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**Reciprocating internal combustion  
engines — Measurement of sound  
power level using sound pressure —**

**Part 1:  
Engineering method**

*Moteurs alternatifs à combustion interne — Mesurage du niveau de  
puissance acoustique à partir de la pression acoustique —*

*Partie 1: Méthode d'expertise*

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## Foreword

ISO (the International Organization for Standardization) is a worldwide federation of national standards bodies (ISO member bodies). The work of preparing International Standards is normally carried out through ISO technical committees. Each member body interested in a subject for which a technical committee has been established has the right to be represented on that committee. International organizations, governmental and non-governmental, in liaison with ISO, also take part in the work. ISO collaborates closely with the International Electrotechnical Commission (IEC) on all matters of electrotechnical standardization.

The procedures used to develop this document and those intended for its further maintenance are described in the ISO/IEC Directives, Part 1. In particular, the different approval criteria needed for the different types of ISO documents should be noted. This document was drafted in accordance with the editorial rules of the ISO/IEC Directives, Part 2 (see [www.iso.org/directives](http://www.iso.org/directives)).

Attention is drawn to the possibility that some of the elements of this document may be the subject of patent rights. ISO shall not be held responsible for identifying any or all such patent rights. Details of any patent rights identified during the development of the document will be in the Introduction and/or on the ISO list of patent declarations received (see [www.iso.org/patents](http://www.iso.org/patents)).

Any trade name used in this document is information given for the convenience of users and does not constitute an endorsement.

For an explanation of the voluntary nature of standards, the meaning of ISO specific terms and expressions related to conformity assessment, as well as information about ISO's adherence to the World Trade Organization (WTO) principles in the Technical Barriers to Trade (TBT), see [www.iso.org/iso/foreword.html](http://www.iso.org/iso/foreword.html).

This document was prepared by Technical Committee ISO/TC 70, *Internal combustion engines*.

This first edition of ISO 6798-1, together with ISO 6798-2, cancels and replaces ISO 6798:1995, which has been technically revised. The main changes compared to the previous edition are as follows:

- the requirements of the test environment and the measurement uncertainty have been changed;
- the accuracy of measurement results has been changed from 1 dB to 0,1 dB;
- the calculation of background noise correction has been changed from table method to formula method;
- the requirements of installation of engine and auxiliaries have been specified clearly;
- the specification for measurement units has been added;
- the criterion for position adequacy of microphone has been added;
- the criterion for acoustic adequacy of test environment has been improved.

A list of all parts in the ISO 6798 series can be found on the ISO website.

Any feedback or questions on this document should be directed to the user's national standards body. A complete listing of these bodies can be found at [www.iso.org/members.html](http://www.iso.org/members.html).

## Introduction

The ISO 6798 series can be used to calculate the sound power level by using the sound pressure level on a measurement surface enveloping a noise source.

The measurement result of sound power level has nothing to do with the test environment and the installation conditions of the noise source, which is one of the important reasons for using sound power level to characterize the noise radiation of different types of machinery and equipment.

Sound power level has the following applications:

- indication of noise radiated from machinery under the specified condition;
- validation of the indicated value of a noise;
- radiation noise comparison of different types and sizes of machinery;
- comparison of the noise limit value specified in the purchase contract or specification;
- making engineering measures to reduce radiation noise of machinery (generally, the frequency band sound power level is also needed);
- prediction of the sound pressure level of noise in the specified position.

[Table 1](#) gives the measurement methods for determining the sound power level of two types of accuracy grade, these measurement methods apply to the measurement on the enveloping surface in the ISO 6798 series. The measurement result of the sound power level is rounded to the nearest 0,1 dB. The method given in this document allows the determination of the A-weighted and frequency-band sound power level, the accuracy of the measurement result is grade 2. The A-weighted sound power level can also be calculated from frequency band sound power levels, but the calculated result from frequency band data can differ from what is determined from the measured A-weighted sound pressure levels.

[Table 2](#) gives the measurement uncertainty of the sound power level (upper bound values of the standard deviation of reproducibility). The standard deviations listed in [Table 2](#) are the comprehensive effect of the measurement uncertainty, but do not include variations of the sound power level caused by installation and operation conditions of the noise source.

In the noise control of a reciprocating internal combustion engine, the relevant members (the manufacturers, installers, and users) should conduct effective communication of acoustic information which is obtained from measurement. The measurement result is valid when in the specified measurement conditions by using the instrumentation and measurement method as specified in this document to obtain a clear acoustic value. The ISO 6798 series can be used according to the purpose of noise measurement and measurement conditions.

**Table 1 — How the ISO 6798 series determines the sound power level using sound pressure**

Parameters	ISO 6798-1 Engineering method Accuracy grade 2	ISO 6798-2 Survey method Accuracy grade 3
International Standards referenced	ISO 3744	ISO 3746
Test environment	An essentially free field over a reflecting plane	An acoustic field over a reflecting plane
Noise source volume	Unlimited, depending on the test environment	
Criterion for background noise <sup>a</sup>	$\Delta L_{pA} \geq 6,0$ dB $K_{1A} \leq 1,3$ dB	$\Delta L_{pA} \geq 3,0$ dB $K_{1A} \leq 3,0$ dB
Criterion for acoustic adequacy of test environment <sup>b</sup>	$K_{2A} \leq 4,0$ dB	$K_{2A} \leq 7,0$ dB

**Table 1** (continued)

Parameters	ISO 6798-1 Engineering method Accuracy grade 2	ISO 6798-2 Survey method Accuracy grade 3
Criterion for position adequacy of microphone <sup>c</sup>	$s(L'_{pAm}) \leq 1,0$ dB	$s(L'_{pAm}) \leq \sqrt{2}$ dB
Instrumentation <sup>d</sup> sound level meter/filter/sound calibrator	Class 1/class 1/class 1	Class 2/class 2/class 1
Sound power level acquired	A-weighted or frequency bands	A-weighted
Application	Acceptance test of sound power level; making engineering measures	Comparative test of sound power level

<sup>a</sup> For the difference of sound pressure level,  $\Delta L_{pA}$ , and the background noise correction,  $K_{1A}$ , see 8.3.2.

<sup>b</sup> For the environmental correction,  $K_{2A}$ , see 8.3.3.

<sup>c</sup> For the standard deviation,  $s(L'_{pAm})$ , see 7.7.

<sup>d</sup> For the requirements of instrumentation, see Clause 5.

**Table 2 — Measurement uncertainty of the sound power level (upper bound values of the standard deviation of reproducibility)**

Mid-band frequency Hz		ISO 6798-1 standard deviation of reproducibility	ISO 6798-2 standard deviation of reproducibility
Octave bands	One-third-octave bands	dB	dB
63	50 to 80	5,0	—
125	100 to 160	3,0	
250	200 to 315	2,0	
500	400 to 630	1,5	
1 000 to 4 000	800 to 5 000	1,5	
8 000	6 300 to 10 000	2,5	
A-weighted		1,5	

# Reciprocating internal combustion engines — Measurement of sound power level using sound pressure —

## Part 1: Engineering method

### 1 Scope

This document specifies the engineering method, which is the measurement method of the sound power level for reciprocating internal combustion engines.

This document applies to all reciprocating internal combustion engines falling within the field of application of ISO 3046-1 and other internal combustion engines where no suitable International Standard exists.

