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**Internal combustion engines — Piston  
rings —**

**Part 4:  
General specifications**

*Moteurs à combustion interne — Segments de piston —  
Partie 4: Spécifications générales*

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## Foreword

ISO (the International Organization for Standardization) is a worldwide federation of national standards bodies (ISO member bodies). The work of preparing International Standards is normally carried out through ISO technical committees. Each member body interested in a subject for which a technical committee has been established has the right to be represented on that committee. International organizations, governmental and non-governmental, in liaison with ISO, also take part in the work. ISO collaborates closely with the International Electrotechnical Commission (IEC) on all matters of electrotechnical standardization.

The procedures used to develop this document and those intended for its further maintenance are described in the ISO/IEC Directives, Part 1. In particular the different approval criteria needed for the different types of ISO documents should be noted. This document was drafted in accordance with the editorial rules of the ISO/IEC Directives, Part 2 (see [www.iso.org/directives](http://www.iso.org/directives)).

Attention is drawn to the possibility that some of the elements of this document may be the subject of patent rights. ISO shall not be held responsible for identifying any or all such patent rights. Details of any patent rights identified during the development of the document will be in the Introduction and/or on the ISO list of patent declarations received (see [www.iso.org/patents](http://www.iso.org/patents)).

Any trade name used in this document is information given for the convenience of users and does not constitute an endorsement.

For an explanation on the meaning of ISO specific terms and expressions related to conformity assessment, as well as information about ISO's adherence to the WTO principles in the Technical Barriers to Trade (TBT), see the following URL: Foreword — Supplementary information.

The committee responsible for this document is ISO/TC 22, *Road vehicles*.

This third edition cancels and replaces the second edition (ISO 6621-4:2003), which has been technically revised.

ISO 6621 consists of the following parts, under the general title *Internal combustion engines — Piston rings*:

- *Part 1: Vocabulary*
- *Part 2: Inspection measuring principles*
- *Part 3: Material specifications*
- *Part 4: General specifications*
- *Part 5: Quality requirements*

## Introduction

ISO 6621 is one of a series of International Standards dealing with piston rings for reciprocating internal combustion engines. Others are ISO 6622-1, ISO 6622-2, ISO 6623, ISO 6624-1, ISO 6624-2, ISO 6624-3, ISO 6624-4, ISO 6625, ISO 6626-1, ISO 6626-2, ISO 6626-3, and ISO 6627.

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# Internal combustion engines — Piston rings —

## Part 4: General specifications

### 1 Scope

This part of ISO 6621 specifies the general characteristics of piston rings for reciprocating internal combustion engines for road vehicles and other applications (the individual dimensional criteria for these rings are given in the relevant International Standards). It also provides a system for ring coding, designation, and marking. It is applicable to all such rings of a nominal diameter from 30 mm up to and including 200 mm.

### 2 Normative references

The following documents, in whole or in part, are normatively referenced in this document and are indispensable for its application. For dated references, only the edition cited applies. For undated references, the latest edition of the referenced document (including any amendments) applies.

ISO 6507-3, *Metallic materials — Vickers hardness test — Part 3: Calibration of reference blocks*

ISO 6621-1, *Internal combustion engines — Piston rings — Part 1: Vocabulary*

ISO 6621-2, *Internal combustion engines — Piston rings — Part 2: Inspection measuring principles*

### 3 Terms and definitions

For the purposes of this document, the terms and definitions given in ISO 6621-1 apply.

### 4 Piston ring codes

Codes used for piston rings shall be as given in [Table 1](#), corresponding to their explanatory descriptions.

**Table 1 — Codes and descriptions in alphabetical order**

Code	Description	Relevant International Standard
B	Barrel-faced rectangular ring	ISO 6622-1, ISO 6622-2
BA	Asymmetrical barrel-faced rectangular ring	ISO 6622-1, ISO 6622-2
CR1E ... CR2E	Peripheral surface chromium plated semi-inlaid design	ISO 6621-4
CR1F ... CR2F	Peripheral surface chromium plated inlaid design	ISO 6621-4
CRF ... CR4	Peripheral surface chromium plated fully faced design	ISO 6621-4
CSN, CSG, CSE	Type of coil spring	ISO 6626-1, ISO 6626-2
D	Bevelled edge oil control ring	ISO 6625
D22	Radial wall thickness for "d1/22"	ISO 6622-1, ISO 6623

<sup>a</sup> Material mark (for alternative materials) at the discretion of the manufacturer.

<sup>b</sup> Any other additional marking on customer's request, which shall be quoted clearly in the order, shall be agreed upon between manufacturer and customer.

Table 1 (continued)

Code	Description	Relevant International Standard
DSF	Coil spring loaded bevelled edge oil control ring	ISO 6626-1, ISO 6626-2
DSF-C	Coil spring loaded bevelled edge oil control ring, chromium plated, and profile ground	ISO 6626-1, ISO 6626-2
DSF-CNP	Coil spring loaded bevelled edge oil control ring, chromium plated, not profile ground	ISO 6626-1
DSF-NG	Coil spring loaded bevelled edge oil control ring (face geometry similar type DSF-C or DSF-CNP)	ISO 6626-1
DV	Bevelled edge V-groove oil control ring	ISO 6625
E	Scraper ring (stepped)	ISO 6623
EM1 ... EM4	Scraper ring (stepped), taper-faced	ISO 6623
ES-1 ... ES-4	Expander/segment oil control rings	ISO 6627
FE	Ferro oxidized on all sides	ISO 6621-4
G	Double bevelled oil control ring	ISO 6625
GSF	Coil spring loaded double bevelled oil control ring	ISO 6626-1, ISO 6626-2
HK	Straight faced half keystone ring 7°	ISO 6624-2, ISO 6624-4
HKB	Barrel faced half keystone ring 7°	ISO 6624-2, ISO 6624-4
HKBA	Asymmetrical barrel-faced half keystone ring	ISO 6624-2, ISO 6624-4
HOL	Openings in oil rings in form of holes	ISO 6626-2
IF	Internal bevel (top side)	ISO 6622, ISO 6624-1, ISO 6624-3
IFU	Internal bevel (bottom side)	ISO 6622
IFV	Variable internal bevel (top side) for defined twist	ISO 6622-1
IFVU	Variable internal bevel (bottom side) for defined twist	ISO 6622-1
IW	Internal step (top side)	ISO 6622-1, ISO 6624-1
IWU	Internal step (bottom side)	ISO 6622-1
K	Straight-faced keystone ring 15°	ISO 6624-1, ISO 6624-3
KA	Peripheral edges chamfered	ISO 6622
KB	Barrel-faced keystone ring 15°	ISO 6624-1, ISO 6624-3
KBA	Asymmetrical barrel-faced keystone ring 15°	ISO 6624-1, ISO 6624-3
KG	Reduced size of peripheral edges at the gap of chromium plated/spray coated/nitrided/PVD coated rings	ISO 6621-4
KI	Inside edges chamfered	ISO 6622
KM1 ... KM5	Taper-faced keystone ring 15°	ISO 6624-1, ISO 6624-3
KU	Reduced peripheral bottom edge chromium plated fully faced design	ISO 6621-4
LF	Uncoated ring peripheral surface or uncoated land peripheral surface, fully lapped	ISO 6621-4
LM	Taper-faced piston ring with partly cylindrical machined peripheral surface	ISO 6621-4

<sup>a</sup> Material mark (for alternative materials) at the discretion of the manufacturer.

