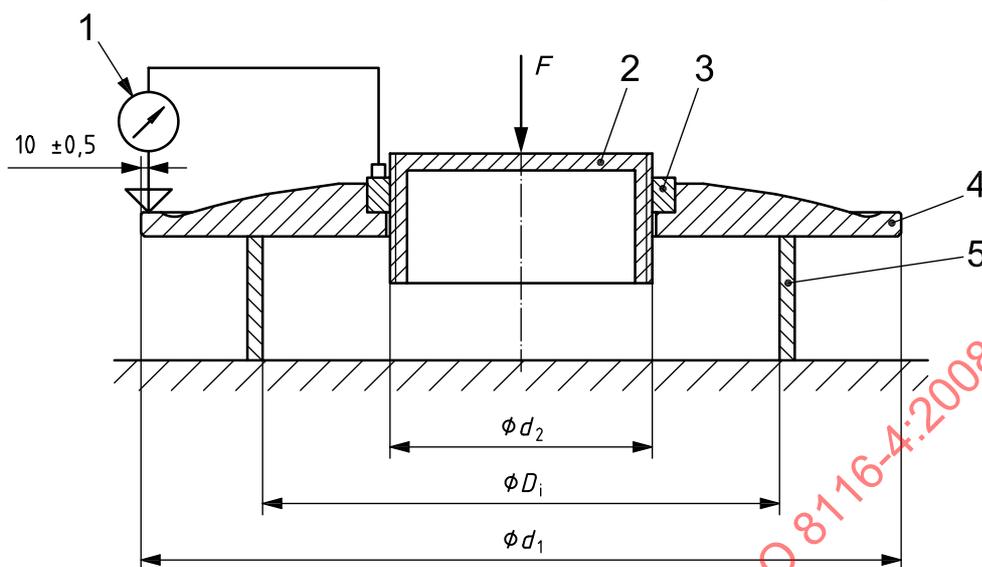
**5.2.5 Beam barrel**, for load application (for weaver's beams).

**5.2.6 Pressure plate**, for load application (for warper's beams and sectional beams).

### 5.3 Testing configuration

For measurement of flange deformation, three dial gauges are installed on the bearing device by means of the measurement device. These are used to measure the relative path between the outer diameter of the beam barrel  $d_2$  and the circle diameter  $d_1 - 20$  mm. The dial gauges are staggered by 120°. The testing configuration for weaver's beams is given in Figure 1. The testing configurations for warper's beams are given in Figure 2 and Figure 3. The testing configuration for sectional beams is given in Figure 4.

Dimensions in millimetres

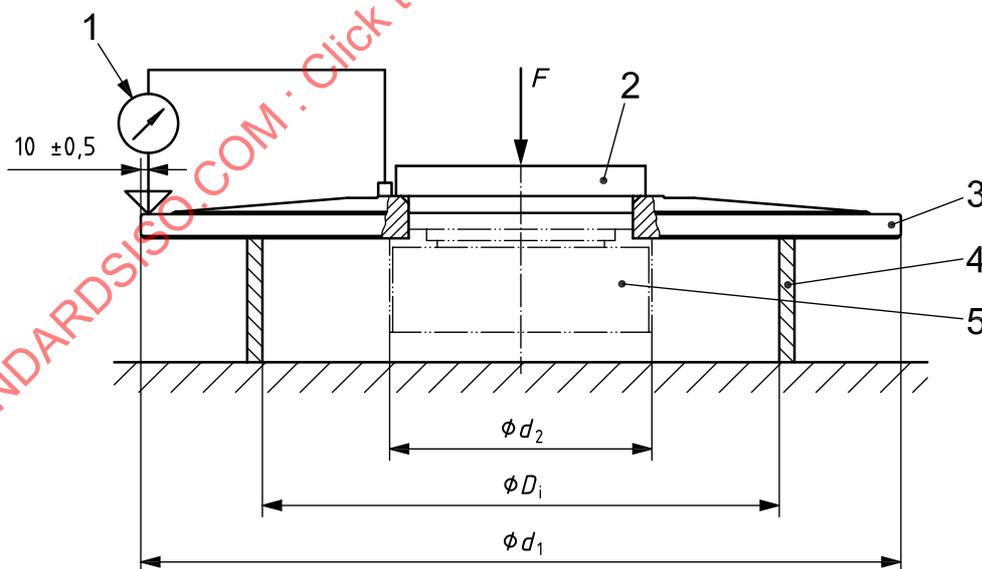


**Key**

- |   |  |
|---|--|
| 1 dial gauge (schematic representation) | $d_1$ outer diameter of weaver's beam flange |
| 2 beam barrel                           | $d_2$ outer diameter of weaver's beam barrel |
| 3 threaded ring                         | $D_i$ inner diameter of pressure ring        |
| 4 weaver's beam                         |  |
| 5 steel pressure ring                   |  |