NOTE In this document, reciprocating internal combustion engines are referred to as engines unless otherwise explained.

### 2 Normative references

The following documents are referred to in the text in such a way that some or all of their content constitutes requirements of this document. For dated references, only the edition cited applies. For undated references, the latest edition of the referenced document (including any amendments) applies.

ISO 3046-1, *Reciprocating internal combustion engines — Performance — Part 1: Declarations of power, fuel and lubricating oil consumptions, and test methods — Additional requirements for engines for general use*

ISO 3046-3, *Reciprocating internal combustion engines — Performance — Part 3: Test measurements*

ISO 6926, *Acoustics — Requirements for the performance and calibration of reference sound sources used for the determination of sound power levels*

IEC 60942, *Electroacoustics — Sound calibrators*

IEC 61260-1, *Electroacoustics — Octave-band and fractional-octave-band filters — Part 1: Specifications*

IEC 61672-1, *Electroacoustics — Sound level meters — Part 1: Specifications*

### 3 Terms, definitions and symbols

#### 3.1 Terms and definitions

For the purposes of this document, the terms and definitions given in ISO 3046-1, ISO 6926, IEC 61260-1, IEC 61672-1 and the following apply.

ISO and IEC maintain terminological databases for use in standardization at the following addresses:

- ISO Online browsing platform: available at <https://www.iso.org/obp>
- IEC Electropedia: available at <http://www.electropedia.org/>

**3.1.1  
sound pressure**

$p$   
difference between the instantaneous pressure and the static pressure

Note 1 to entry: It is expressed in pascals (Pa).

[SOURCE: ISO 80000-8:2007, 8-9.2, modified — Note1 to entry has been added.]

**3.1.2  
sound pressure level**

$L_p$   
ten times the logarithm to the base 10 of the ratio of the square of the *sound pressure* (3.1.1),  $p$ , to the square of a reference value,  $p_0$

Note 1 to entry: Sound pressure level is calculated using [Formula \(1\)](#):

$$L_p = 10 \times \lg \left( \frac{p^2}{p_0^2} \right) \tag{1}$$

where

- $p$  is the sound pressure;
- $p_0$  is the reference value, which equals 20  $\mu$ Pa.

Note 2 to entry: If specific frequency and time weightings, as specified in IEC 61672-1, and/or specific frequency bands are applied, this is indicated by appropriate subscripts, e.g.  $L_{pA}$  denotes the A-weighted sound pressure level.

Note 3 to entry: It is expressed in decibels (dB).

[SOURCE: ISO 3744:2010, 3.2, modified — Editorial modifications have been made.]

**3.1.3  
time-averaged sound pressure level**

$L_{p,T}$   
ten times the logarithm to the base 10 of the ratio of the time average of the square of the *sound pressure* (3.1.1),  $p$ , during a stated time interval of duration,  $T$  (starting at  $t_1$  and ending at  $t_2$ ), to the square of a reference value,  $p_0$

Note 1 to entry: the time-averaged sound pressure level is calculated using [Formula \(2\)](#):

$$L_{p,T} = 10 \times \lg \left[ \frac{\frac{1}{T} \int_{t_1}^{t_2} p^2(t) dt}{p_0^2} \right] \tag{2}$$

where

- $p$  is the sound pressure;
- $p_0$  is the reference value, which equals 20  $\mu$ Pa;
- $T$  is a stated time interval of duration.

Note 2 to entry: In general, the subscript “ $T$ ” is omitted since time-averaged sound pressure levels are necessarily determined over a certain measurement time interval.

Note 3 to entry: Time-averaged sound pressure levels are often A-weighted, in which case they are denoted by  $L_{pA,T}$  which is usually abbreviated to  $L_{pA}$ .

Note 4 to entry: It is expressed in decibels (dB).

[SOURCE: ISO 3744:2010, 3.3, modified — Editorial modifications have been made.]

### 3.1.4 surface time-averaged sound pressure level

$$\overline{L}_p$$

mean (energy average) of the *time-averaged sound pressure levels* (3.1.3) over all the microphone positions, or traverses, on the measurement surface, with the background noise correction,  $K_1$ , and the environmental correction,  $K_2$ , applied

Note 1 to entry: It is expressed in decibels (dB).

[SOURCE: ISO 3744:2010, 3.18, modified — Editorial modifications have been made.]

### 3.1.5 measurement time interval

$$T$$

portion or a multiple of an operational period or operational cycle of the noise source under test for which the *time-averaged sound pressure level* (3.1.3) is determined

Note 1 to entry: It is expressed in seconds (s).

[SOURCE: ISO 3744:2010, 3.5, modified — Editorial modifications have been made to Note 1 to entry.]

### 3.1.6 acoustic free field

sound field in a homogeneous, isotropic medium free of boundaries

Note 1 to entry: In practice, an acoustic free field is a field in which the influence of reflections at the boundaries or other disturbing objects are negligible over the frequency range of interest.

[SOURCE: ISO 3744:2010, 3.6]

### 3.1.7 reflecting plane

sound- reflecting planar surface on which the noise source under test is located

[SOURCE: ISO 3744:2010, 3.8]

### 3.1.8 acoustic free field over a reflecting plane

*acoustic free field* (3.1.6) in the half-space above an infinite *reflecting plane* (3.1.7) in the absence of any other obstacles

[SOURCE: ISO 3744:2010, 3.7]

### 3.1.9 frequency range of interest

frequency range of octave bands with nominal mid-band frequencies from 63 Hz to 8 000 Hz (including one-third octave bands with mid-band frequencies from 50 Hz to 10 000 Hz)

Note 1 to entry: For special purposes, the frequency range can be extended or reduced, provided that the test environment and instrument specifications are satisfactory for use over the modified frequency range. Changes to the frequency range of interest are included in the test report.

[SOURCE: ISO 3744:2010, 3.9, modified — Frequencies have been changed.]

### 3.1.10 reference box

hypothetical right smallest parallelepiped terminating on one *reflecting plane* (3.1.7) on which the noise source under test is located, that just encloses the source including all the significant sound radiating components

[SOURCE: ISO 3744:2010, 3.10, modified — Test table has been deleted.]

**3.1.11**

**measurement distance**

*d*

distance from the *reference box* (3.1.10) to a parallelepiped measurement surface

[SOURCE: ISO 3744:2010, 3.12, modified — Note has been deleted.]

**3.1.12**

**measurement surface**

*S*

hypothetical parallelepiped surface of area on which the microphone positions are located at which the *sound pressure levels* (3.1.2) are measured, enveloping the noise source under test and terminating on the *reflecting plane* (3.1.7) on which the source is located

[SOURCE: ISO 3744:2010, 3.14]

**3.1.13**

**background noise**

noise from all sources other than the noise source under test

Note 1 to entry: Background noise includes contributions from airborne sound, noise from structure-borne vibration, and electrical noise in the instrumentation.

[SOURCE: ISO 3744:2010, 3.15]

**3.1.14**

**background noise correction**

$K_1$

correction applied to the mean (energy average) of the *time-averaged sound pressure levels* (3.1.3) over all the microphone positions on the *measurement surface* (3.1.12), to account for the influence of *background noise* (3.1.13)

Note 1 to entry: The background noise correction is frequency dependent; the correction in the case of a frequency band is denoted by  $K_{1f}$ , where  $f$  denotes the relevant mid-band frequency, and that in the case of A-weighting is denoted by  $K_{1A}$ .