<sup>b</sup> Any other additional marking on customer's request, which shall be quoted clearly in the order, shall be agreed upon between manufacturer and customer.

Table 1 (continued)

Code	Description	Relevant International Standard
LP	Taper-faced piston ring with lapped land over the whole circumference but not over the whole width of the peripheral surface	ISO 6621-4
M1 ...M5	Taper-faced rectangular ring	ISO 6622-1, ISO 6622-2
MC11 ... MC68	Material subclasses	ISO 6621-3
MM	Manufacturer's mark	ISO 6621-4
MR	Reduced ratio $m/(d_1 - a_1)$ for reduced load	ISO 6621-4
MU	Any other additional mark <sup>b</sup>	ISO 6621-4
MX	Material mark <sup>a</sup>	ISO 6621-4
MY	Mark for required ring shape "negative ovality"	ISO 6621-4
MZ	Mark for required ring shape "round"	ISO 6621-4
N	Napier ring (undercut step)	ISO 6623
NB030 ... NB130	Nitrided surface, case depth specified on peripheral surface and bottom side	ISO 6621-4
NE1 ... NE3	Ring joint with lateral stop	ISO 6621-4
NH1 ... NH3	Ring joint with internal stop	ISO 6621-4
NM1 ... NM4	Napier ring (undercut step), taper-faced	ISO 6623
NP030 ... NP130	Nitrided surface, case depth specified on peripheral surface only	ISO 6621-4
NS 010 ... NS 050	Nitrided surface, case depth on segments	ISO 6627
NT030 ... NT130	Nitrided surface, case depth specified on peripheral surface and side faces	ISO 6621-4
NX	Nitrided surface of expanders/spacers	ISO 6627
PC001...PC040	Physical vapour deposition coating (PVD) thickness	ISO 6621-4
PN 10...PN 25	Nominal contact pressure classes	ISO 6626-3
PNE, PNL, PNR, PNM, PNH, PNV	Contact pressure class	ISO 6626-1, ISO 6626-2, ISO 6627
PO	Phosphated on all sides	ISO 6621-4
PR	Phosphated on all sides (for rust protection purposes)	ISO 6621-4
R	Straight-faced rectangular ring	ISO 6622-1, ISO 6622-2
RU	Napier ring with reduced undercut or step	ISO 6623
S	Slotted oil control ring	ISO 6625
S005 ... S100	Closed gap (minimum values)	ISO 6621-4
SC1 ... SC4	Peripheral surface spray coated fully faced design	ISO 6621-4
SC1E ... SC4E	Peripheral surface spray coated semi-inlaid design	ISO 6621-4
SC1F ... SC4F	Peripheral surface spray coated inlaid design	ISO 6621-4
SSF	Coil spring loaded slotted oil control ring	ISO 6626-1, ISO 6626-2
SSF-L	Coil spring loaded slotted oil control ring with 0,6 mm nominal land width	ISO 6626-1, ISO 6626-2
<sup>a</sup> Material mark (for alternative materials) at the discretion of the manufacturer. <sup>b</sup> Any other additional marking on customer's request, which shall be quoted clearly in the order, shall be agreed upon between manufacturer and customer.		

Table 1 (continued)

Code	Description	Relevant International Standard
T	Straight-faced keystone ring 6°	ISO 6624-1, ISO 6624-3
TB	Barrel-faced keystone ring 6°	ISO 6624-1, ISO 6624-3
TBA	Asymmetrical barrel-faced keystone ring 6°	ISO 6624-1, ISO 6624-3
TM1 ... TM5	Taper-faced keystone ring 6°	ISO 6624-1, ISO 6624-3
TT	Seating tab angle $\theta$	ISO 6627
WF	Reduced heat set	ISO 6621-5, ISO 6626-1, ISO 6626-2
WK	Reduced slot length	ISO 6626-1, ISO 6626-2
WTL	Radial wall thickness (large)	ISO 6626-3
WTS	Radial wall thickness (small)	ISO 6626-3
Y	Ring shape negative ovality	ISO 6621-4
Z	Ring shape round	ISO 6621-4
<p><sup>a</sup> Material mark (for alternative materials) at the discretion of the manufacturer.</p> <p><sup>b</sup> Any other additional marking on customer's request, which shall be quoted clearly in the order, shall be agreed upon between manufacturer and customer.</p>		

## 5 Designation of piston rings

### 5.1 Designation elements and order

#### 5.1.1 General

When designating piston rings complying with the relevant International Standards, the following details shall be provided in the order given, using the codes according to [Table 1](#).

#### 5.1.2 Mandatory elements

The following mandatory elements shall constitute the designation of a piston ring:

- designation (i.e. piston ring);
- number of International Standard;
- type of piston ring (e.g. R);
- hyphen;
- size of piston ring,  $d_1 \times h_1$ ;
- radial wall thickness "regular" without code;
- Code D22 if the selected wall thickness, in accordance with ISO 6622-1 and ISO 6623, is  $d_1/22$ ;
- hyphen;
- material code (e.g. MC11).

### 5.1.3 Additional elements

The following optional elements may be added to the designation of a piston ring and, if so added, shall be positioned on a second line beneath or separated by a slash (/) from the mandatory elements given in [5.1.2](#):

- reduced ratio  $m/(d_1 - a_1)$ , MR;
- ring shape (e.g. Z);
- selected nominal closed gap if it differs from the closed gap specified in the dimension tables (e.g. S05);
- the selected coating (e.g. CR3);
- uncoated rings with fully lapped peripheral surface [e.g. for LF taper faced rings with partly cylindrical peripheral surface, LM (machined), or LP (lapped)];
- selected surface treatment (e.g. PO);
- selected inside edge feature (e.g. KA);
- inside step of bevel (e.g. IWU);
- selected notch to prevent ring rotation (e.g. NH1);
- reduced slot length, if required (e.g. WK);
- coil spring with reduced heat set, if required, (e.g. WF);
- selected type of coil spring, (e.g. CSG);
- selected pressure class (e.g. PNM).

### 5.1.4 Elements for additional marking

Any additional marking shall be the following with the additional elements of [5.1.3](#):

- manufacturer's mark, if required (e.g. MM);
- marking of required ring shape (e.g. MZ);
- material, MX (see [Table 1](#), Footnote a);
- code for any other marking, MU (see [Table 1](#), Footnote b).

