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**Flame arresters — Performance  
requirements, test methods and limits  
for use**

*Arrête-flammes — Exigences de performance, méthodes d'essai  
et limites d'utilisation*

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## Foreword

ISO (the International Organization for Standardization) is a worldwide federation of national standards bodies (ISO member bodies). The work of preparing International Standards is normally carried out through ISO technical committees. Each member body interested in a subject for which a technical committee has been established has the right to be represented on that committee. International organizations, governmental and non-governmental, in liaison with ISO, also take part in the work. ISO collaborates closely with the International Electrotechnical Commission (IEC) on all matters of electrotechnical standardization.

International Standards are drafted in accordance with the rules given in the ISO/IEC Directives, Part 2.

The main task of technical committees is to prepare International Standards. Draft International Standards adopted by the technical committees are circulated to the member bodies for voting. Publication as an International Standard requires approval by at least 75 % of the member bodies casting a vote.

Attention is drawn to the possibility that some of the elements of this document may be the subject of patent rights. ISO shall not be held responsible for identifying any or all such patent rights.

ISO 16852 was prepared by Technical Committee ISO/TC 21, *Equipment for fire protection and fire fighting*.

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## Introduction

Flame arresters are safety devices fitted to openings of enclosures or to pipe work, and are intended to allow flow but prevent flame transmission. They have widely been used for decades in the chemical and oil industry, and a variety of national standards is available. This International Standard was prepared by an international group of experts, whose aim was to establish an international basis by harmonizing and incorporating recent national developments and standards as far as reasonable.

This International Standard addresses manufacturers (performance requirements) and test institutes (test methods), as well as customers (limits for use).

Only relatively general performance requirements are specified and these are kept to a strict minimum. Experience has shown that excessively specific requirements in this field often create unjustified restrictions and prevent innovative solutions.

The hazard identification of common applications found in industry leads to the specification of the test methods. These test methods reflect standard practical situations and, as such, form the heart of this International Standard because they also allow classification of the various types of flame arresters and then determination of the limits of use.

A considerable number of test methods and test conditions had to be taken into account for two main reasons:

- a) different types of flame arresters are covered with respect to the operating principle (static, hydraulic, liquid, dynamic), and each type clearly needs its specific test set-up and test procedure;
- b) it is necessary to adapt flame arresters to the special conditions of application (gas, installation) because of the conflicting demands of high flame quenching capability and low pressure loss; this situation is completely different from the otherwise similar principle of protection by flameproof enclosure (of electrical equipment), where the importance of gas flow through gaps is negligible.

Consequently, in this International Standard, the testing and classification related to the gas groups and the installation conditions has been subdivided more than is usually the case. In particular,

- explosion group IIA is subdivided into sub-groups IIA1 and IIA,
- explosion group IIB is subdivided into sub-groups IIB1, IIB2, IIB3 and IIB, and
- the type “detonation arrester” is divided into four sub-types, which take into account specific installation situations.

The test conditions lead to the limits for use which are most important for the customer. This International Standard specifies this safety relevant information and its dissemination through the manufacturer's written instructions for use and the marking of the flame arresters.

The limits for use are also a link to more general (operational) safety considerations and regulations, which remain the responsibility of national or corporate authorities. Annexes B, C and D offer some guidance in this field.

# Flame arresters — Performance requirements, test methods and limits for use

## 1 Scope

This International Standard specifies the requirements for flame arresters that prevent flame transmission when explosive gas-air or vapour-air mixtures are present. It establishes uniform principles for the classification, basic construction and information for use, including the marking of flame arresters, and specifies test methods to verify the safety requirements and determine safe limits of use.

This International Standard is valid for pressures ranging from 80 kPa to 160 kPa and temperatures ranging from  $-20\text{ }^{\circ}\text{C}$  to  $+150\text{ }^{\circ}\text{C}$ .

NOTE 1 In designing and testing flame arresters for operation under conditions other than those specified above, this International Standard can be used as a guide. However, additional testing related specifically to the intended conditions of use is advisable. This is particularly important when high temperatures and pressures are applied. The test mixtures might need to be modified in these cases.

This International Standard is not applicable to the following:

- external safety-related measurement and control equipment that might be required to keep the operational conditions within the established safe limits;

NOTE 2 Integrated measurement and control equipment, such as integrated temperature and flame sensors as well as parts which, for example, intentionally melt (retaining pin), burn away (weather hoods) or bend (bimetallic strips), is within the scope of this International Standard.