Note 2 to entry: It is expressed in decibels (dB).

[SOURCE: ISO 3744:2010, 3.16]

**3.1.15**

**environmental correction**

$K_2$

correction applied to the mean (energy average) of the *time-averaged sound pressure levels* (3.1.3) over all the microphone positions on the *measurement surface* (3.1.12), to account for the influence of reflected sound

Note 1 to entry: The environmental correction is frequency dependent; the correction in the case of a frequency band is denoted by  $K_{2f}$ , where  $f$  denotes the relevant mid-band frequency, and that in the case of A-weighting is denoted by  $K_{2A}$ .

Note 2 to entry: It is expressed in decibels (dB).

[SOURCE: ISO 3744:2010, 3.17, modified — Note 3 has been deleted.]

**3.1.16**

**sound power**

*W*

through a surface, product of the *sound pressure* (3.1.1),  $p$ , and the component of the particle velocity,  $u_n$ , at a point on the surface in the direction normal to the surface, integrated over that surface

Note 1 to entry: The quantity relates to the rate per time at which airborne sound energy is radiated by a source.

Note 2 to entry: It is expressed in watts (W).

[SOURCE: ISO 3744:2010, 3.20, modified — Symbol has been changed.]

### 3.1.17 sound power level

$L_W$

ten times the logarithm to the base 10 of the ratio of the *sound power* (3.1.16) of a source,  $W$ , to a reference value,  $W_0$

Note 1 to entry: the sound power level is calculated using [Formula \(3\)](#):

$$L_W = 10 \times \lg \left( \frac{W}{W_0} \right) \quad (3)$$

where

$W$  is the sound power;

$W_0$  is the reference value, which equals 1 pW.

Note 2 to entry: If a specific frequency weighting, as specified in IEC 61672-1, and/or specific frequency bands are applied, this is indicated by appropriate subscripts, e.g.  $L_{WA}$  denotes the A-weighted sound power level.

Note 3 to entry: It is expressed in decibels (dB).

[SOURCE: ISO 3744:2010, 3.21, modified — Editorial modifications have been made.]

## 3.2 Symbols

Symbol	Description	Unit
$2a$	measurement surface length	m
$2b$	measurement surface width	m
$c$	measurement surface height	m
$d$	measurement distance	m
FS	flywheel side	—
$l_1$	reference box length	m
$l_2$	reference box width	m
$l_3$	reference box height	m
$r_s$	size ratio	—
•	key microphone positions	—
◦	additional microphone positions	—
▨	reflecting plane	—
■	reference box	—

## 4 Test environment

### 4.1 General

The test environments that are applicable for measurements in accordance with this document are as follows:

- a) a room or a flat outdoor area which is adequately isolated from background noise and which provides an acoustic free field over a reflecting plane, or;

- b) a room or a flat outdoor area which is adequately isolated from background noise and in which an environmental correction can be applied to allow for a limited contribution from the reverberant field to the sound pressures on the measurement surface.

Environmental conditions having an adverse effect on the microphones used for the measurements (e.g. wind, impingement of air discharge, high or low temperatures) shall be avoided. The instructions of the manufacturer of the measuring instrumentation regarding adverse environmental conditions shall be followed. Particular care should be exercised to ensure that any plane does not radiate any appreciable sound due to vibrations.

#### 4.2 Criterion for background noise

The time-averaged sound pressure level (abbreviated as sound pressure level in the following text) of the background noise measured and averaged over the microphone positions shall be at least 6,0 dB, and preferably more than 15,0 dB, below the corresponding uncorrected sound pressure level of the noise source under test when measured in the presence of this background noise.

For the measurements in frequency bands, the criteria for background noise may not be achievable in all frequency bands, even when the background noise levels in the test room are extremely low and well controlled. In this situation, for the measurements in frequency bands, the following steps shall be followed to determine whether the requirements of the background noise criteria are met.

- a) Calculate the data from every frequency band within the frequency range of interest to A-weighted sound power level.
- b) Delete those bands within the frequency range of interest in which the A-weighted sound power level of the noise source under test is at least 15,0 dB below the highest A-weighted sound power level and for which  $\Delta L_{pA} < 6,0$  dB (see 8.3), then repeat the calculation of A-weighted sound power level.
- c) If the calculation value difference between a) and b) is less than or equal to 0,5 dB, the A-weighted sound power level determined from the data for all bands may be considered as conforming to the background noise criteria of this document. If the calculation value difference between a) and b) is larger than 0,5 dB, the measurement is not valid.

#### 4.3 Criterion for acoustic adequacy of test environment

[Annex A](#) specifies the procedures for determining the environmental correction,  $K_2$ .

As far as is practicable, the test environment shall be free from reflecting objects other than the reflecting plane (the ground). The reflecting plane shall extend at least 0,5 m beyond the projection of the measurement surface on the plane. The sound absorption coefficient of the reflecting plane shall be less than 0,1 in the frequency range of interest.

NOTE 1 Smooth concrete or smooth sealed asphalt surface(s) can meet the requirements.

Measurements in accordance with this document are only valid when  $K_2 \leq 4,0$  dB.

NOTE 2 When  $4,0 < K_2 \leq 7,0$ , see ISO 6798-2. If necessary, ISO 9614 (all parts) can be used.

NOTE 3 The environmental correction,  $K_2$ , is assumed to be zero for measurements made in hemi-anechoic rooms which meet the requirements of ISO 3745.

The environmental correction,  $K_2$ , shall be first determined without reference to frequency band data, using one of the procedures in [Annex A](#). Where it is decided to make measurements in frequency bands, the relevant environmental correction  $K_2$  and the sound power level of the noise source  $L_W$  shall be determined in each band over the frequency range of interest in accordance with [A.2](#) or [A.3](#).  $L_{WA}$  of a noise source shall be calculated in accordance with [Annex B](#).

## 5 Instrumentation

### 5.1 General

The instrumentation system, including the microphones, cables and windscreen, if used, shall meet the requirements of IEC 61672-1, class 1, and the filters shall meet the requirements of IEC 61260-1, class 1.

### 5.2 Calibration

Before and after each series of measurements, a sound calibrator meeting the requirements of IEC 60942, class 1 shall be applied to each microphone to verify the calibration of the entire measuring system at one or more frequencies within the frequency range of interest. Without any adjustment, the difference between the readings made before and after each series of measurements shall be less than or equal to 0,5 dB. If this value is exceeded, the results of the series of measurements shall be discarded.

The sound calibrator, filter and the instrumentation system which meet the requirements, and the reference sound source (RSS) that meets the requirements of ISO 6926, shall be verified at intervals in a laboratory making calibrations traceable to appropriate standards.

Unless otherwise specified, the sound calibrator should be calibrated at intervals not exceeding 1 year, the instrumentation system, filter and the reference sound source should be calibrated at intervals not exceeding 2 years.

### 5.3 Application

To minimize the influence of observers on the noise measurements, the microphones shall be preferably mounted on a rigid frame or stand which is not connected to the vibrating surface, the microphone shall always be oriented in such a way that the angle of incidence of the sound waves is that for which the microphone is calibrated and always be oriented to the centre of the tested object (the measurement unit(s) related to the microphone position).