## 5.2 Designation examples

### 5.2.1 Designation example of a piston ring in accordance with ISO 6622-1

For a straight-faced rectangular ring (R) of nominal diameter  $d_1 = 90$  mm (90) and nominal ring width  $h_1 = 2,5$  mm (2,5), made of grey cast iron, non heat treated material subclass 11 (MC11):

**Piston ring ISO 6622-1 R - 90 × 2,5 - MC11.**

Parameters in parentheses are used in the ISO ring designation.

### 5.2.2 Designation example of a piston ring in accordance with ISO 6624-1

For a keystone ring  $6^\circ$ , taper faced  $60'$  (TM3) of nominal diameter  $d_1 = 105$  mm (105) and nominal ring width  $h_1 = 2,5$  mm (2,5) made of spheroidal graphite cast iron, martensitic type, material subclass 51

(MC51), ring shape round (Z) with a selected closed gap of 0,3 mm (S030), inside edges chamfered (KI), and peripheral surface chromium plated, with plating thickness 0,1 mm minimum (CR2):

**Piston ring ISO 6624-1 TM3 – 105 × 2,5 – MC51 / Z S030 KI CR2**

Parameters in parentheses are used in the ISO ring designation.

**5.2.3 Designation example of a piston ring in accordance with ISO 6626-1**

For a coil spring loaded, bevelled edge oil control ring, chromium plated and profile ground (DSF-C), with nominal diameter  $d_1 = 125$  mm (125) and nominal ring width  $h_1 = 5$  mm (5) made of grey cast iron, non heat treated, material subclass 11 (MC11) with a selected closed gap of 0,2 mm (S020) having a chromium plating thickness on the lands of 0,15 mm minimum (CR3), phosphated on all cast iron surfaces to a depth of 0,002 mm minimum (PO) with reduced slot length (WK), a coil spring with reduced heat set (WF) having a variable pitch with coil diameter,  $d_7$  ground (CSE), tangential force,  $F_t$ , according to the medium nominal contact pressure class (PNM) marked with manufacturer's mark (MM):

**Piston ring ISO 6626-1 DSF-C – 125 × 5 – MC11 / S020 CR3 PO WK WF CSE PNM MM**

Parameters in parentheses are used in the ISO ring designation.

**6 Marking of piston rings**

**6.1 General**

The requirements and recommendations for piston ring marking according to 6.2 and 6.3 apply to piston rings of 1,6 mm radial wall thickness and above. Marking of piston rings of less than 1,6 mm is at the discretion of the manufacturer.

**6.2 Mandatory topside identification marking**

All rings requiring orientation shall be marked to indicate the top side only (i.e. the side nearest the combustion chamber).

In the absence of any other mark agreed upon between manufacturer and customer, the mark "TOP" should be used.

Marking of the top side applies to *all* the following types of ring:

- taper faced rings;
- asymmetrical barrel-faced rings;
- rings with reduced peripheral bottom edge;
- internally bevelled or stepped rings;
- semi-inlaid rings;
- scraper rings;
- half keystone rings;
- directional oil control rings.

All such rings requiring marking are specified in the relevant International Standards (see Foreword and Bibliography).

### 6.3 Additional marking

**6.3.1** Additional marking of piston rings is optional or at the customer's request. Such additional marking may comprise of the following:

- manufacturer's mark;
- mark for required ring shape;
- oversize rings;
- material mark (for alternative materials);
- any other additional mark agreed upon between manufacturer and customer.

**6.3.2** Colour marking on the running surface is in common use. Colour marking may be used to identify the following:

- assembling orientation;
- groove assignment;
- oversize diameters;
- supplier identification;
- engine identification.

The choice of colour and acceptance conditions may be agreed upon between ring manufacturer and customer.

## 7 General characteristics

### 7.1 Ring shape

Degrees of ovality only apply to rectangular rings,[1] [2] scraper rings,[3] and keystone rings.[4] [5] [6] [7] The following are forms of ovality:

- positive ovality, without code;
- round, Code Z;
- negative ovality, Code Y.

Values are given in [Table 2](#).

**Table 2 — Ovality**

Dimensions in millimetres

Nominal diameter $d_1$	Positive ovality	Round <sup>a</sup> Code: Z	Negative ovality <sup>b</sup> Code: Y
$30 \leq d_1 < 60$	0 ... +0,60	-0,30 ... +0,30	-0,60 ... 0
$60 \leq d_1 < 100$	+0,05 ... +0,85	-0,35 ... +0,35	-0,70 ... 0
$100 \leq d_1 < 150$	+0,10 ... +1,10	-0,45 ... +0,45	-0,95 ... -0,05
$150 \leq d_1 \leq 200$	+0,15 ... +1,35	-0,50 ... +0,50	-1,10 ... -0,10

<sup>a</sup> For taper-faced coated and uncoated rings with lapped land, the recommended ring shape is round.

<sup>b</sup> Not applicable for material Class 10 of ISO 6621-3.

## 7.2 Light tightness

At least 90 % of the circumference of the piston ring peripheral surface shall be light-tight.

At least 95 % of the circumference on the peripheral surface of a taper-faced ring with plated/coated or nitrided and ground peripheral surface shall be light-tight.

100 % of the circumference on the peripheral surface of the following piston ring designs shall be light-tight:

- piston rings with machined land over the whole circumference of the peripheral surface;
- taper-faced piston rings with machined land over the whole circumference of the peripheral surface.

In the case of piston rings with a treated surface, the light tightness is normally measured prior to surface treatment. When it is checked after treatment, rotation of the ring in the gauge will be required. In the case of rings with negative point deflection, visible light is permitted at the butt ends but should be confined to the angle  $\theta$  as defined in ISO 6621-2.

## 7.3 Closed gap

Whenever the selected closed gap differs from that given in the dimensional tables of the relevant International Standard, [Table 3](#) shall apply and the tolerances shall remain the same.

**Table 3 — Closed gap**

Dimensions in millimetres

Code	S005	S010	S015	S020	S025	S030	S035	S040	S045	S050	S055	S060	S070	S080	S090	S100
<b>Closed gap</b>	0,05	0,10	0,15	0,20	0,25	0,30	0,35	0,40	0,45	0,50	0,55	0,60	0,70	0,80	0,90	1,00

## 7.4 Tangential force, $F_t$ , and diametral force, $F_d$ , of single piece piston rings

NOTE The individual types of piston rings are given in Reference [1] to Reference [8]. The definitions of  $F_t$  and  $F_d$  are given in ISO 6621-2.

### 7.4.1 Calculation of $F_t$ and $F_d$ values in dimension tables of dimensional standards

The tangential and diametral forces of piston rings are tabulated in the dimension tables of the dimensional standards.