- flame arresters used for explosive mixtures of vapours and gases, which tend to self-decompose (e.g. acetylene) or which are chemically unstable;
- flame arresters used for carbon disulphide, due to its special properties;
- flame arresters whose intended use is for mixtures other than gas-air or vapour-air mixtures (e.g. higher oxygen-nitrogen ratio, chlorine as oxidant, etc.);
- flame arrester test procedures for internal-combustion compression ignition engines;
- fast acting valves, extinguishing systems and other explosion isolating systems;
- flame arresters integrated or combined with explosion-protected equipment, such as blowers, fans, compressors and pumps.

## 2 Normative references

The following referenced documents are indispensable for the application of this document. For dated references, only the edition cited applies. For undated references, the latest edition of the referenced document (including any amendments) applies.

IEC 60079-1, *Explosive atmospheres — Part 1: Equipment protection by flameproof enclosures “d”*

IEC 60079-1-1:2002, *Electrical apparatus for explosive gas atmospheres — Part 1-1: Flameproof enclosures “d” — Method of test for ascertainment of maximum experimental safe gap*

### 3 Terms and definitions

For the purposes of this document, the following terms and definitions apply.

**3.1 flame arrester**  
device fitted to the opening of an enclosure, or to the connecting pipe work of a system of enclosures, and whose intended function is to allow flow but prevent the transmission of flame

**3.2 housing**  
portion of a flame arrester whose principal function is to provide a suitable enclosure for the flame arrester element and allow mechanical connections to other systems

**3.3 flame arrester element**  
portion of a flame arrester whose principal function is to prevent flame transmission

**3.4 stabilized burning**  
steady burning of a flame stabilized at, or close to, the flame arrester element

**3.5 short time burning**  
stabilized burning for a specified time

**3.6 endurance burning**  
stabilized burning for an unlimited time

**3.7 explosion**  
abrupt oxidation or decomposition reaction producing an increase in temperature, pressure, or in both simultaneously

**3.8 deflagration**  
explosion propagating at subsonic velocity

**3.9 detonation**  
explosion propagating at supersonic velocity and characterized by a shock wave

**3.10 stable detonation**  
detonation progressing through a confined system without significant variation of velocity and pressure characteristics

NOTE For the atmospheric conditions, test mixtures and test procedures of this International Standard, typical velocities range between 1 600 m/s and 2 200 m/s.

**3.11 unstable detonation**  
detonation during the transition of a combustion process from a deflagration into a stable detonation

NOTE The transition occurs in a limited spatial zone, where the velocity of the combustion wave is not constant and where the explosion pressure is significantly higher than in a stable detonation. The position of this transition zone depends, amongst other factors, on pipe diameter, pipe configuration, test gas and explosion group.

### 3.12 Characteristic safety data of explosive mixtures

#### 3.12.1

##### maximum experimental safe gap

##### MESG

safe gap measured in accordance with IEC 60079-1-1:2002

#### 3.12.2

##### explosion group

##### Ex.G

ranking of flammable gas-air mixtures with respect to the MESG

NOTE See Table 2, columns 1 and 2.

#### 3.13

##### bi-directional flame arrester

flame arrester that prevents flame transmission from both sides

#### 3.14

##### deflagration flame arrester

##### DEF

flame arrester designed to prevent the transmission of a deflagration

NOTE It can be an **end-of-line flame arrester** (3.21) or an **in-line flame arrester** (3.22).

#### 3.15

##### detonation flame arrester

##### DET

flame arrester designed to prevent the transmission of a detonation

NOTE It can be an **end-of-line flame arrester** (3.21) or an **in-line flame arrester** (3.22), and can be used for both **stable detonations** (3.10) and **unstable detonations** (3.11).

#### 3.16

##### endurance burning flame arrester

flame arrester that prevents flame transmission during and after endurance burning

#### 3.17

##### static flame arrester

flame arrester designed to prevent flame transmission by quenching gaps

##### 3.17.1

##### measurable type

flame arrester where the quenching gaps of the flame arrester element can be technically drawn, measured and controlled

##### 3.17.2

##### non-measurable type

flame arrester where the quenching gaps of the flame arrester element cannot be technically drawn, measured or controlled

EXAMPLE Random structures such as knitted mesh, sintered materials and gravel beds.

**3.18**

**dynamic flame arrester  
high velocity vent valve**

pressure relief valve designed to have nominal flow velocities that exceed the flame velocity of the explosive mixture, thus preventing flame transmission

**3.19**

**liquid product detonation flame arrester**

flame arrester in which the liquid product is used to form a liquid seal as a flame arrester medium, in order to prevent flame transmission of a detonation

NOTE There are two types of liquid product detonation flame arrester for use in liquid product lines: liquid seals and foot valves.