The sound pressure level shall be measured using an integrating sound level meter. If the sound level meter is used to measure time-weighting sound pressure level, the time-weighting characteristic "S" shall be used for the noise source under test operated in steady condition and the time-weighting characteristic "F" shall be used for the noise source under test operated in non-steady condition (e.g. engine operated in the accelerated or decelerated condition). The measured average value can be expressed as the sound pressure level.

The period of stationary measurement for the sound pressure level shall be at least 4 s, 8 s or above is better.

## 6 Installation and operation conditions

### 6.1 General

The way the engine under test is installed and operated has a significant influence on the sound power radiated by a noise source. This clause specifies conditions that are intended to minimize variations in the sound power level due to the installation and operating conditions of the noise source under test.

The engine is a multiple noise source, including the following noise sources:

- air-borne noise (this document);
- exhaust gas noise;
- intake-air noise;
- structure-borne noise.

NOTE For exhaust noise, see ISO 15619; For intake noise, see ISO/TS 19425; For structural noise, See ISO 13332.

## 6.2 Installation conditions

The engine to be tested shall be installed with respect to, or driven on, the reflecting plane (the ground), the engine shall be located at a sufficient distance from any reflecting wall(s) or the ceiling or any reflecting object(s) so that the requirements given in 4.2, 4.3 and 7.4 are satisfied on the measurement surface.

The engine noise radiated is affected by supporting type of engine, connection type with dynamometer equipment, installation height etc.

If the mounting base is rigid, the engine shall be resiliently mounted on the base, the mounting base has a sufficiently high mechanical impedance to prevent extraneous noise radiation from vibration. If the mounting base is resilient, the engine may be rigidly mounted on the base and the natural frequency of the mounting base shall be  $\sqrt{2}/2$  times lower than the firing frequency under test. Otherwise, any sound radiating from the foundation as a result of structure vibration shall be treated as extraneous noise and minimize its effect.

The engine shall be resiliently connected with dynamometer equipment to avoid coupling with it, which affects engine noise radiation.

The distance between the engine lowest noise radiation surface (usually is oil pan bottom) and the reflecting plane (the ground) shall be less than or equal to 0,5 m.

## 6.3 Engine conditions and operation conditions

### 6.3.1 Engine conditions

The engine noise radiated is affected by the auxiliaries which are equipped on the engine; the condition of engine shall meet the requirements of ISO 3046-1. Any air cleaner, exhaust silencer and cooling fan, etc., if equipped, shall be recorded in the report. A gearbox or any driven machinery which load the engine under test should be stated in the report. Noise radiated from any such driven machinery shall be regarded as extraneous noise.

NOTE 1 For the determination of the sound power level of exhaust noise, see ISO 15619. For special purposes, the test distance starts from the contour of the exhaust pipe and a number of measuring points of two (90° to outlet) can be used although not recommended.

NOTE 2 For the determination of the sound power level of intake noise, see ISO/TS 19425.

It is essential to use equipment or non-basic auxiliaries (such as a blower for cooling) to do bench test for some engines with specified purposes (such as motorcycles). Noise radiated from this equipment or non-basic auxiliaries shall be regarded as extraneous noise, or this equipment or non-basic auxiliaries shall be temporarily turned off to ensure that the engine can operate normally.

The extraneous noise is a part of background noise; appropriate steps shall be taken to reduce extraneous noise in order to comply with 4.2. This can be done by shielding or wrapping the structure surface with a heavy material that has low transmission capabilities in the frequency range of the extraneous noise, and by using a muffler to reduce the aerodynamic noise (gas/liquid).

### 6.3.2 Operating conditions

For the noise measurement, the engine shall be operated at the ISO standard power and corresponding rate as defined in ISO 3046-1 under the ISO standard reference conditions in a steady state. At that time, the temperature of the oil and coolant shall be stable, the ambient and intake air temperature shall not be higher than 45 °C.

Measurements can be made in accelerated/decelerated conditions and other operating conditions if necessary, all measurements made in such conditions shall be stated in the test report.

The engine power and corresponding rate shall be measured according to the requirements of ISO 3046-3.

## 7 Measurement

### 7.1 General

Engineering method (accuracy grade 2) is a method for determining the sound power level (A-weighted or in frequency bands) of the noise source from sound pressure levels (A-weighted or in frequency bands) measured on a measurement surface enveloping the noise source in an environment that approximates to an acoustic free field over a reflecting plane, which provides a relatively complete evaluation about the engine. This method can be used for acceptance tests and engineering measures.

NOTE 1 The aim of engineering method in measuring the sound power level is to obtain accuracy grade 2 test results. When the correction for background noise and/or the environmental correction and/or the installation condition and/or microphone locations cannot meet the requirements of this document, accuracy grade 3 result of sound power level is obtained (see ISO 6798-2).

NOTE 2 If declaration is necessary, see ISO 4871.

In order to facilitate the selection of the measurement surface and the arrangement of the microphones, the reference box and measurement distance shall first be determined for noise measurement.

The measurands include the sound pressure level of noise source under operation and the sound pressure level of background noise when the noise source does not work.

### 7.2 Measurement uncertainty

The measurement uncertainty of the sound power level determined in accordance with this document shall meet the requirements of [Table 3](#).

**Table 3 — Measurement uncertainty of sound power level (upper bound values of the standard deviation of reproducibility)**

Mid-band frequency Hz		Engineering method standard deviation of reproducibility dB
Octave bands	One-third-octave bands	
63	50 to 80	5,0
125	100 to 160	3,0
250	200 to 315	2,0
500 to 4 000	400 to 5 000	1,5
8 000	6 300 to 10 000	2,5

NOTE 1 The standard deviations are associated with the test conditions and procedures defined in this document, including the methods of arrangement of microphones and the measurement procedures of environmental correction but not with the noise source itself, i.e. variations of installation and operation conditions.

NOTE 2 For a family of noise sources, with similar size or similar sound power spectra, and/or several laboratories using the same/similar facilities and instrumentation, the uncertainty associated with interlaboratory variability is less than the values given in this table.

NOTE 3 The standard deviations of reproducibility include the standard deviations of repeatability; this uncertainty is usually much smaller than the uncertainty associated with interlaboratory variability.

NOTE 4 The standard deviations are applicable to measurements on an individual noise source.

**Table 3** (continued)

Mid-band frequency Hz		Engineering method standard deviation of reproducibility dB
Octave bands	One-third-octave bands	
A-weighted		1,5
<p>NOTE 1 The standard deviations are associated with the test conditions and procedures defined in this document, including the methods of arrangement of microphones and the measurement procedures of environmental correction but not with the noise source itself, i.e. variations of installation and operation conditions.</p> <p>NOTE 2 For a family of noise sources, with similar size or similar sound power spectra, and/or several laboratories using the same/similar facilities and instrumentation, the uncertainty associated with interlaboratory variability is less than the values given in this table.</p> <p>NOTE 3 The standard deviations of reproducibility include the standard deviations of repeatability, this uncertainty is usually much smaller than the uncertainty associated with interlaboratory variability.</p> <p>NOTE 4 The standard deviations are applicable to measurements on an individual noise source.</p>		

The measurement uncertainty depends on the standard deviation of reproducibility and on the degree of confidence that is desired. As examples, for a normal distribution of sound power levels, there is 90 % confidence that the true value of the sound power level of a source lies within the range  $\pm 1,64\sigma_R$  of the measured value and 95 % confidence that it lies within the range  $\pm 1,96\sigma_R$  of the measured value.