**Figure 1 — Testing configuration for weaver's beam**

Dimensions in millimetres

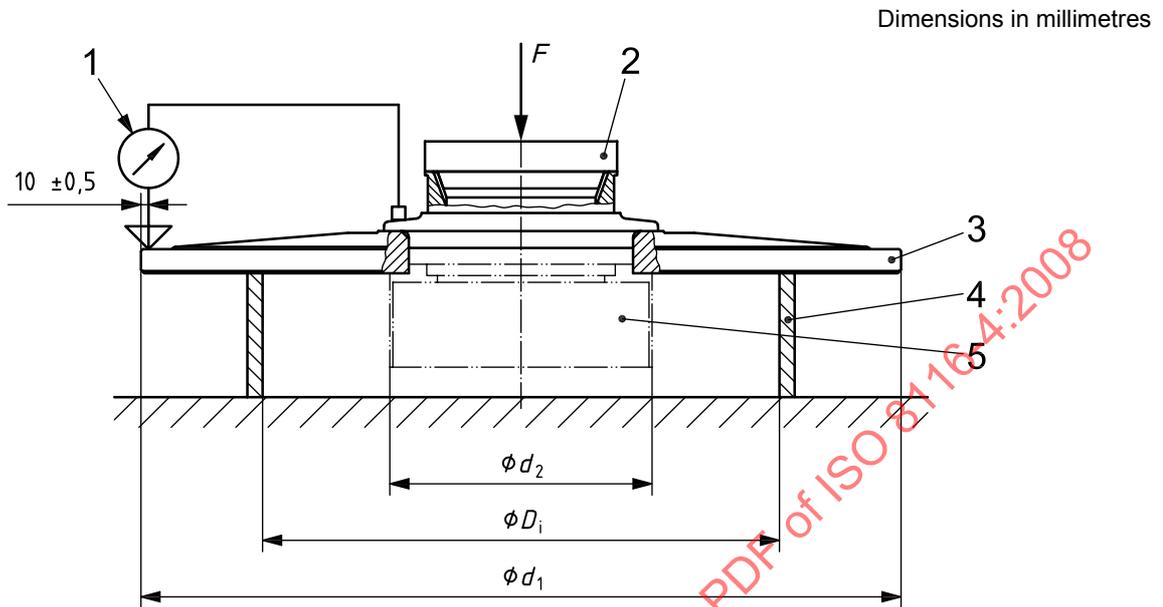


**Key**

- |   |  |
|---|--|
| 1 dial gauge (schematic representation)                 | $d_1$ outer diameter of warper's beam flange |
| 2 pressure plate  | $d_2$ outer diameter of warper's beam barrel |
| 3 warper's beam   | $D_i$ inner diameter of pressure ring        |
| 4 steel pressure ring                                   |  |
| 5 warper's beam barrel (not required for pressure test) |  |

**Figure 2 — Testing configuration for warper's beam flange with shaft (Type A) and cylindrical hole (Type B)**

The diameter of the pressure plate for load application for warper's beams of Type A and Type B is defined as  $d_2 - 20$  mm (see Figure 2).