**3.19.1**

**liquid seal flame arrester**

flame arrester designed to use the liquid product to form a barrier to flame transmission

**3.19.2**

**foot valve flame arrester**

flame arrester designed to use the liquid product combined with a non-return valve to form a barrier to flame transmission

**3.20**

**hydraulic flame arrester**

flame arrester designed to break the flow of an explosive mixture into discrete bubbles in a water column, thus preventing flame transmission

**3.21**

**end-of-line flame arrester**

flame arrester that is fitted with one pipe connection only

**3.22**

**in-line flame arrester**

flame arrester that is fitted with two pipe connections, one on each side of the flame arrester

**3.23**

**pre-volume flame arrester**

flame arrester that, after ignition by an internal ignition source, prevents flame transmission from inside an explosion-pressure-resistant containment (e.g. a vessel or closed pipe work) to the outside, or into the connecting pipe work

NOTE Explosion-pressure resistance is a property of vessels and equipment designed to withstand the expected explosion pressure without becoming permanently deformed.

**3.24**

**integrated temperature sensor**

temperature sensor integrated into the flame arrester, as specified by the manufacturer of the flame arrester, in order to provide a signal suitable to activate counter measures

**3.25**

**atmospheric conditions**

conditions with pressures ranging from 80 kPa to 110 kPa and temperatures ranging from  $-20\text{ }^{\circ}\text{C}$  to  $+60\text{ }^{\circ}\text{C}$

## 4 Symbols

$A_0$  free area of a static flame arrester element

$A_p$  nominal cross sectional area of the flame arrester connection

$A_t$	cross sectional area on the unprotected side of the flame arrester element
$A_u$	effective open area of the flame arrester element on the protected side
$D$	pipe diameter
$D_M$	minimum diameter of the pipe on the protected side of a dynamic flame arrester
$L_M$	maximum length without undamped oscillations
$L_m$	pipe length upstream of the dynamic flame arrester used in flame transmission test
$L_p$	pipe length on the protected side
$L_r$	pipe length between flame arrester and restriction
$L_u$	pipe length on the unprotected side, maximum allowable run-up length for installation
$L_1, L_2, L_3, L_4$	pipe lengths in the flow test
$p_{md}$	time average value of the detonation pressure in the time interval of 200 $\mu$ s after arrival of the detonation shock wave
$p_{mu}$	maximum time average value of the transient pressure of an unstable detonation over a time interval of 200 $\mu$ s
$p_t$	pressure in the pressure test
$p_T$	pressure in the flow test of an end-of-line flame arrester
$p_{TB}$	pressure before ignition
$p_0$	maximum operational pressure
$\Delta p$	pressure drop in the flow test of an in-line flame arrester
$R_A$	ratio of the effective open area of the flame arrester element to pipe cross sectional area
$R_U$	ratio of the free volume of the flame arrester element to the whole volume
$t_{BT}$	burning time
$T_{TB}$	temperature of the flame arrester before ignition
$T_0$	maximum operational temperature of the flame arrester
$v_l$	laminar burning velocity
$v_{max}$	maximum flow velocity during the volume flow-pressure drop measurement (flow test)
$v_{min}$	minimum flow velocity during the volume flow-pressure drop measurement (flow test)
$\dot{V}$	volume flow rate
$\dot{V}_c$	critical volume flow rate
$\dot{V}_{CL}$	flow rate at closing point of dynamic flame arresters
$\dot{V}_0$	minimum volume flow rate for endurance burning on dynamic flame arresters
$\dot{V}_E$	maximum volume flow rate for endurance burning on dynamic flame arresters

$\dot{V}_K$	maximum volume flow rate for dynamic flame arresters at the set pressure
$\dot{V}_m$	volume flow rate leading to maximum temperature
$V_M$	minimum volume in the protected tank
$\dot{V}_{max}$	safe volume flow rate
$\dot{V}_s$	safe volume flow rate including a safety margin
$\dot{V}_t$	maximum volume flow rate leading to flame transmission
$Z_{Rmin}$	minimum water seal immersion depth at rest above the outlet openings of the immersion tubes
$Z_R$	immersion depth at rest, corresponding to $Z_{Rmin}$ plus the manufacturer's recommended safety margin
$Z_{0min}$	minimum operational water seal immersion depth when the mixture flow displaces the water from the immersion tubes, where $Z_{0min} > Z_{Rmin}$
$Z_0$	operational immersion depth, corresponding to $Z_{0min}$ plus the manufacturer's recommended safety margin

NOTE All pressure values are absolute pressures.