NOTE For a normal distribution of sound power levels, there is 90 % confidence that the probability of acceptance is 95 % and 95 % confidence that the probability of acceptance is 97,5 %.

### 7.3 Reference box

When defining the dimensions of the reference box, elements protruding from the engine which are not significant radiators of sound energy should be disregarded. For safety reasons, the reference parallelepiped may be made sufficiently large to include danger areas, for example, moving parts of an otherwise stationary machine.

### 7.4 Measurement distance

For noise source of unfavourable acoustic conditions (e.g. there are many reflectors, the background noise is much higher), a shorter measurement distance can be selected. For noise source satisfying the acoustic conditions, a larger measurement distance can be selected.

The recommended measurement distance,  $d$ , is 1,0 m. The selection of measurement distance value from the series: 0,25 m, 0,5 m, 1,0 m, 2,0 m, 4,0 m, 8,8 m takes precedence. The value may also be selected from the following series: 0,25 m, 0,315 m, 0,4 m, ..., 5,0 m, 6,3 m, 8,0 m. The distance between the measurement surface and wall(s) and ceiling should be equal to or greater than 0,25 m.

NOTE For the criterion for position adequacy of microphones, see 7.7.

### 7.5 Measurement surface and area

The parallelepiped measurement surface area,  $S$ , in square metres ( $m^2$ ), is given by [Formula \(4\)](#):

$$S = 4(ab + bc + ca) \tag{4}$$

where

$$a = 0,5l_1 + d ;$$

$$b = 0,5l_2 + d ;$$

$$c = l_3 + d .$$

## 7.6 Microphone positions

Divide each measurement surface into rectangular area units of equal size as few as possible, the maximum length of the side of the area unit is  $r_s d$  ( $r_s$  is size ratio, which is the ratio of the maximum length of the side of the area unit to the measurement distance,  $r_s \leq 3$ ), see [Figure 1](#). The microphone positions specified in this document are located in the centre and corners of each area unit (except those falling into the position of the reflecting plane). Typical examples of the microphone position arrangement are shown in [Figure 2](#) to [Figure 6](#); other types of different number of measurement unit can be obtained by the microphone positions in this way.

NOTE 1 Reducing the value of  $r_s$  until the number of rectangular areas increases to increase the microphone positions can generally reduce the value of  $s(L'_{pAm})$ , see [7.7](#). If necessary, ISO 9614 (all parts) can be used.

NOTE 2 The engine size shown in [Figure 2](#) to [Figure 6](#) is the size relative to the measurement distance, which does not reflect the absolute size.

If the measurements at any position are not permissible due to machine obstructions (driving shaft, driven machinery, etc.) or safety reasons, or are being adversely affected by air flow etc., another position(s) as close as is practicable to the prescribed position(s) shall be selected. Any such revised microphone position(s) shall be recorded [see [Clause 9 d](#)) 2)].

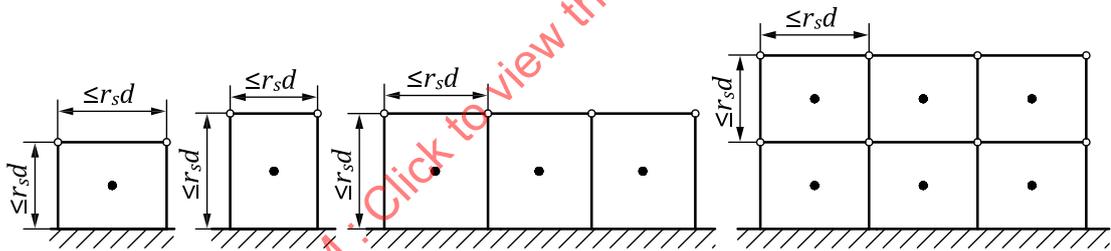
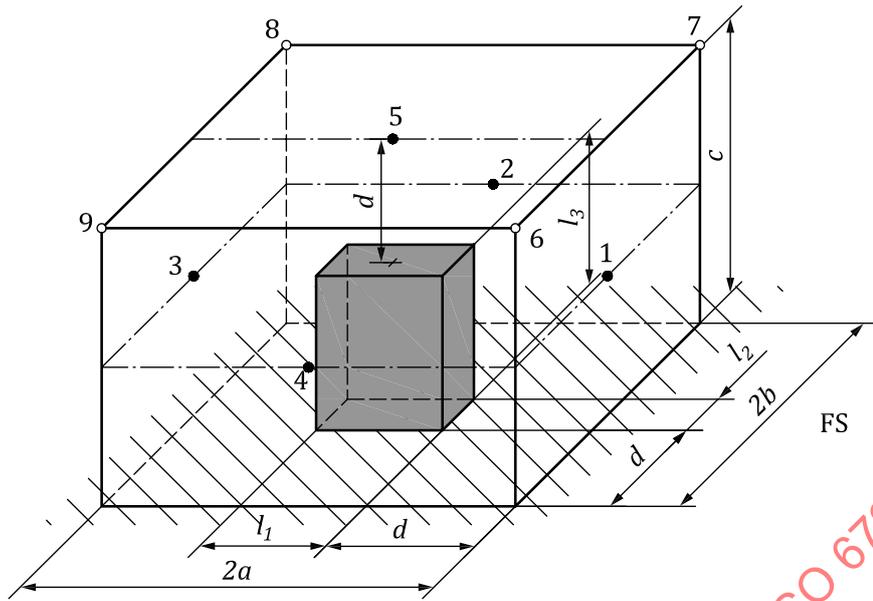
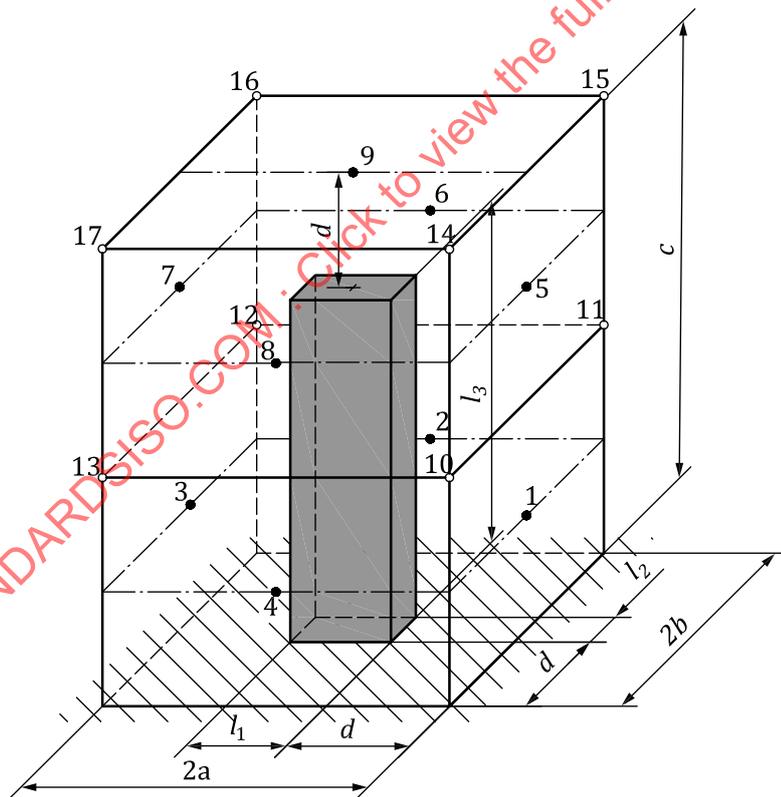