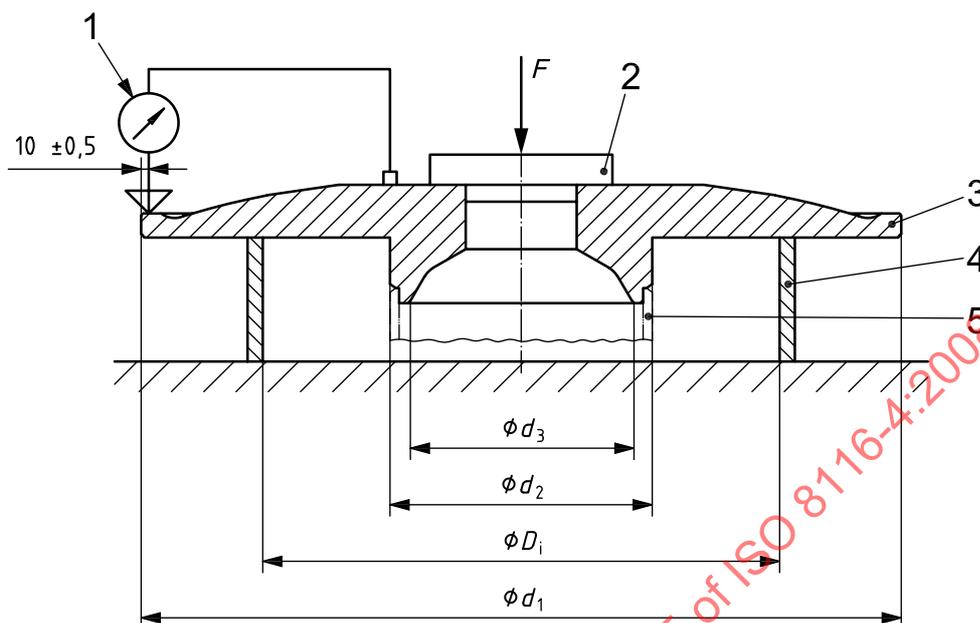
**Key**

- |   |  |
|---|--|
| 1 dial gauge (schematic representation)                 | $d_1$ outer diameter of warper's beam flange |
| 2 pressure plate  | $d_2$ outer diameter of warper's beam barrel |
| 3 warper's beam flange                                  | $D_i$ inner diameter of pressure ring        |
| 4 steel pressure ring                                   |  |
| 5 warper's beam barrel (not required for pressure test) |  |

**Figure 3 — Testing configuration for warper's beam flange with tooth cone — Type C**

The diameter of the pressure plate for load application for warper's beams with tooth cone (Type C) is defined using  $d_5$  in accordance with ISO 8116-2:2008, Table 2.

Dimensions in millimetres

**Key**

- |  |  |
|--|--|
| 1 dial gauge (schematic representation)                  | $d_1$ outer diameter of sectional beam flange                      |
| 2 pressure plate   | $d_2$ outer diameter of sectional beam barrel                      |
| 3 sectional beam flange                                  | $d_3$ bore diameter of flange (see also ISO 8116-5:2008, Figure 1) |
| 4 steel pressure ring                                    | $D_i$ inner diameter of pressure ring                              |
| 5 sectional beam barrel (not required for pressure test) |  |

**Figure 4 — Testing configuration for sectional beams**

The diameter of the pressure plate for load application for sectional beams of knitting machines is defined using  $d_3 + 40$  mm.

**5.4 Performance**

The measurement device is installed as described in 5.3. The beam flange, the pressure ring and the pressure plate, if required, are aligned centrally below the press loading pad.

Stepwise loading of the flange shall occur in steps to be chosen usefully.

The load applied and the deformation are determined at the test area for each loading step. The value of the total deformation is calculated from the average of the three measurement values. After each load step, unloading of the flange is optional.

After unloading, the values indicated are read with the dial gauge. The values for the plastic deformation are calculated from the average of the three measurement values.

Then loading is applied with the next higher load value.

This procedure is repeated until the defined maximum test load of the corresponding quality class as given in Equation (2) and Table 1 is reached.

The beam flange corresponds to the quality class if the value measured for the total deformation and the value measured for the plastic deformation are below the values obtained when using Equation (3) and Equation (4).

Once the given maximum load has been achieved, the plastic deformation shall be measured after unloading. Subsequently, the dial gauges are set to "zero". The maximum test load shall again be applied. After unloading, only an insignificantly low residual deformation value shall be read.

## 6 Pressure ring diameter, maximum test load and limit values of deformation

The diameter of the pressure ring, maximum test load and limit values of deformation shall be calculated using Equations (1), (2) or (3) for any flange geometry:

- for weaver's beams in accordance with ISO 8116-3, the values are given in Table 2;
- for warper's beams in accordance with ISO 8116-2, the values are given in Table 3;
- for sectional beams in accordance with ISO 8116-5, the values are given in Table 4.