The values are calculated for the following:

- the basic feature of each piston ring type;
- nominal radial wall thickness  $a_1$ , and mean ring width  $h_1$  or  $h_3$ ;
- piston rings made of cast iron with a modulus of elasticity of 100 GN/m<sup>2</sup> (100 GN/m<sup>2</sup> = 100 000 MPa = 100 000 N/mm<sup>2</sup>);
- piston rings made of steel with a modulus of elasticity of 210 GN/m<sup>2</sup>;
- ratio of total free gap to nominal diameter [ $m/(d_1 - a_1)$ ], according to [Table 4](#).

NOTE The calculation of tangential forces and diametral forces of rectangular rings made of steel (ISO 6622-2) is based on a theoretical contact pressure of  $0,16 \pm 0,01$  N/mm<sup>2</sup>. The calculation of tangential forces and diametral forces of keystone rings (ISO 6624-3) and half keystone rings (ISO 6624-4) made of steel is based on the same ratio  $m/(d_1 - a_1)$  used for rectangular rings (ISO 6622-2). The ratio  $m/(d_1 - a_1)$  for rings made of steel is quite different from the values given in [Table 5](#) for rings made of cast iron and depends on the nominal diameter and the special radial wall thickness. This radial wall thickness is not in a constant ratio to nominal diameter because there are steps of wall thickness which belong to a range of nominal diameters (e.g.  $a_1 = 2,1$  mm for  $d_1 = 57 \dots 61$  mm).

## 7.4.2 Correction of $F_t$ and $F_d$ values

### 7.4.2.1 General

The  $F_t$  and  $F_d$  values shall be corrected whenever the following are being used:

- a) additional features such as rings with
  - coated peripheral surface, and/or
  - inside chamfered edges, and/or
  - outside chamfered edges, and/or
  - taper, and/or
  - internal step or internal bevel;
- b) piston ring materials with a modulus of elasticity other than 100 GN/m<sup>2</sup>;
- c) ratio of total free gap to nominal diameter [ $m/(d_1 - a_1)$ ] other than that given in [Table 4](#).

The values for the regular ratio of free gap to nominal diameter  $m/(d_1 - a_1)$  regular are given in [Table 4](#).

**Table 4 — Regular ratio of total free gap to nominal diameter**

Dimensions in millimetres

Nominal diameter $d_1$	$m/(d_1 - a_1)$	
	Cast iron	Steel <sup>a</sup>
$30 \leq d_1 < 60$	0,15	0,10 ... 0,14
$60 \leq d_1 < 100$		
$100 \leq d_1 < 160$	0,17 to 0,000 2 $d_1$	0,11 ... 0,13
$160 \leq d_1 \leq 200$		
<sup>a</sup> Variation of $m/(d_1 - a_1)$ depends on contact pressure and radial wall thickness.		

### 7.4.2.2 Multiplier factors for common features

For common features, the necessary multiplier correction factors are tabulated in the dimensional standards Reference [1] to Reference [8], under "Force factors".

### 7.4.2.3 Multiplier force correction factors for materials

For materials specified in ISO 6621-3, the force correction factors given in [Table 5](#) should be used.

**Table 5 — Material force correction factors**

Material class	Material force correction factor
10	0,9 to 1 <sup>a</sup>
20	1,1 to 1,3 <sup>a</sup>
<sup>a</sup> Force correction factors for material depend on the modulus of elasticity in the manufacturer's material specification:	
Correction factor = $\frac{\text{Typical modulus of elasticity in GN/m}^2}{100 \text{ GN/m}^2}$ .	

**Table 5** (continued)

Material class	Material force correction factor
30	1,45
40	1,6
50	1,6
<p><sup>a</sup> Force correction factors for material depend on the modulus of elasticity in the manufacturer's material specification:</p> $\text{Correction factor} = \frac{\text{Typical modulus of elasticity in GN/m}^2}{100 \text{ GN/m}^2}$	

#### 7.4.2.4 Multiplier force correction factors for ratio $m/(d_1 - a_1)$

Piston rings made of materials in Class 30 to Class 50 increase the tangential force and diametral force in relationship to the modulus of elasticity (see [Table 5](#)) when ratio  $m/(d_1 - a_1)$  regular is used.

For limitation of such increased forces, it is common to use reduced values of  $m/(d_1 - a_1)$ . See [Table 6](#) for the recommended correction factors  $m/(d_1 - a_1)$  regular and  $m/(d_1 - a_1)$  reduced.

**Table 6** — Force correction factors for ratio  $m/(d_1 - a_1)$ 

Material class	Factor	
	$m/(d_1 - a_1)$ regular	$m/(d_1 - a_1)$ reduced Code: MR
10	1	—
20	1	—
30	1	0,825
40	1	0,75
50	1	0,75
<p>NOTE For the calculation of the real force correction values, the correction factor for the material given in <a href="#">Table 5</a> shall be applied first, and then the correction factor of <a href="#">Table 6</a> shall be applied.</p>		

#### 7.4.3 Examples for correction of $F_t$ and $F_d$

##### 7.4.3.1 First example — Selected piston ring type: ISO 6622-1 B - 95 × 2,5 - MC53 / MR CR2 IW

###### 7.4.3.1.1 Multiplying factors

- 1,6 for material Subclass 53
- 0,75 for ratio  $m/(d_1 - a_1)$  reduced
- 0,88 for peripheral surface chromium plated CR2
- 0,78 for internal step IW

###### 7.4.3.1.2 Calculation

Total force correction factors:  $1,6 \times 0,75 \times 0,88 \times 0,78 = 0,824$ .

Basic values  $F_t$  and  $F_d$  according to ISO 6622-1:  $F_t = 18,5$  N and  $F_d = 39,8$  N.

Corrected values:  $F_t = 0,824 \times 18,5 \text{ N} \pm 20 \%$  and  $F_d = 0,824 \text{ N} \times 39,8 \text{ N} \pm 20 \%$ ;

$$F_t = 15,2 \text{ N} \pm 20 \text{ and } F_d = 32,8 \text{ N} \pm 20 \%$$

$$F_t = 12,2 \text{ N} \dots 18,2 \text{ N} \text{ and } F_d = 26,2 \text{ N} \dots 39,4 \text{ N}.$$

#### 7.4.3.2 Second example — Selected piston ring type: ISO 6623 N - 70 × 2 D22 - MC24 / SC2F

##### 7.4.3.2.1 Multiplying factors

- 1,15 for material subclass 24
- 1 for ratio  $m/(d_1 - a_1)$  regular
- 0,9 for peripheral surface spray coated SC2F (inlaid type)

##### 7.4.3.2.2 Calculation

Total force correction factor:  $1,15 \times 1 \times 0,9 = 1,035$ .

Basic values  $F_t$  and  $F_d$  according to ISO 6623:  $F_t = 9,3 \text{ N}$  and  $F_d = 20,0 \text{ N}$ .