Figure 1 — Microphone positions on the measurement surface



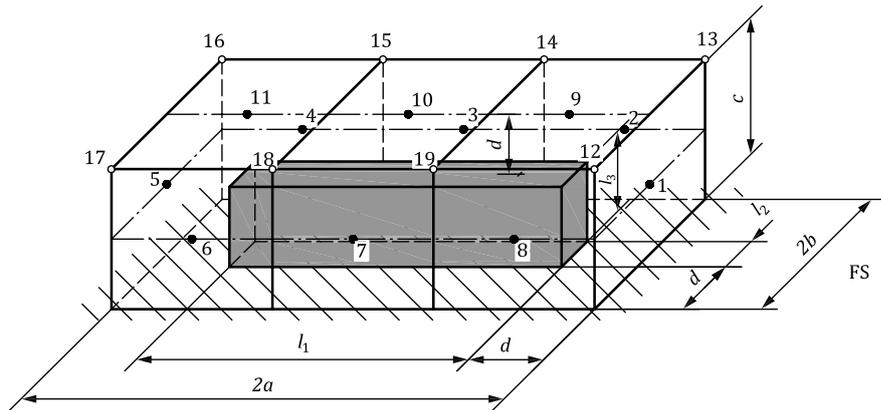
NOTE  $l_1 \leq (r_s - 2) d, l_2 \leq (r_s - 2) d, l_3 \leq (r_s - 1) d$ ; one measurement unit.

Figure 2 — Microphone positions — Small size engine



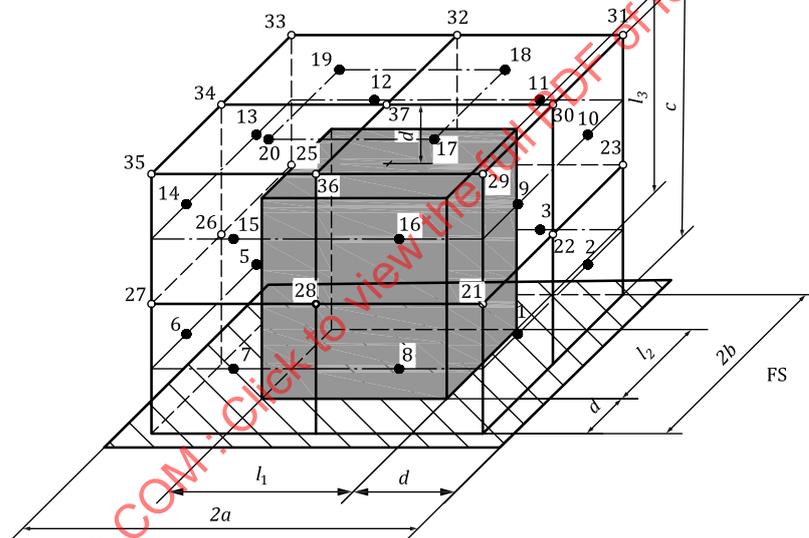
NOTE  $l_1 \leq (r_s - 2) d, l_2 \leq (r_s - 2) d, (r_s - 1) d < l_3 \leq (2r_s - 1) d$ ; two measurement units.

Figure 3 — Microphone positions — Small size erected engine



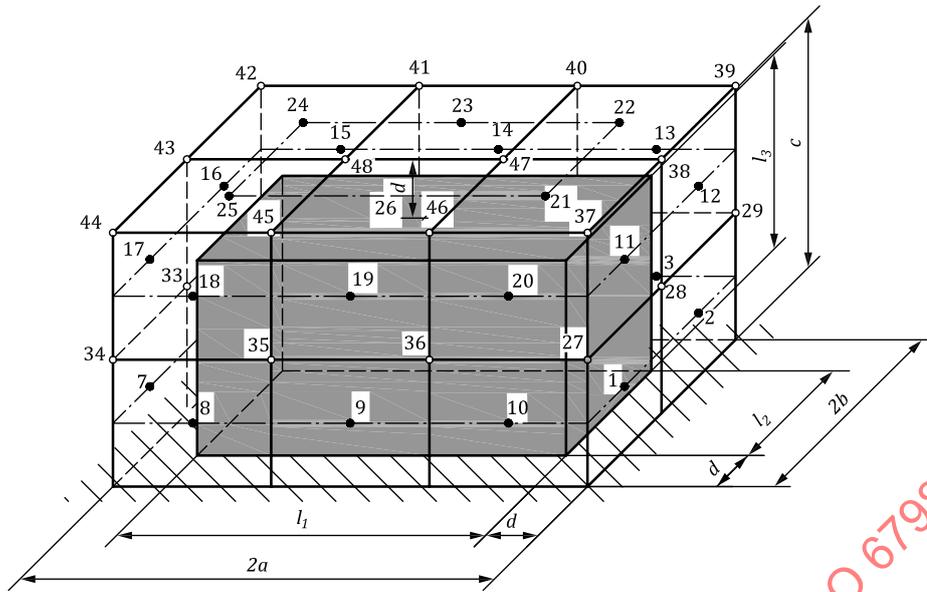
NOTE  $2(r_s - 1) d < l_1 \leq (3r_s - 2) d, l_2 \leq (r_s - 2) d, l_3 \leq (r_s - 1) d$ ; three measurement units.

Figure 4 — Microphone positions — Long size engine



NOTE  $(r_s - 2) d < l_1 \leq 2(r_s - 1) d, (r_s - 2) d < l_2 \leq 2(r_s - 1) d, (r_s - 1) d < l_3 \leq (2r_s - 1) d$ ; eight measurement units.

Figure 5 — Microphone positions — Middle size engine



NOTE  $2(r_s - 1)d < l_1 \leq (3r_s - 2)d$ ,  $(r_s - 2)d < l_2 \leq 2(r_s - 1)d$ ,  $(r_s - 1)d < l_3 \leq (2r_s + 1)d$ ; 12 measurement units.

Figure 6 — Microphone — Large size engine

## 7.7 Criterion for position adequacy of microphones

### 7.7.1 General

If the standard deviation,  $s(L'_{pAm})$ , of the mean sound pressure level (A-weighted) measured in all microphone positions (see 8.2) is less than or equal to 1,0 dB during the engine operation, the criterion for position adequacy of microphones is satisfied. If the standard deviation,  $s(L'_{pAm})$  is larger than 1,0 dB, the measurement is not valid.

NOTE 1 The mean sound pressure level and the surface sound pressure level measured in all microphone positions are not exactly the same. But the standard deviation,  $s(L'_{pAm})$ , of the mean sound pressure level reflects the measurement uncertainty caused by acoustic condition, noise source characteristics, measurement distance, microphone positions and number.

NOTE 2 Increasing the measurement distance and the number of microphone positions can generally reduce the value of  $s(L'_{pAm})$ .

NOTE 3 For  $L'_{pAm}$ , see 8.2.

### 7.7.2 Reduction of microphone positions

In practical measurement, the centre microphone position of each partial area can be only preserved while ignoring the corner microphone positions, but the standard deviation  $s(L'_{pAm})$  of the measured mean sound pressure level shall meet the requirement of 7.7.1. The difference in the surface sound pressure level measured before and after reducing the microphone positions is used as a correction value, the sound power level measurement result given in the final report is the summation of the sound power level that is measured under reduced microphone positions condition and correction value, and the number of measurement points shall be recorded.

