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**Textiles — Determination of the  
total heat transfer through textiles in  
simulated environments**

*Textiles — Détermination du transfert de chaleur total à travers les  
textiles dans des simulations d'environnements*

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## Foreword

ISO (the International Organization for Standardization) is a worldwide federation of national standards bodies (ISO member bodies). The work of preparing International Standards is normally carried out through ISO technical committees. Each member body interested in a subject for which a technical committee has been established has the right to be represented on that committee. International organizations, governmental and non-governmental, in liaison with ISO, also take part in the work. ISO collaborates closely with the International Electrotechnical Commission (IEC) on all matters of electrotechnical standardization.

The procedures used to develop this document and those intended for its further maintenance are described in the ISO/IEC Directives, Part 1. In particular, the different approval criteria needed for the different types of ISO documents should be noted. This document was drafted in accordance with the editorial rules of the ISO/IEC Directives, Part 2 (see [www.iso.org/directives](http://www.iso.org/directives)).

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For an explanation of the voluntary nature of standards, the meaning of ISO specific terms and expressions related to conformity assessment, as well as information about ISO's adherence to the World Trade Organization (WTO) principles in the Technical Barriers to Trade (TBT) see [www.iso.org/iso/foreword.html](http://www.iso.org/iso/foreword.html).

This document was prepared by Technical Committee ISO/TC 38, *Textiles*.

Any feedback or questions on this document should be directed to the user's national standards body. A complete listing of these bodies can be found at [www.iso.org/members.html](http://www.iso.org/members.html).

## Introduction

This document specifies the testing method for the determination of the amount of the heat transferred through clothing fabrics by the combined dry and evaporative heat emission under the simulated and specified conditions.

The amount of heat emission through clothing from our body is very important for comfort in hot environment or during vigorous activities. It is why we consider the comfort of our body as a thermal balancing among ambient climate, energy metabolism and the performance of clothing through removing the excessive heat from our body. The total heat transfer from the body occurs during both the dry heat transmission such as radiation, convection, conduction and the evaporative heat transmission by sweating at the same time. The amount of total heat transfer depends on both gradients of temperature and humidity, for example, the evaporative heat emission has more weight in hot environment with moderate humidity because the dry heat transfer is decreased by the reduction of the temperature difference between body and ambient climate.

Therefore, this document specifies the testing method for the determination of the amount of the heat transferred through clothing fabrics by the combined dry and evaporative heat emission simultaneously under the simulated and specified standard conditions using sweating guarded hot plate. It is for evaluating the performance of clothing fabrics for cooling down the excessive heat from our body.

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# Textiles — Determination of the total heat transfer through textiles in simulated environments

## 1 Scope

This document specifies the test method for determining the amount of heat transferred through clothing fabrics by the combined dry and evaporative heat emission under simulated and specified conditions. This test method can be used for fabrics, films, coatings, foams and leathers including multilayer assemblies used in hot environment or in activities.

The application of this measurement technique is restricted to a maximum amount of total heat transfer which depend on the dimensions and construction of the apparatus used (e.g. about 1 200 W/m<sup>2</sup> for the maximum specifications of the equipment according to ISO 11092).

## 2 Normative references

The following documents are referred to in the text in such a way that some or all of their content constitutes requirements of this document. For dated references, only the edition cited applies. For undated references, the latest edition of the referenced document (including any amendments) applies.

ISO 3696, *Water for analytical laboratory use — Specification and test methods*

ISO 11092:2014, *Textiles — Physiological effects — Measurement of thermal and water-vapour resistance under steady-state conditions (sweating guarded-hotplate test)*

## 3 Terms and definitions

For the purposes of this document, the following terms and definitions apply.