Corrected values:  $F_t = 1,035 \text{ N} \times 9,3 \text{ N} \pm 30 \%$  and  $F_d = 1,035 \text{ N} \times 20,0 \text{ N} \pm 30 \%$ ;

$$F_t = 9,6 \text{ N} \pm 30 \% \text{ and } F_d = 20,7 \text{ N} \pm 30 \%$$

$$F_t = 6,7 \text{ N} \dots 12,5 \text{ N} \text{ and } F_d = 14,5 \text{ N} \dots 26,9 \text{ N}.$$

#### 7.4.3.3 Third example — Selected piston ring type: ISO 6624-1 KB - 140 × 4 - MC42 / SC4 KI

##### 7.4.3.3.1 Multiplying factors

- 1,6 for material subclass 42
- 0,85 for peripheral surface spray coated SC4 (fully faced type)
- 0,96 for inside chamfered edges KI

##### 7.4.3.3.2 Calculation

Total force correction factor:  $1,6 \times 0,85 \times 0,96 = 1,306$ .

Basic values  $F_t$  and  $F_d$  according to ISO 6624-1:  $F_t = 29,3 \text{ N}$  and  $F_d = 63 \text{ N}$ .

Corrected values:  $F_t = 1,306 \times 29,3 \text{ N} \pm 20 \%$  and  $F_d = 1,306 \times 63 \text{ N} \pm 20 \%$ ;

$$F_t = 38,3 \text{ N} \pm 20 \% \text{ and } F_d = 82,3 \text{ N} \pm 20 \%$$

$$F_t = 30,6 \text{ N} \dots 46,0 \text{ N} \text{ and } F_d = 65,8 \text{ N} \dots 98,8 \text{ N}.$$

#### 7.4.3.4 Fourth example — Selected piston ring type: ISO 6625 G - 120 × 5 - MC11 / KI

##### 7.4.3.4.1 Multiplying factors

- 0,9 for material subclass 11
- 0,98 for inside chamfered edges, KI

#### 7.4.3.4.2 Calculation

Total force correction factor:  $0,9 \times 0,98 = 0,882$ .

Basic values  $F_t$  and  $F_d$  according to ISO 6625:  $F_t = 24,7$  N and  $F_d = 53,1$  N.

Corrected values:  $F_t = 0,882 \times 24,7$  N  $\pm 20$  % and  $F_d = 0,882 \times 53,1$  N  $\pm 20$  %;

$$F_t = 21,8 \text{ N} \pm 20 \text{ \% and } F_d = 46,8 \text{ N} \pm 20 \text{ \%};$$

$$F_t = 17,4 \text{ N} \dots 26,2 \text{ N and } F_d = 37,4 \text{ N} \dots 56,2 \text{ N}.$$

### 7.5 Tangential force $F_t$ of multipiece oil control rings as specified in ISO 6626-1, ISO 6626-2, and ISO 6626-3

#### 7.5.1 General

The tangential force of a coil spring loaded oil control ring depends on the following:

- piston ring type;
- class of nominal contact pressure;
- specific tangential force  $F_{tc}$  for unit contact pressure of forces, tabulated in ISO 6626-1 and ISO 6626-2.

NOTE The formula for calculating the actual tangential force is also given in ISO 6626-1 and ISO 6626-2.

#### 7.5.2 Rounding of values

Actual values of tangential force should be rounded up or down as follows:

- $F_t < 50$  N, to the nearest 0,5 N;
- $F_t > 50$  N, to the nearest 1 N, where 0,5 N is rounded up.

#### 7.5.3 Examples for calculating tangential force $F_t$

##### 7.5.3.1 First example — Selected piston ring type: ISO 6626-1 DSF-C - 100 × 4 - MC11/CR1 CSG PNM

##### 7.5.3.1.1 Pressure class and specific tangential force

Class of nominal contact pressure:  $PNM = 1,49$  N/mm<sup>2</sup>.

Specific tangential force for unit contact pressure of 1 N/mm<sup>2</sup>:  $F_{tc} = 40,4$  N.

##### 7.5.3.1.2 Calculation

Tangential force:  $F_t = 1,49$  N  $\times 40,4$  N  $\pm 20$  %;

$$F_t = 60,2 \text{ N} \pm 20 \text{ \%};$$

$$F_t = 48 \text{ N} \dots 72 \text{ N}.$$

### 7.5.3.2 Second example — Selected type of piston ring: ISO 6626-1 SSF - 175 × 6 - MC11/CSG PNE

#### 7.5.3.2.1 Pressure class and specific tangential force

Class of nominal contact pressure:  $PNE = 0,59 \text{ N/mm}^2$ .

Specific tangential force for unit contact pressure of  $1 \text{ N/mm}^2$ :  $F_{tc} = 192,5 \text{ N}$ .

#### 7.5.3.2.2 Calculation

Tangential force:  $F_t = 0,59 \times 192,5 \text{ N} \pm 20 \%$ ;

$$F_t = 113,6 \text{ N} \pm 20 \%$$

$$F_t = 91 \text{ N} \dots 136 \text{ N}.$$

## 7.6 Tangential force $F_t$ of expander/segment oil control rings as specified in ISO 6627

### 7.6.1 General

The tangential force of an expander/segment oil control ring depends on the following:

- nominal contact pressure,  $p_o$ ;
- segment width  $h_{12}$ ;
- specific tangential force  $F_{tc}$  for a unit contact pressure of  $1 \text{ N/mm}^2$ .

The values for nominal contact pressure and specific tangential forces are tabulated in ISO 6627.

### 7.6.2 Example for calculating the tangential force $F_t$ — Selected type of piston ring: ISO 6627 - ES3 - 85 × 3 - MC67 MC68/CR1 PNH

#### 7.6.2.1 Pressure class and specific tangential force

Class of nominal contact pressure:  $p_o = 1,2 \text{ N/mm}^2$ ; multiplying factor = 1,2.

Specific tangential force  $F_{tc}$  for unit contact pressure of  $p_{ou} = 1 \text{ N/mm}^2$  and segment width 0,45 (e.g.  $F_{tc} = 38,2$ ).

#### 7.6.2.2 Calculation

Tangential force:  $F_t = 1,2 \times 38,2 \text{ N} \pm 20 \%$ ;

$$F_t = 45,8 \text{ N} \pm 20 \%$$

$$F_t = 36,5 \text{ N} \dots 55 \text{ N}.$$

## 8 Notches for preventing ring rotation

### 8.1 Ring joint with internal notch (only for compression rings as specified in ISO 6622 and ISO 6624)

See [Figure 1](#), [Figure 2](#), [Table 7](#), and [Table 8](#).