## 5 Hazards and flame arrester classifications

### 5.1 Flame transmission: deflagration, stable and unstable detonation

The ignition of an explosive mixture will initiate a deflagration. A flame arrester covering only this hazard is classified as a deflagration flame arrester.

A deflagration when confined in a pipe may accelerate and undergo transition through an unstable to a stable detonation, provided sufficient pipe length is available. This pipe length may vary depending upon the initial conditions of the mixture and the pipe work configuration.

A flame arrester tested in accordance with 7.3.3.2 or 7.3.3.3 is classified as a stable detonation flame arrester and is suitable for deflagrations and stable detonations.

Unstable detonations are a specific hazard requiring higher performance flame arresters than for stable detonations.

A flame arrester tested in accordance with 7.3.3.4 or 7.3.3.5 is classified as an unstable detonation flame arrester and is suitable for deflagrations, stable detonations and unstable detonations.

These hazards relate to specific installations and in each case the flame arrester successfully tested at  $p_{TB}$  is suitable for operational pressures  $p_0 \leq p_{TB}$ , and the application is limited to mixtures with an MESG equal to or greater than that tested.

The specific hazards covered by this International Standard, the classification and the testing required for the appropriate flame arrester are listed in Table 1.

**Table 1 — Flame arrester classification for deflagration, stable and unstable detonation**

Application	Flame arrester classification
a) unconfined deflagration into an enclosure or vessel	end-of-line deflagration
b) confined deflagration propagating along a pipe into connecting pipe work	in-line deflagration
c) deflagration confined by an enclosure or pipe work to the outside atmosphere or into connecting apparatus	pre-volume deflagration
d) stable detonation propagating along a pipe into connecting pipe work	in-line stable detonation
e) unstable detonation propagating along a pipe into connecting pipe work	in-line unstable detonation
f) stable detonation into an enclosure or vessel	end-of-line stable detonation

## 5.2 Flame transmission: stabilized burning

Stabilized burning after ignition creates additional hazards in applications where there could be a continuous flow of the explosive mixture towards the unprotected side of the flame arrester. The following situations shall be taken into account:

- if the flow of the explosive mixture can be stopped within a specific time that is between 1 min and 30 min, flame arresters which prevent flame transmission during that period of stabilized burning are suitable for that hazard, and they are classified as safe against short time burning;

NOTE Bypassing, sufficient diluting or inerting are measures equivalent to stopping the flow.

- if the flow of the explosive mixture cannot be stopped or, for operational reasons, is not intended to be stopped within 30 min, flame arresters which prevent flame transmission for this type of stabilized burning are suitable for that hazard, and they are classified as safe against endurance burning.

## 6 General requirements

### 6.1 Measuring instruments

Appropriate and calibrated measuring instruments shall be used for the tests.

NOTE It is advisable that the uncertainty of measurement in the tests be such that it can be shown that all the required test parameter limits are met.

### 6.2 Construction

All parts of the flame arrester shall resist the expected mechanical, thermal and chemical loads for the intended use.

Production flame arresters shall have flame quenching capabilities no less than the tested flame arrester.

Light metal alloys shall not contain more than 6 % magnesium. Coatings of components which may be exposed to flames during operation shall not be damaged in a way that makes flame transmission possible.

Flame arresters for short time burning shall be fitted with one or more integrated temperature sensors, taking into account the intended orientation of the flame arrester.

### 6.3 Housings

Thread gaps, which shall prevent flame transmission, shall be in accordance with the constructional requirements of IEC 60079-1.

### 6.4 Joints

All joints shall be constructed and sealed in such a way that

- flame cannot bypass the flame arrester element, and
- flame is prevented from propagating to the outside of the flame arrester.

### 6.5 Pressure test

Pressure testing of in-line and end-of-line detonation flame arresters shall be carried out at each flame arrester at a pressure of not less than  $10 \times p_0$ , and of all in-line deflagration flame arresters at not less than  $10^6$  Pa for not less than 3 min. No permanent deformation shall occur during the test.

End-of-line deflagration flame arresters need not be pressure tested.

### 6.6 Leak test

Each flame arrester shall be leak tested with air at  $1,1 \times p_0$ , with a minimum of 150 kPa absolute for not less than 3 min. No leak shall occur.