ISO and IEC maintain terminological databases for use in standardization at the following addresses:

- ISO Online browsing platform: available at <https://www.iso.org/obp>
- IEC Electropedia: available at <http://www.electropedia.org/>

### 3.1

#### **dry heat emission**

heat transferred by the temperature difference between the two faces of a material divided by the resultant heat flux per unit area in the direction of the gradient in dry state

Note 1 to entry: It is a quantity which determines the dry heat flux across a given area in response to a steady applied temperature gradient.

### 3.2

#### **evaporative heat emission**

heat transferred by the water-vapour pressure difference between the two faces of a material divided by the resultant evaporative heat flux per unit area in the direction of the gradient, when evaluated non-isothermally

Note 1 to entry: It is a quantity which determines the “latent” evaporative heat flux across a given area in response to a steady applied water-vapour pressure gradient. The evaporative heat flux may consist of condensation as well as diffusive and convective components.

### 3.3

#### total heat transfer

amount of heat transferred by the combined dry and evaporative heat exchanges under the specified conditions

Note 1 to entry: It is expressed in watts per square metre.

## 4 Symbols and units

$R_{ct}$	total thermal resistance of the test specimen and the air layer, $K \cdot m^2/W$
$R_{ct0}$	thermal resistance including the air layer on the surface of the plate without a test specimen This is the apparatus constant, $K \cdot m^2/W$ .
$R_{cf}$	intrinsic thermal resistance of the test specimen only In the calculation of this value, the assumption is made that the boundary layers of the bare plate and the boundary layers of the test specimen are equal, $K \cdot m^2/W$ .
$R_{et}^A$	apparent total evaporative resistance of the test specimen, liquid barrier, and surface air layer when evaluated non-isothermally, $kPa \cdot m^2/W$ The term apparent A is used as a modifier for total evaporative resistance to reflect the fact that condensation may occur within the specimen, $kPa \cdot m^2/W$ .
$R_{et0}^A$	evaporative resistance including the air layer on the surface of the liquid barrier without a test specimen (that is, bare plate) when evaluated non-isothermally. This is the apparatus constant, $kPa \cdot m^2/W$ .
$R_{ef}^A$	intrinsic evaporative resistance of the test specimen only when evaluated non-isothermally, $kPa \cdot m^2/W$ In the calculation of this value, the assumption is made that the boundary layers of the bare plate and the boundary layers of the fabric are equal.
$A$	area of the measuring unit, $m^2$
$T_a$	temperature in the air flowing over the specimen, $^{\circ}C$
$T_m$	temperature of the measuring unit, $^{\circ}C$
$T_s$	temperature of the thermal guard, $^{\circ}C$
$P_a$	water-vapour partial pressure, $kPa$ , in the test enclosure at temperature $T_a$
$P_m$	saturation water-vapour partial pressure, $kPa$ , at the surface of the measuring unit at temperature $T_m$
$R.H.$	relative humidity, %
$H$	heating power supplied to the measuring unit, $W$
$Q_t$	total heat transfer through textiles, $W/m^2$
$R_{ct0_{t25}}$	0,065 $K \cdot m^2/W$ , the standardized bare plate thermal resistance at the air temperature 25 $^{\circ}C$ in test enclosure
$R_{et0_{t25}}^A$	0,003 5 $kPa \cdot m^2/W$ , the standardized bare plate evaporative resistance at the air temperature 25 $^{\circ}C$ in test enclosure

## 5 Principle

This test evaluates two forms of heat transfer which are dry heat and evaporative heat emission. The total heat transfer results from combining both by calculation. Dry heat emission represents the heat loss resulting from the external environment due to the temperature gradient  $10\text{ }^{\circ}\text{C}$  and it is drawn from the standardized total thermal resistance of the test specimen and air layer. Evaporative heat emission represents the heat loss resulting from the external environment due to the vapour pressure gradient  $3,57\text{ kPa}$  and it is drawn from the standardized total evaporative resistance of the test specimen and air layer.

## 6 Apparatus

6.1 **Sweating guarded hot plate** test machine, as described in ISO 11092.