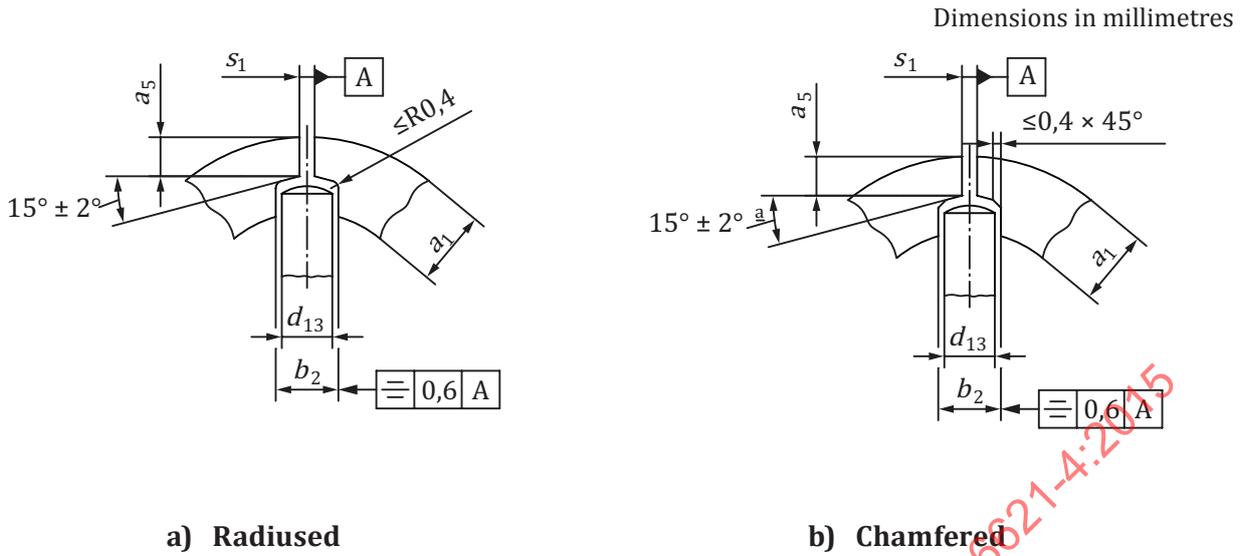


Figure 1 — Internal notch

Table 7 — Dimensions of internal notch

Dimensions in millimetres

Code	Pin diameter $d_{13}$	Notch <sup>a</sup>		
		$b_2$	tol.	$r_6$ <sup>b</sup>
NH1	1,5	2	+0,2 -0,1	0,8
NH2	2	2,5		0,9
NH3	2,5	3		1

<sup>a</sup>  $b_2 - d_{13} > s_1$  nom.

<sup>b</sup>  $r_6$  applies only to notch design according to Figure 2.

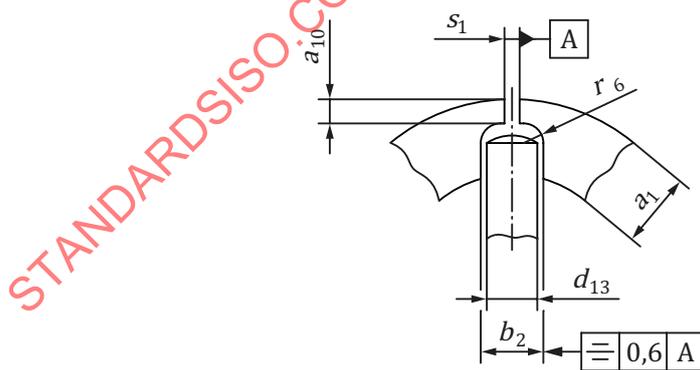


Figure 2 — Internal notch: Option for piston rings with radial wall thickness  $a_1 > 2,1$

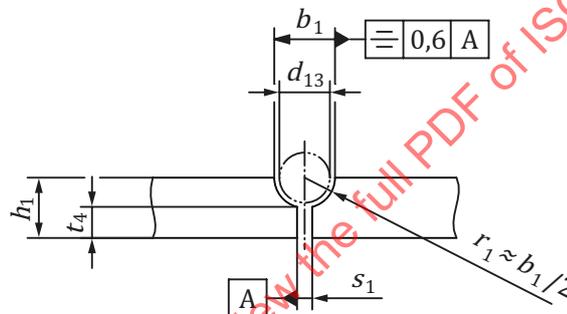
**Table 8 — Width of overlap  $a_5$  and optional  $a_{10}$  for internal notch**

Dimensions in millimetres

Radial wall thickness $a_1$	Overlap			
	$a_5$	tol.	$a_{10}$	tol.
$1,5 \leq a_1 < 2,1$	0,6	±0,1	—	±0,1
$2,1 \leq a_1 < 2,7$	0,7		0,6	
$2,7 \leq a_1 < 3,1$	1		0,7	
$3,1 \leq a_1 < 3,5$	1,2		0,8	
$3,5 \leq a_1 < 3,9$	1,4		0,9	
$3,9 \leq a_1 < 4,1$	1,6		1	

**8.2 Ring joint with side notch (only for compression rings as specified in ISO 6622)**

See [Figure 3](#) and [Table 9](#).



**Figure 3 — Side notch**

**Table 9 — Dimensions of side notch**

Dimensions in millimetres

Code	Ring width	Pin diameter	Notch <sup>a</sup>				
	$h_1$		$d_{13}$	$b_1$	tol.	$t_4$	tol.
NE1	1,2 <sup>b</sup>	1,5	2			0,5	
	1,5					0,7	
	1,75					0,95	
	2					1,2	
	2,5					1,7	
NE2	1,5	2	2,3	+0,2 -0,1	0,7	0 -0,15	
	2		2,5		0,9		
	2,5		2,5		1,4		
	3		2,5		1,9		
NE3	2,5	2,5	3		1		
	3	2,5	3		1,5		

<sup>a</sup>  $b_1 - d_{13} > s_1$  nom.

<sup>b</sup> Not applicable for material Class 10 according to ISO 6621-3.

## 9 Machining of surfaces

### 9.1 Peripheral surfaces

Standard machined: no code required. See [Table 10](#).

**Table 10 — Standard machined peripheral surfaces**

Ring Type	Ring description	Standard machining methods of peripheral surfaces
All Types	All unplated/uncoated rings made of cast iron	Fine turned
R; B; BA; BM; BAM; N; E; T; TB; TBA; K; KB; KBA HK; HKB; HKBA	Plated/spray coated peripheral surface  Straight or barrel faced  On rectangular, napier/scrapper, or keystone rings  Made of cast iron or steel	Machined (i.e. ground, lapped, or polished) over full face
R; B; BA; BM; BAM; T; TB; TBA; K; KB; KBA; HK; HKB; HKBA	Nitrided peripheral surface on straight or barrel faced rectangular or keystone rings made of steel	Machined (i.e. ground, lapped, or polished) over full face
M; NM, EM; TM; KM	Plated/spray coated or nitrided peripheral surface on taper faced rings made of cast iron or steel	Witness machined (i.e. ground, lapped, or polished) on part of the width of the peripheral surface only
ES1 ... ES4	Plated or nitrided peripheral surfaces on segments for expander/segment oil control rings made of steel	Machined (= lapped) over part of the width Or machined (= polished) over full face of the peripheral surface
DSF-C; DSF-CNP	Plated lands on oil control rings made of cast iron	Machined (i.e. ground, lapped, or polished) over full face

NOTE Roughness values and measurement method may be agreed upon between manufacturer and customer as there is no standard method available which is applicable in all cases.