Flame arresters shall not be painted or coated on the inside and/or outside with materials which are able to seal or cover leaks.

End-of-line deflagration flame arresters need not be leak tested.

### 6.7 Flow measurement (air)

The pressure drop shall be tested before and after flame transmission tests and endurance burning tests at a volume flow that is suitable for identifying any alteration (deformation) of the flame arrester, particularly of the flame arrester element. After flame transmission testing, the pressure drop shall not differ by more than 20 % from the value measured at the same flow rate before that testing.

The flow capacity of in-line flame arresters shall be recorded in accordance with Clause A.2 in a type test.

The flow capacity of end-of-line flame arresters shall be recorded in accordance with Clause A.3 in a type test.

The flow capacity of end-of-line flame arresters combined with or integrated into pressure and/or vacuum valves shall be recorded in accordance with Clause A.3. Pressure and/or vacuum valves manufactured for different pressure settings shall be tested at the lowest and the highest set pressure and for intermediate set pressures  $\leq 1$  kPa apart.

The flow capacity of dynamic flame arresters shall be recorded in accordance with Clause A.3 in a type test.

In addition, all dynamic flame arresters shall be tested for undamped oscillations in accordance with Clause A.4 in a type test.

## 6.8 Flame transmission test

### 6.8.1 General

All flame arresters shall be type tested against flame transmission. There shall be no permanent visible deformation of the housing.

The tests shall be specific for the basic types of operation (as defined in 3.17, 3.18, 3.19 and 3.20) and shall be carried out in accordance with Clause 7, 8, 9 or 10. One flame arrester shall be used throughout all deflagration or detonation flame transmission tests. No replacement parts or modifications shall be made to the flame arrester during these tests.

Short time and endurance burning tests shall be carried out in the orientation to be used in service. Bi-directional flame arresters shall only be tested from one side if the protected and unprotected sides are identical.

All flame transmission tests shall be carried out with gas-air mixtures at ambient temperatures. When heat tracing of the flame arrester is required, tests shall be carried out as described in the specific section, but with the flame arrester only being heated to the required temperature,  $T_{TB} \leq 150$  °C. Gas-air or vapour-air mixtures shall be as specified in 6.8.2.

Depending on their intended use, flame arresters shall be tested to the specific explosion group of the explosive gas-air or vapour-air mixture (see Table 2, columns 1 and 2).

For the purposes of this International Standard, group IIC covers hydrogen and other gas-air or vapour-air mixtures with MESG less than 0,5 mm, and group IIB is divided into four sub-groups: IIB1, IIB2, IIB3 and IIB. Explosion group IIA is divided into two sub-groups: IIA1 and IIA. This International Standard covers deflagration and detonation tests for IIA, IIB1, IIB2, IIB3, IIB and IIC. IIA1 shall only be used for the testing of deflagration flame arresters.

The limiting MESG values, which define the explosion groups IIA1, IIA, IIB1, IIB2, IIB3, IIB and IIC, are shown in Table 2.

A flame arrester for a particular explosion group is suitable for explosive mixtures of another group having a higher MESG.

NOTE The testing of flame arresters attached to flow machines (e.g. blowers, fans, pumps, compressors) is not covered and needs specific testing.

### 6.8.2 Test mixtures

Tables 2, 3 and 4 specify the mixtures for deflagration and detonation tests, short time burning and endurance burning tests.

Gas-air mixtures for testing shall be established with a concentration measuring instrument or a MESG test apparatus.

Table 2 — Specification of gas-air mixtures for deflagration and detonation tests

Range of application (marking)		Requirements for test mixture			
Explosion group	MESG of mixture mm	Gas type	Gas purity by volume %	Gas in air by volume <sup>a</sup> %	Safe gap of gas-air mixture mm
IIA1	≥ 1,14	Methane	≥ 98	8,4 ± 0,2	1,16 ± 0,02
IIA <sup>b</sup>	> 0,90	Propane	≥ 95	4,2 ± 0,2	0,94 ± 0,02
IIB1 <sup>b</sup>	≥ 0,85	Ethylene	≥ 98	5,2 ± 0,2	0,83 ± 0,02
IIB2 <sup>b</sup>	≥ 0,75			5,7 ± 0,2	0,73 ± 0,02
IIB3 <sup>b</sup>	≥ 0,65			6,6 ± 0,3	0,67 ± 0,02
IIB <sup>b</sup>	≥ 0,50	Hydrogen	≥ 99	45,0 ± 0,5	0,48 ± 0,02
IIC	< 0,50	Hydrogen	≥ 99	28,5 ± 2,0	0,31 ± 0,02

NOTE The ranking in columns 1 and 2 is not comparable with the ranking in IEC 60079-1-1.