## 8 Calculation

### 8.1 General

This clause specifies the calculation methods of the standard deviation of the mean sound pressure level (see 7.7) and the sound power level (A-weighted or frequency-band).

The A-weighted sound power level can also be calculated from frequency band levels in accordance with Annex B which shall be stated in the report.

### 8.2 Calculation of standard deviation of mean sound pressure levels

The mean (arithmetic average) A-weighted sound pressure level,  $L'_{pAm}$  from all microphone positions, expressed in decibels (dB), shall be calculated using Formula (5):

$$L'_{pAm} = \frac{\sum_{i=1}^{N_M} L'_{pAi}}{N_M} \quad (5)$$

where

$L'_{pAi}$  is the sound pressure level measured at the  $i^{\text{th}}$  microphone position with the noise source under test in operation, in decibels (dB);

$N_M$  is the number of microphone positions.

NOTE The subscript A in  $L'_{pAm}$  represents A-weighted, m in  $L'_{pAm}$  represents arithmetic average.

The standard deviation,  $s(L'_{pAm})$ , of the mean A-weighted sound pressure level,  $L'_{pAm}$ , from all microphone positions, expressed in decibels (dB), shall be calculated using Formula (6):

$$s(L'_{pAm}) = \sqrt{\frac{\sum_{i=1}^{N_M} (L'_{pAi} - L'_{pAm})^2}{(N_M - 1)N_M}} \quad (6)$$

If  $s(L'_{pAm}) \leq 1,0$  dB, the measurement is valid. If  $s(L'_{pAm}) > 1,0$  dB, the measurement is not valid. Another measurement surface or a better test environment shall be chosen to carry out the measurement.

### 8.3 Calculation of sound power level

#### 8.3.1 Measured surface time-averaged sound pressure levels

The measured surface time-averaged sound pressure level,  $\overline{L'_p}$  (A-weighted or frequency-band), and the measured surface time-averaged sound pressure level of the background noise,  $\overline{L'_{p(B)}}$  (A-weighted or frequency-band), from the array of microphone positions over the measurement surface shall be calculated using Formula (7) and Formula (8), expressed in decibels (dB).

$$\overline{L'_p} = 10 \times \lg \left[ \frac{1}{N_M} \sum_{i=1}^{N_M} 10^{0,1L'_{pi}} \right] \quad (7)$$

$$\overline{L_{p(B)}} = 10 \times \lg \left[ \frac{1}{N_M} \sum_{i=1}^{N_M} 10^{0,1 L_{pi(B)}} \right] \quad (8)$$

where  $L_{pi(B)}$  is the sound pressure level (A-weighted or frequency-band) of the background noise measured at the  $i^{\text{th}}$  microphone position, in decibels (dB).

### 8.3.2 Corrections for background noise

The background noise correction,  $K_1$  (A-weighted or frequency-band), expressed in decibels (dB), shall be calculated using [Formula \(9\)](#):

$$K_1 = -10 \times \lg \left( 1 - 10^{-0,1 \Delta L_p} \right) \quad (9)$$

where  $\Delta L_p$  is the difference between the measured surface time-averaged sound pressure level (A-weighted or frequency-band) and the surface time-averaged sound pressure level of the background noise (A-weighted or frequency-band) from the array of microphone positions over the measurement surface, with the noise source under test in operation, i.e.  $\Delta L_p = \overline{L'_p} - \overline{L_{p(B)}}$ , in decibels (dB).

If  $\Delta L_{pA} > 15,0$  dB,  $K_{1A}$  is assumed to be zero and no correction for background noise is applied. If  $6,0 \text{ dB} \leq \Delta L_{pA} \leq 15,0$  dB, corrections calculated with [Formula \(9\)](#) shall be applied, i.e.  $0,1 \text{ dB} \leq K_{1A} \leq 1,3$  dB. If  $\Delta L_{pA} < 6,0$  dB, i.e.  $K_{1A} > 1,3$  dB, the measurement is not valid.

NOTE If  $K_{1A} > 1,3$  dB, the measurement results of the sound power level do not satisfy the accuracy grade 2, but the measurement result corrected by  $K_{1A} = 1,3$  can be useful for indicating an upper boundary to the sound power level of the noise source under test.

### 8.3.3 Environmental correction

Determine the environmental correction,  $K_2$  (A-weighted or frequency-band), according to [Annex A](#).

The measurement is valid if  $K_{2A} \leq 4,0$  dB and is not valid if  $K_{2A} > 4,0$  dB.

NOTE If  $K_{2A} > 4,0$  dB, the measurement results of the sound power level do not satisfy the accuracy grade 2, but measurement result corrected by  $K_{2A} = 4,0$  dB can be useful for indicating an upper boundary to the sound power level of the noise source under test.

### 8.3.4 Surface time-averaged sound pressure level

The surface time-averaged sound pressure level,  $\overline{L_p}$  (A-weighted or frequency-band), shall be calculated by correcting the measured surface time-averaged sound pressure level,  $\overline{L'_p}$  (A-weighted or frequency-band), background noise,  $K_1$  (A-weighted or frequency-band), and the influence of the test environment,  $K_2$  (A-weighted or frequency-band), using [Formula \(10\)](#), expressed in decibels (dB).

$$\overline{L_p} = \overline{L'_p} - K_1 - K_2 \quad (10)$$

### 8.3.5 Sound power level

The sound power level,  $L_W$ , expressed in decibels (dB), shall be calculated using [Formula \(11\)](#):

$$L_W = \overline{L_p} + 10 \times \lg(S/S_0) \quad (11)$$

where

$S$  is the area of the measurement surface, in square metres (m<sup>2</sup>);

$S_0$  is equal to 1,0 m<sup>2</sup>.

Atmospheric pressure and/or a temperature create a bias in the radiation of sound power. At altitudes higher than 500 m above sea level and/or temperatures below 10 °C, the sound power levels,  $L_{Wref,atm}$ , corresponding to the reference static pressure 101,325 kPa and reference atmospheric temperature 23 °C shall be calculated in accordance with [Annex C](#) and stated in the report.

## 9 Information to be recorded

The information below marked with \* shall be recorded in the report, others are optional.

### a) Engine under test

- 1) the description of the engine under test including the type\*, specifications (i.e. form\*, number of strokes, number of cylinders, cylinder bore, stroke displacement\*, appearance dimensions, type of cooling\*, ISO standard power\* and corresponding speed\*), serial number\*, and manufacturer\*;
- 2) the type of fuel used and its octane or cetane number;
- 3) the injection timing (static and dynamic) for diesel engines or the ignition timing (static and dynamic) for petrol engines;
- 4) the character of the foundation bed\* and the connection type with the engine\* (elasticity or rigidity);
- 5) the connection type of the engine and the dynamometer\* (elasticity or rigidity);
- 6) the mounting conditions, including height of the crankshaft centre and oil pan bottom above the reflecting plane\*;
- 7) the description of dependent auxiliaries\*, including air filter, exhaust silencer (if any) and cooling fan (if any), encapsulation (if any);
- 8) the engine power\* and the corresponding speed\* of rotation during noise test.