## 7 Materials

### 7.1 Water

For the evaporative resistance measurements, water for analytical laboratory use over grade 3, according to ISO 3696, shall be used to wet the test plate surface.

### 7.2 Liquid barrier

A smooth, water-vapour permeable but liquid-water impermeable cellophane membrane of thickness  $10\text{ }\mu\text{m}$  to  $50\text{ }\mu\text{m}$  shall be fitted over the porous plate.

## 8 Test specimens

Three test specimens are used. Use test specimens large enough to cover the surface of the hot plate test section and the guard section completely. Remove any undesirable wrinkles from the test specimens. Possible techniques for removing wrinkles include smoothing, free-hanging, pressing, steaming, ironing, and so forth. Allow the test specimens to come into equilibrium with the atmosphere  $25\text{ }^{\circ}\text{C}$ ,  $65\text{ }\%$  R.H. of the testing chamber after conditioning them at the same environment for at least 12 h.

## 9 Test procedure

### 9.1 Test conditions

Maintain the temperature of the test plate, guard section and bottom plate at  $(35 \pm 0,5)\text{ }^{\circ}\text{C}$  without fluctuating more than  $\pm 0,1\text{ }^{\circ}\text{C}$  during a test.

Air temperature should be  $(25 \pm 0,5)\text{ }^{\circ}\text{C}$  and it should maintain the air flowing over the test plate at the same condition without fluctuating more than  $\pm 0,1\text{ }^{\circ}\text{C}$  during a test.

Maintain the relative humidity of the air flowing over the plate at  $(65 \pm 4)\text{ }\%$  R.H. during the test.

Set the air velocity  $1\text{ m/s}$ . Maintain the same air velocity for all calibrations and tests, and without fluctuating more than  $\pm 0,1\text{ m/s}$  over the duration of the test measurement.

## 9.2 Procedure

### 9.2.1 Determination of $R_{ct0}$

Measure the bare plate thermal resistance  $R_{ct0}$  according to ISO 11092:2014, 7.1.1 at the test condition  $(25 \pm 0,5) ^\circ\text{C}$ ,  $(65 \pm 4) \% \text{ R.H.}$  of 9.1. The bare plate thermal resistance shall be average of at least three measurements with nothing mounted on the test plate.

### 9.2.2 Measurement of total thermal resistance $R_{ct}$ for a test specimen

Maintain the same condition of 9.1. Place the test specimen to be tested on the measuring unit surface and measure the total thermal resistance  $R_{ct}$ . Measure and calculate the total resistance to dry heat transfer  $R_{ct}$  for a test specimen including the air layer resistance when equilibrium is reached, using Formula (1). The total thermal resistance shall be the average of the measurements for the 3 specimens at least.

$$R_{ct} = \frac{(T_m - T_a) A}{H} \quad (1)$$

where

$R_{ct}$  is the total resistance to dry heat transfer provided by the test specimen and air layer,  $\text{K}\cdot\text{m}^2/\text{W}$ ;

$A$  is the area of the measuring unit,  $\text{m}^2$ ;

$H$  is the heating power supplied to the measuring unit,  $\text{W}$ ;

$T_m$  is the temperature of the measuring unit,  $^\circ\text{C}$ ;

$T_a$  is the temperature in the air flowing over the test specimen,  $^\circ\text{C}$ .

### 9.2.3 Measurement of intrinsic thermal resistance of the test specimen, $R_{cf}$

Determine the intrinsic thermal resistance provided by the test specimen alone,  $R_{cf}$  by subtracting the average thermal resistance value measured for the bare plate including the air layer,  $R_{ct0}$  in 9.2.1 from the average total thermal resistance value measured for the test specimen and air layer,  $R_{ct}$  in 9.2.2. See Formula (2):

$$R_{cf} = R_{ct} - R_{ct0} \quad (2)$$

where  $R_{cf}$  is the intrinsic thermal resistance of the test specimen only.