<sup>a</sup> When the test gas mixture is measured by the safe gap of the gas-air mixture, the mixture shall be in the lower half of the specified gap range. If the test gas mixture is measured by the percentage of gas in air by volume, then for IIA1, IIA, IIB3 and IIC, the mixture shall be within the specified percentage volume range. For IIB1 and IIB2, the mixture shall be in the upper half side of the specified percentage volume range. For IIB, the mixture shall be on the lower half side of the specified percentage volume range. All the stated full range tolerances relate to the uncertainty of the measuring equipment.

<sup>b</sup> With small diameters, it may be difficult to generate stable detonations. Tests may be carried out using a gas-air mixture of a lower safe gap.

Table 3 — Specification of gas-air mixtures for short time burning tests

Range of application (marking) Explosion group	Requirements for test mixture		
	Gas type	Gas purity by volume %	Gas in air by volume %
IIA1	Methane	≥ 98	9,5 ± 0,2
IIA	Propane	≥ 95	4,2 ± 0,2
IIB1	Ethylene	≥ 98	6,6 ± 0,3
IIB2			
IIB3			
IIB			
IIC	Hydrogen	≥ 99	28,5 ± 2,0

Table 4 — Specification of gas-air or vapour-air mixtures for endurance burning tests

Range of application (marking) Explosion group	Requirements for test mixture		
	Gas or liquid	Purity by volume %	Gas vapour in air by volume <sup>a</sup> %
IIA1 <sup>b</sup>	Methane	≥ 98	9,5 ± 0,2
IIA <sup>b</sup>	Hexane	≥ 70	2,1 ± 0,1
IIB1 <sup>b</sup>	Ethylene	≥ 98	6,6 ± 0,3
IIB2 <sup>b</sup>			
IIB3 <sup>b</sup>			
IIB <sup>b</sup>			
IIC	Hydrogen	≥ 99	28,5 ± 2,0

<sup>a</sup> Testing of dynamic flame arresters may require a variation in mixture composition.

<sup>b</sup> For static flame arresters, the range of applications is limited to pure hydrocarbons (compounds containing only carbon and hydrogen).

## 6.9 Summary of tests to be conducted

The tests to be conducted are given in Table 5.

Table 5 — Summary of tests to be conducted

Type of flame arrester	Flame transmission test	Burning test (when required)	Flow test
End-of-line deflagration flame arrester	7.3.2.1	7.3.4	A.3
		7.3.5	
In-line deflagration flame arrester	7.3.2.2	7.3.4	A.2
		7.3.5	
Pre-volume flame arrester	7.3.2.3	—	A.2 or A.3
Stable detonation flame arrester without restriction	7.3.3.2	7.3.4	A.2
		7.3.5	
Stable detonation flame arrester with restriction	7.3.3.3	7.3.4	A.2
		7.3.5	
Unstable detonation flame arrester without restriction	7.3.3.4	7.3.4	A.2
		7.3.5	
Unstable detonation flame arrester with restriction	7.3.3.5	7.3.4	A.2
		7.3.5	
Liquid seal and foot valve	8.3	—	—
Dynamic flame arrester (high velocity vent valve)	9.2	9.3	A.3.2 and A.4
Hydraulic flame arrester	10.2.3, 10.2.4	10.2.2	—

## 7 Specific requirements for static flame arresters

### 7.1 Construction

Static flame arresters shall consist of a flame arrester element and a housing.

For flame arrester elements with quenching gaps, the dimensions and tolerances shall be indicated (for example, gap length and width of gap).

For crimped ribbon flame arrester elements used for the test, the gaps shall not fall below the upper tolerance limit over 90 % of the entire surface. For production reasons, the gap dimensions may be less than the lower tolerance limit in the inner and outer areas of the flame arrester element. The total affected area shall not exceed 10 % of the total surface area.

Evidence shall be available that manufacture is controlled within tolerances to ensure reproducibility.

Materials for flame arresters shall be suitable for the intended use (e.g. temperature range, chemical properties of the gases and vapours).

### 7.2 Design series

Static flame arresters of similar design, except endurance burning and pre-volume flame arresters, may be grouped in a design series. The design series shall comply with the following:

- a) one drawing shall cover all nominal sizes in a design series and all parts shall be listed and dimensioned;
- b) the flame arrester elements shall have identical features of construction, such as the quenching gaps, and shall have the same thickness measured in the direction of the flame path.