### 9.2 Side faces

The standard method of machining is by grinding of side faces: no code required.

The standard side face finish is  $Rz$  4 or  $Ra$  0,8, and for steel nitrided,  $Rz$  3,2 or  $Ra$  0,6

In the case of piston rings with treated surfaces (FE, PO, PR), the roughness shall be measured before surface treatment.

Segments for expander/segment oil control rings made of steel are without machining.

### 9.3 Other surfaces

See [Table 11](#).

**Table 11 — Standard machined other surfaces**

Surface description	Standard machining methods
Inside surface: rings made of cast iron	Turned
rings made of steel	Without machining
Gap faces	Ground or milled
Oil control rings OD profile	Turned or ground (DSF-C)
Coil spring	Ground or without machining
Expander	Without machining
Other surfaces	Turned, ground, or milled
NOTE Roughness values and measurement method may be agreed upon between manufacturer and customer as there is no standard method available which is applicable in all cases.	

## 10 Plated, coated, and treated surfaces

### 10.1 Chromium plating on peripheral surfaces

#### 10.1.1 General

Codes are required for chromium plated surfaces as specified in the dimensional standards.

#### 10.1.2 Chromium plating thickness

See [Table 12](#).

**Table 12 — Chromium plating thickness**

Dimensions in millimetres

Code	Thickness min	Tolerance guideline <sup>a</sup>	
		$d_1 < 160$	$160 \leq d_1 \leq 200$
CRF	0,005	—	—
CR1/CR1E/CR1F	0,05	+0,15 0	+0,2 0
CR2/CR2E/CR2F	0,1		
CR3	0,15		
CR4	0,2		
<sup>a</sup> Usually, a minimum specification does not call for tolerances. If a tolerance is required on the plating thickness, this guideline is recommended.			

#### 10.1.3 Chromium plated rings of fully faced design

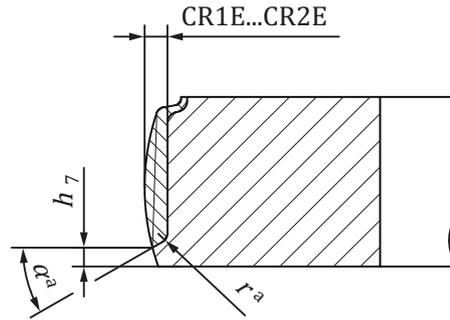
Code: CRF ... CR4.

Piston rings with plated peripheral surfaces are normally designed fully faced.

#### 10.1.4 Chromium plated rings of semi-inlaid design

Code: CR1E ... CR2E.

See [Figure 4](#) and [Table 13](#).



a At the manufacturer's discretion.

Figure 4 — Chromium plated ring semi-inlaid

Table 13 — Land dimensions  $h_7$  of peripheral edges for chromium plated rings semi-inlaid

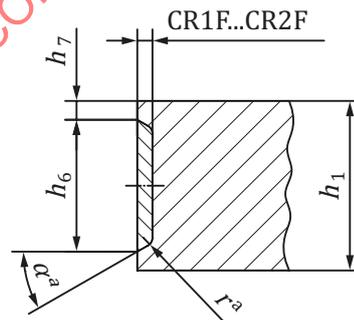
Dimensions in millimetres

Ring width $h_1$	Land dimension $h_7$	
	MC 10, 20, 30	MC 40, 50, 60
$\leq 2$	0,15 ... 0,45	0,1 ... 0,4
$2 < h_1 < 3,5$	0,15 ... 0,5	0,1 ... 0,45
$3,5 \leq h_1 \leq 4,5$	0,15 ... 0,55	0,1 ... 0,5

10.1.5 Chromium plated rings of inlaid design

Code: CR1F ... CR2F.

See [Figure 5](#) and [Table 14](#).



a At the manufacturer's discretion.

Figure 5 — Chromium plated ring inlaid

**Table 14 — Dimensions of groove and land of peripheral edges for chromium plated rings**

Dimensions in millimetres

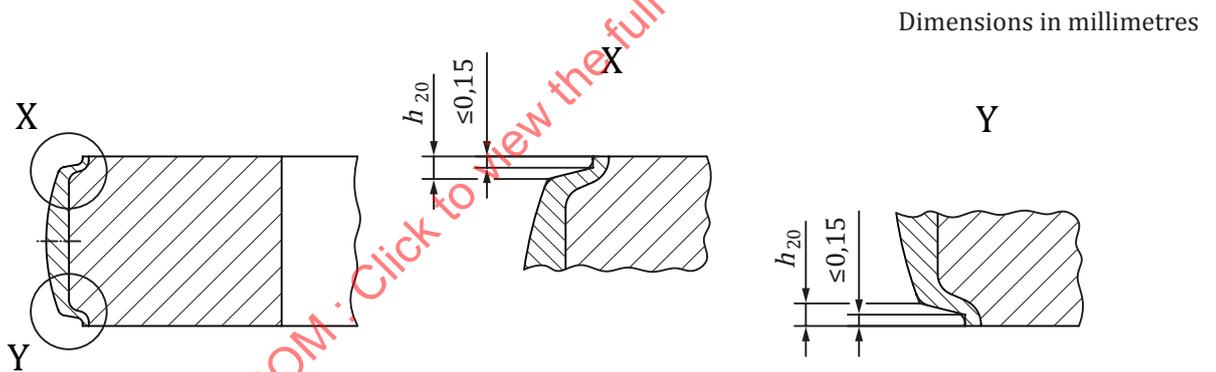
Ring width $h_1$	Groove dimension $h_6$ min.	Land dimension $h_7$	
		MC 10, 20, 30	MC 40, 50, 60
2	1,3	0,15 ... 0,45	0,1 ... 0,4
2,5	1,7	0,15 ... 0,5	0,1 ... 0,45
3	2,2		
3,5	2,5	0,15 ... 0,55	0,1 ... 0,5
4	3		
4,5	3,5		