In the calculation of this value, the assumption is made that the boundary layers of the bare plate and the boundary layers of the test specimen are equal,  $\text{K}\cdot\text{m}^2/\text{W}$ .

### 9.2.4 Measurement of the evaporative resistance including the air layer on the surface of the liquid barrier without a test specimen, $R_{et0}^A$

After testing all specimens for thermal resistance according to 9.2.2, perform the following procedures before the apparent evaporative resistance measurements are made.

Maintain the same environmental condition to  $(25 \pm 0,5) ^\circ\text{C}$ ,  $(65 \pm 4) \% \text{ R.H.}$  of 9.1. Feed distilled water to the test plate so that water uniformly wets the test plate and guard section surface. Cover the test plate and guard section with the liquid barrier to prevent wetting of the test specimen by the liquid water. Adhere the liquid barrier closely to the test plate and guard section with no wrinkles or air bubbles present.

Calculate the bare plate evaporative resistance  $R_{et0}^A$ , including the air layer and the liquid barrier when equilibrium is reached using [Formula \(3\)](#). The bare plate evaporative resistance shall be average of at least three measurements.

$$R_{et0}^A = \frac{(P_m - P_a)A}{H - (T_m - T_a)A/R_{ct0}} \quad (3)$$

where

$R_{et0}^A$  is the evaporative resistance including the air layer on the surface of the liquid barrier without a test specimen (that is, bareplate) when evaluated non-isothermally;

NOTE This is the apparatus constant,  $\text{kPa}\cdot\text{m}^2/\text{W}$ .

$P_m$  is the saturation water-vapour partial pressure,  $\text{kPa}$ , at the surface of the measuring unit at the temperature  $T_m$ ;

$P_a$  is the water-vapour partial pressure,  $\text{kPa}$ , in the test enclosure at temperature  $T_a$ ;

$H$  is the heating power supplied to the measuring unit,  $\text{W}$ ;

$R_{ct0}$  is the average bare plate thermal resistance including the air layer on the surface test plate without a test specimen  $\text{K}\cdot\text{m}^2/\text{W}$  determined in [9.2.1](#),  $\text{K}\cdot\text{m}^2/\text{W}$ ;

### 9.2.5 Measurement of the apparent total evaporative resistance $R_{et}^A$

Maintain the same condition as specified in [9.2.4](#). Place the test specimen on the test plate with the side normally facing the human body towards the test plate without any bubbles and wrinkles.

Measure and calculate the apparent total evaporative resistance  $R_{et}^A$  when equilibrium is reached using [Formula \(4\)](#). The total apparent evaporative resistance shall be the average of the measurements for the 3 specimens at least.

$$R_{et}^A = \frac{(P_m - P_a)A}{H - (T_m - T_a)A/R_{ct}} \quad (4)$$

where

$R_{et}^A$  is the apparent total evaporative resistance of the test specimen, liquid barrier, and surface air layer when evaluated non-isothermally,  $\text{kPa}\cdot\text{m}^2/\text{W}$ ;

$R_{ct}$  is the average total thermal resistance of the test specimen and the air layer,  $\text{K}\cdot\text{m}^2/\text{W}$ .

### 9.2.6 Measurement the intrinsic evaporative resistance provided by the test specimen alone $R_{ef}^A$

Determine the intrinsic evaporative resistance provided by the test specimen alone,  $R_{ef}^A$  by subtracting the average bare plate evaporative resistance value measured for the air layer,  $R_{et0}^A$  from the average total evaporative resistance value measured for the fabric system and air layer,  $R_{et}^A$ . See [Formula \(5\)](#):

$$R_{ef}^A = R_{et}^A - R_{et0}^A \quad (5)$$

where  $R_{ef}^A$  is the intrinsic evaporative resistance of the fabric test specimen only when evaluated non-isothermally,  $\text{kPa}\cdot\text{m}^2/\text{W}$ .