Additional requirements for in-line flame arresters are the following:

- a design series limited to four consecutive nominal sizes, in accordance with Table 6;
- for every nominal size in a design series (maximum four), the ratio,  $R_A$ , as calculated in Equation (1), shall not deviate by more than  $\pm 10\%$  from the ratio of the largest nominal size of the four members:

$$R_A = \frac{A_u}{A_p} \tag{1}$$

Concentric and eccentric shaped housings form different design series.

**Table 6 — Connection**

Design series	Nominal size of connection																
	mm																
	10	20	32	50	60	75	100	125	150	200	250	300	350	400	450	600	800
	to	to	to		to	to									to	to	to
	15	25	40		65	80									500	750	1000

### 7.3 Flame transmission test

#### 7.3.1 General

For non-measurable types of flame arresters, evidence shall be available that production flame arrester elements are equivalent in design, manufacture and construction to the test sample. The test pressure shall be at least 10 % higher than the maximum operational pressure,  $p_0$ , of the flame arrester.

Flame arresters with pressure and/or vacuum valve(s) integrated on the protected side shall have the valve secured in the fully open position, or the pressure and/or vacuum valve pallets shall be taken out during the test.

Flame arresters with pressure and/or vacuum valve(s) integrated on the unprotected side shall have the valve pallets installed and blocked for an opening gap of  $(2,5 \pm 0,5)$  mm during each test.

Flame arresters directly combined with separate pressure and/or vacuum valves used as end-of-line venting systems shall be tested in the same way as end-of-line flame arresters with integrated pressure and/or vacuum valves.

NOTE These end-of-line venting systems could be classified as follows:

- a) as end-of-line deflagration arresters, in accordance with 7.3.2.1;
- b) as end-of-line deflagration arresters, in accordance with 7.3.2.1, and with a short time burning test, in accordance with 7.3.4;
- c) as end-of-line deflagration arresters, in accordance with 7.3.2.1, and with an endurance burning test, in accordance with 7.3.5.

The protected and unprotected side of a flame arrester may be modified to allow connection to smaller pipe sizes without further testing. The connection on the protected side shall not be smaller than the connection on the unprotected side.

The temperatures (mixture, pipe, flame arrester) during testing shall be given in the test report.

#### 7.3.2 Deflagration test

##### 7.3.2.1 End-of-line flame arrester

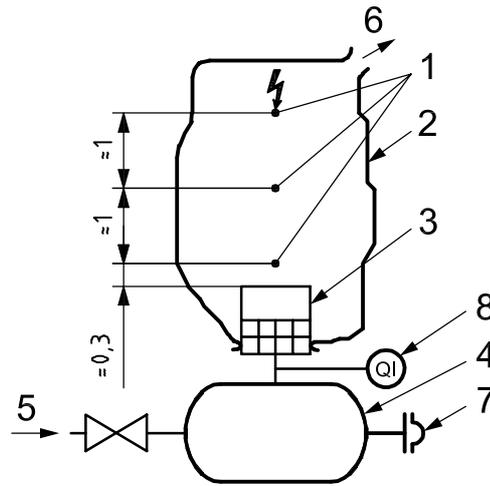
The test apparatus is as shown in Figure 1. Distances shall be measured from the top of the complete flame arrester.

For end-of-line flame arresters with non-measurable elements, it might be necessary to pressurize the plastic bag (see 7.4.1). In this case, the mixture outlet (item 6 in Figure 1) needs to be fitted with a shut-off valve.

Assemble the flame arrester with all ancillary equipment, including weather cowls or other covers, and enclose it in a plastic bag.

Fill the apparatus, fully inflating the bag with a mixture as specified in 6.8.2. Disconnect the mixture supply and ignite. The ignition source shall be a spark plug. Carry out two tests for each ignition point so that a total of six tests will result. Flame transmission shall be indicated by the flame detector on the protected side. No flame transmission shall occur in any of the tests.

If the largest and smallest nominal sizes of a design series are satisfactorily tested, intermediate sizes may be considered acceptable without testing.