### 6.1 Pressure ring diameter

The diameter of the pressure ring is calculated, depending on the inner and outer diameter of the beam flange, using Equation (1):

$$D_i = \frac{2}{3} \times \frac{d_1^3 - d_2^3}{d_1^2 - d_2^2} \quad (1)$$

where

- $D_i$  is the inner diameter of the pressure ring, in millimetres;
- $d_1$  is the outer diameter of the beam flange, in millimetres;
- $d_2$  is the outer diameter of the beam barrel, in millimetres.

The tolerance for the diameter of the pressure ring,  $D_i$ , may not exceed  $\pm 1$  mm.

NOTE Equation (1) corresponds to the centre of the diameter of a circular ring segment on the condition that the angle of the circular ring segment reaches zero. In practice, the actual load on the beam flange is different, depending on the winding.

### 6.2 Maximum test load

Depending on the quality class, the maximum test load is calculated from the maximum test load given in Table 1 multiplied by the maximum winding area of the beam flange, using Equation (2).

$$F_{\max} = A_{\max} \times p_i \quad (2)$$

where

- $F_{\max}$  is the maximum test load, in kilonewtons;
- $A_{\max}$  is the maximum winding area of the beam flange, in square millimetres;

$$A_{\max} = \frac{\pi}{4} \times (d_1^2 - d_2^2)$$

- $p_i$  is the maximum test load, in megapascals.

Table 1 — Limit loads of quality classes

Quality class	Maximum test load $p_i$ MPa
Q1	0,08
Q2	0,2
Q3	0,5
Q4	0,8

### 6.3 Limit value of deformation

The limit value of total deformation at maximum test load is calculated, depending on the geometry of the flange, using Equation (3):

$$f_{\text{tot-lim}} = \frac{4 \times (d_1 - d_2)}{1000} \quad (3)$$

where

- $f_{\text{tot-lim}}$  is the admissible total flange deformation, in millimetres;
- $d_1$  is the outer diameter of the beam flange, in millimetres;
- $d_2$  is the outer diameter of the beam barrel, in millimetres.

The limit value of the plastic deformation at maximum test load amounts to a quarter of the limit value of total deformation in the case of initial loading of the beam flange.

If the maximum test load is again applied to the beam flange, as shown in Equation (4), the proportion of plastic deformation shall be insignificantly low.

$$f_{\text{plast-lim}} = \frac{f_{\text{tot-lim}}}{4} = \frac{(d_1 - d_2)}{1000} \quad (4)$$

where

- $f_{\text{plast-lim}}$  is the admissible plastic flange deformation, in millimetres;
- $f_{\text{tot-lim}}$  is the admissible total flange deformation, in millimetres;
- $d_1$  is the outer diameter of the beam flange, in millimetres;
- $d_2$  is the outer diameter of the beam barrel, in millimetres.

### 6.4 Values for weaver's beams

The values for the pressure ring diameter, the maximum test load and the limit values of deformation for weaver's beams in accordance with ISO 8116-3 are given in Table 2.

Table 2 — Test values for weaver's beams in accordance with ISO 8116-3

Flange geometry		Pressure ring inner diameter $D_i$ mm	Maximum test load of quality Class Q1				Limit values of flange deformations	
$d_1$ mm	$d_2$ mm		$F_{\max Q1}$ kN	$F_{\max Q2}$ kN	$F_{\max Q3}$ kN	$F_{\max Q4}$ kN	$f_{\text{tot-lim}}$ mm	$f_{\text{plast-lim}}$ mm
500	150	356	14	36	89	143	1,4	0,4
600	150	420	21	53	133	212	1,8	0,5
700	150	484	29	73	184	294	2,2	0,6
750	150	517	34	85	212	339	2,4	0,6
800	150	549	39	97	242	388	2,6	0,7
800	216	564	37	93	233	373	2,3	0,6
850	216	596	42	106	265	425	2,5	0,6
900	216	628	48	120	300	480	2,7	0,7
950	216	660	54	134	336	538	2,9	0,7
1 000	269	705	58	146	364	583	2,9	0,7
1 250	269	865	94	234	585	936	3,9	1,0
1 400	269	962	119	297	741	1 186	4,5	1,1
1 500	269	1 027	137	342	855	1 368	4,9	1,2

### 6.5 Values for warper's beams

The values for the pressure ring diameter, the maximum test load and the limit values of deformation for warper's beams in accordance with ISO 8116-2 are given in Table 3.