### b) Acoustic environment

- 1) the description of the test environment (including the nature of the floor, walls and ceiling, and the sketch showing the location of the noise source under test and any other contents of the room);
- 2) the description of the acoustical qualification of the test environment\* in accordance with [Annex A](#);
- 3) the description of the ambient conditions near the noise source under test (including the barometric pressure\*, air temperature\*, relative humidity and wind speed\*).

### c) Description of instrumentation

- 1) the equipment used for the measurements\*, including the name, type, serial number, and manufacturer;
- 2) the date\*, place\*, results\* and methods\* used to calibrate the sound calibrator and to verify the calibration of the instrumentation system;

- 3) the characteristics of the microphone windscreen, if any.
- d) Acoustical data
  - 1) the measurement method\* and accuracy grade\*;
  - 2) the dimensions of the reference box\*, measurement distance\*, microphone positions\* and number and revised microphone positions\* (if any, see 7.6);
  - 3) the sound pressure level measured at the  $i^{\text{th}}$  microphone position with the noise source under test in operation\*,  $L'_{pi}$ , and the standard deviation of the averaged sound pressure level\*,  $s(L'_{pAm})$ ;
  - 4) the correction(s) \*,  $K_{1A}$ , to account for background noise;
  - 5) the correction(s)\*,  $K_{2A}$ , to account for the test environment, and the method from [Annex A](#) used to determine it (them)\*;
  - 6) the surface time-averaged sound pressure levels\*,  $\overline{L}_p$  ;
  - 7) the sound power levels\*,  $L_W$ ;
  - 8) the date, place and performing person for the measurements.

## 10 Test report

Test report should record the data and information required in [Clause 9](#) which only provides the measurement results of the sound power level (A-weighted or frequency-band). The report shall specify that the measurement is made in full conformity with the requirements of this document and the test result meets the requirement of accuracy grade 2. The report shall also contain any statements required to be reported in some clauses of this document.

The measurement results of sound power level (A-weighted) in the report should be rounded to the nearest 0,1 dB.

## Annex A (normative)

### Qualification procedures for the acoustic environment

#### A.1 General

This annex specifies procedures to determine the environmental correction,  $K_2$ . These procedures can be used to qualify a given measurement surface of an actual noise source under test.

The first qualification test (absolute comparison test, see [A.2](#)) is carried out with a reference sound source (RSS) and can be used outdoors and indoors. This is the preferred procedure for qualifying a test environment, particularly when data in frequency bands are required, and when the noise source under test can be removed from the test site.

The second qualification test (method based on room absorption, see [A.3](#)) requires the determination of the equivalent absorption area,  $A$ , of the test room, and is based on the assumption that the room is approximately cubic and empty, and that sound is absorbed at the room boundaries.  $A$  can be calculated either by measurements of sound pressure levels from the noise source under test using a secondary measurement surface or by measurements on a reference sound source. If the noise source under test cannot be moved and if its dimensions are large, one of these is the preferred method.

#### A.2 Absolute comparison test

A reference sound source meeting the requirements of ISO 6926 shall be mounted on the ground in the test environment, in essentially the same centre of the undersurface as that of the reference box under test. The measurement surface, microphone positions and number for the reference sound source shall be the same as that of the noise source under test. The sound power level of the reference sound source shall be determined in accordance with the procedure of [Clause 7](#) without the environmental correction,  $K_2$  ( $K_2$  is assumed to be zero).

The environmental correction,  $K_2$ , expressed in decibels (dB), is given by [Formula \(A.1\)](#):

$$K_2 = L_W^* - L_{W(RSS)} \quad (\text{A.1})$$

where

$L_W^*$  is the environmentally uncorrected sound power level of the reference sound source when using the value 0 for  $K_2$ , in decibels (dB);

$L_{W(RSS)}$  is the sound power level of the calibrated reference sound source under the meteorological conditions of the test, in decibels (dB).

### A.3 Determination of the environmental correction based on room absorption

#### A.3.1 General

The environmental correction,  $K_2$ , expressed in decibels (dB), shall be calculated from [Formula \(A.2\)](#):

$$K_2 = 10 \times \lg \left[ 1 + 4 \frac{S}{A} \right] \quad (\text{A.2})$$

where

$A$  is the equivalent sound absorption area of the room, in square metres (m<sup>2</sup>);

$S$  is the area of the measurement surface, in square metres (m<sup>2</sup>).

#### A.3.2 Two-surface method

This test method shall be used only in rooms where  $K_2 \leq 2$  dB.

Two surfaces that surround the noise source shall be selected. The first surface shall be the measurement surface, in accordance with [Clause 7](#), for the determination of the sound power level. The area of the first surface shall be designated  $S_1$ . The second surface with area  $S_2$  shall be geometrically similar to the first surface and located further away and symmetrical with respect to the noise source under test. On both surfaces, the background noise criteria specified in [4.2](#) shall be fulfilled.

The microphone locations on the second surface shall correspond to those on the first surface. The ratio  $S_2/S_1$  shall not be less than 2 and preferably should be greater than 4. The ratio  $S_1/A$  in [Formula \(A.3\)](#) is calculated from:

$$\frac{A}{S_1} = \frac{4(M-1)}{1-M(S_1/S_2)} \quad (\text{A.3})$$

where

$$M = 10^{0,1(\overline{L_{p1}} - \overline{L_{p2}})}$$

where

$\overline{L_{p1}}$  is the surface time-averaged sound pressure level on  $S_1$ , see [Formula \(7\)](#), corrected for background noise but not for the influence of the environment (see [8.3.4](#)), in decibels (dB);

$\overline{L_{p2}}$  is the surface time-averaged sound pressure level on  $S_2$ , see [Formula \(7\)](#), corrected for background noise but not for the influence of the environment (see [8.3.4](#)), in decibels (dB);

$S_1$  is the area of the first measurement surface, in square metres (m<sup>2</sup>);

$S_2$  is the area of the second measurement surface, in square metres (m<sup>2</sup>).

The environmental correction  $K_2$  for A-weighting or in frequency bands is obtained from [Formula \(A.2\)](#), with the  $S_1/A$  ratio calculated from [Formula \(A.3\)](#).

#### A.3.3 Determination of the equivalent absorption area $A$ with a reference sound source

A reference sound source meeting the requirements of ISO 6926 shall be mounted on the ground in the test environment and hemi-anechoic room respectively, in essentially the same centre of the undersurface as that of the reference box under test, the same measurement surface, the same microphone positions and number as that of the noise source under test. The sound power level of the reference sound source shall be determined in accordance with the procedure in [Clause 7](#) without the environmental correction ( $K_2$  is assumed to be zero).

The environmental correction of the measurement surface,  $K_2$ , expressed in decibels (dB), is given by [Formula \(A.4\)](#):

$$K_2 = L_W^* - L_{W(SA)} \quad (\text{A.4})$$

where

$L_W^*$  is the environmentally uncorrected sound power level of the reference sound source when using the value 0 for  $K_2$ , in decibels (dB);

$L_{W(SA)}$  is the sound power level of the reference sound source measured in hemi-anechoic room under the meteorological conditions of the test, in decibels (dB).

The equivalent absorption area,  $A$ , is then calculated using [Formula \(A.5\)](#):

$$A = \frac{4S}{10^{0,1K_2} - 1} \quad (\text{A.5})$$

where  $S$  is the area of the measurement surface, in square metres (m<sup>2</sup>)

Then the environmental correction  $K_2$  of other measurement surface is obtained from [Formula \(A.2\)](#).

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