**10.1.6 Radiusing, chamfering, and dimensions of peripheral edges of chromium plated rings**

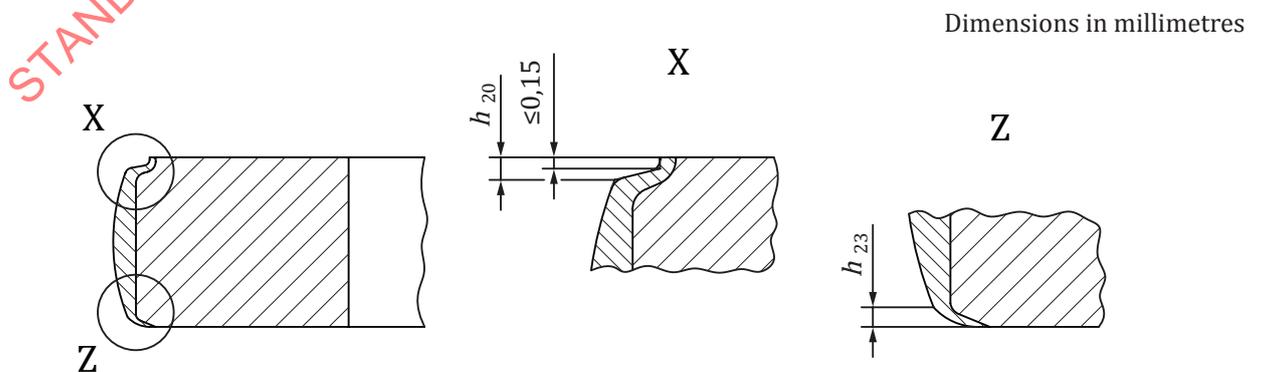
NOTE Values do not apply to chromium plated oil control rings and segments.

Rings of Code CRF to CR4, both peripheral edges, and rings of Code CR1E to CR2E, the upper peripheral edge, may be radiused or chamfered before plating.

See [Figure 6](#) to [Figure 8](#) and [Table 15](#).



**Figure 6 — Chromium plated ring fully faced**



**Figure 7 — Chromium plated ring fully faced, reduced peripheral bottom edge — Code: KU**

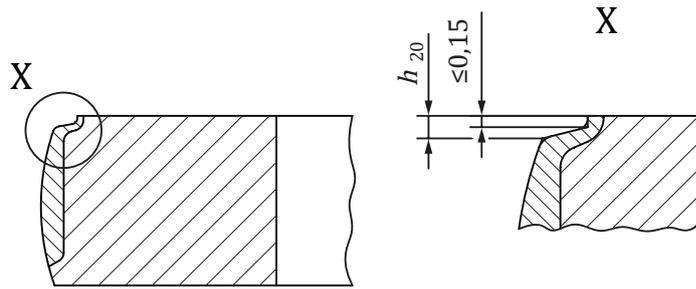


Figure 8 — Chromium plated ring semi-inlaid

Table 15 — Axial dimensions,  $h_{20}$  and  $h_{23}$  (acc. code KU) of peripheral edges of chromium plated rings

Dimensions in millimetres

Ring width $h_1$	Axial dimension	
	$h_{20}$ max.	$h_{23}$ max.
$1,0 \leq h_1 < 3,5$	0,3	0,2
$3,5 \leq h_1 \leq 4,5$	0,4	0,3

10.1.7 Peripheral edges at the gap of chromium plated rings and segments

After plating, the peripheral edges at the gap shall be radiused or chamfered. See [Table 16](#).

Table 16 — Circumferential dimensions of peripheral edges at gap of chromium plated rings and segments

Dimensions in millimetres

Ring width $h_1, h_{12}$	Circumferential dimension	
	$s_3$ max.	reduced $s_3$ (Code: KG) max.
$< 6$	0,4	0,15
$\geq 6$	0,6	0,25

10.1.8 Hardness of chromium plating

The hardness of chromium plating shall be 800 HV 0,1 minimum, in accordance with ISO 6507-3.

10.2 Spray coated peripheral surfaces

10.2.1 Codes

Codes are required for spray-coated surfaces as specified in the dimensional standards.

10.2.2 Spray coating thickness

See [10.2.8](#) and [Table 17](#).

### 10.2.3 Spray-coated rings of fully faced design

Code: SC1 to SC4.

### 10.2.4 Spray coated rings of semi-inlaid design

Code: SC1E to SC4E.

See [Figure 9](#).

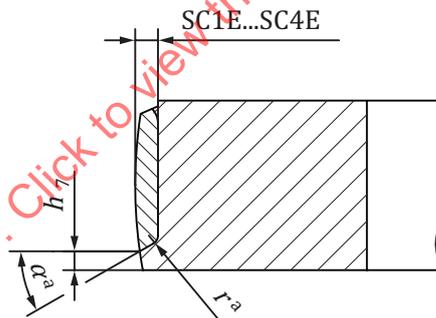
The dimensions of the land at the bottom of the peripheral edge for spray coated rings of semi-inlaid design shall be those given for  $h_7$  in [Table 18](#).

**Table 17 — Spray coating thickness**

Dimensions in millimetres

Code	Thickness min.	Tolerance guideline <sup>a</sup>	
		$d_1 < 160$	$160 \leq d_1 \leq 200$
SC1/SC1E/SC1F	0,05	+0,2 0	+0,25 0
SC2/SC2E/SC2F	0,1		
SC3/SC3E/SC3F	0,15		
SC4/SC4E/SC4F	0,2		

<sup>a</sup> Usually, minimum specification does not call for tolerances. If a tolerance is required on the coating thickness, this guideline is recommended.



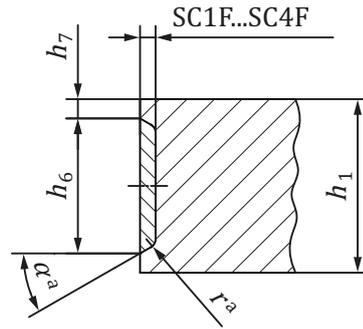
<sup>a</sup> At the manufacturer's discretion.

**Figure 9 — Spray coated ring semi-inlaid**

### 10.2.5 Spray-coated rings of inlaid design

Code: SC1F to SC4F.

See [Figure 10](#) and [Table 18](#).



a At the manufacturer's discretion.

Figure 10 — Spray coated ring inlaid design

Table 18 — Dimensions of groove and land of peripheral edges for spray-coated rings

Dimensions in millimetres

Ring width $h_1$	Groove dimension $h_6$ min.	Land dimension $h_7$	
		MC 10, 20, 30	40, 50, 60
1,2	0,6	0,15 ... 0,45	0,1 ... 0,4
1,5	0,8		
1,75	1,05		
2	1,3	0,15 ... 0,5	0,1 ... 0,45
2,5	1,7		
3	2,2		
3,5	2,5	0,15 ... 0,55	0,1 ... 0,5
4	3		
4,5	3,5		

10.2.6 RADIUSING, CHAMFERING OF PERIPHERAL EDGES OF SPRAY-COATED RINGS

Rings of Codes SC1 to SC4, both peripheral edges, and rings of Codes SC1E to SC4E, the upper peripheral edge, may be radiused or chamfered at the choice of the manufacturer. See Figure 11, Figure 12, and Table 19.