**Key**

- 1 ignition sources
- 2 plastic bag ( $\varnothing \geq 1,2$  m; length  $\geq 2,5$  m; foil thickness  $\geq 0,05$  mm)
- 3 end-of-line flame arrester
- 4 explosion-pressure-resistant containment (vessel or closed pipe work)
- 5 mixture inlet with shut-off valve
- 6 mixture outlet
- 7 bursting diaphragm
- 8 flame detector for indication

**Figure 1 — Test apparatus for end-of-line flame arrester for deflagration test**

**7.3.2.2 In-line flame arrester**

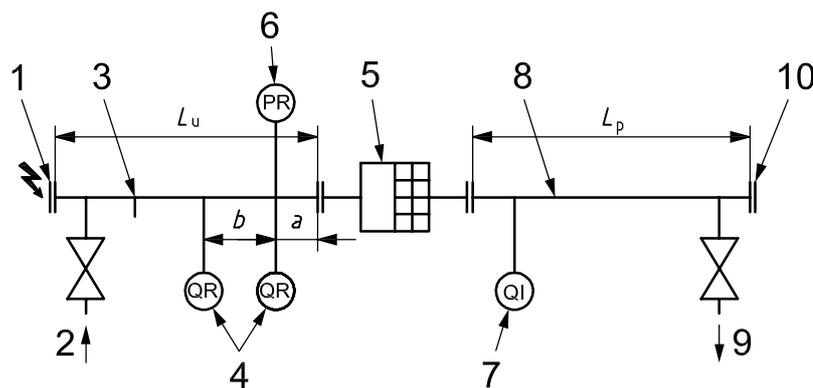
The test apparatus is shown in Figure 2. The ignition source shall be a spark plug fitted in the centre of the blind flange.

The pipe diameter  $D$  shall have the same size as the flame arrester connection. The pipe length  $L_u$  shall be not less than  $10 \times D$  and not greater than  $50 \times D$  for hydrocarbon-air mixtures (IIA1, IIA, IIB1, IIB2 and IIB3) and not greater than  $30 \times D$  for hydrogen-air mixtures (IIB and IIC). The pipe length  $L_p$  shall be  $50 \times D$  for hydrocarbon-air mixtures (IIA1, IIA, IIB1, IIB2 and IIB3) and  $30 \times D$  for hydrogen-air mixtures (IIB and IIC).

NOTE 1 It is advisable that the pipe length  $L_u$  be given by the manufacturer. In case of successful testing,  $L_u$  will be the maximum allowable run-up length for practical installations (see 7.4.2).

NOTE 2 It is possible in larger pipe sizes to approach the transition from a deflagration to a detonation when testing at raised  $p_{TB}$  and  $L_u = 50 \times D$ . If a deflagration to detonation transition is indicated, then testing with lower  $L_u$  is appropriate.

The flame velocity shall be measured by two flame detectors fitted to the pipe on the unprotected side, in accordance with Figure 2. The distance  $b$  between the two flame detectors shall be in accordance with Figure 2. The pressure shall be recorded by a pressure recording system (limiting frequency  $\geq 100$  kHz) fitted to the pipe on the unprotected side, at a distance  $a$  in accordance with Figure 2.

**Key**

- 1 blind flange with ignition source
- 2 mixture inlet
- 3 unprotected pipe (length  $L_u$ ; diameter  $D$ )
- 4 flame detectors for recording
- 5 in-line deflagration flame arrester
- 6 pressure transducer for recording
- 7 flame detector for indication
- 8 protected pipe (length  $L_p$ ; diameter  $D$ )
- 9 mixture outlet
- 10 blind flange or other closure

$$a \leq 2 \times D (\pm 10 \%, \text{ max. } \pm 50 \text{ mm}), \text{ but } a \leq 250 \text{ mm}$$

$$b \leq 3 \times D$$

**Figure 2 — Test apparatus for in-line flame arrester for deflagration test**

Fill the apparatus with a test mixture as specified in 6.8.2 and pressurize to  $p_{TB}$  when  $p_{TB} \geq p_0$  (where  $p_0$  is the maximum operational pressure requested by the manufacturer or user). In six consecutive tests, no flame transmission shall occur. A flame transmission is indicated by the flame detector on the protected side.

The flame velocities, maximum explosion pressures and pipe length ( $L_u$ ) in each test shall be given in the test report.

If the largest and smallest nominal size of a design series are satisfactorily tested, the two intermediate nominal sizes in accordance with 7.2 may be considered acceptable without testing. Each size larger than 1 000 mm shall be tested.

### 7.3.2.3 Pre-volume flame arrester

The test apparatus is shown in Figure 3.

For pre-volume flame arresters with non-measurable elements, it might be necessary to pressurize the plastic bag (end-of-line application, see 7.4.1). In this case, the mixture outlet (item 6 in Figure 3) needs to be fitted with a shut-off valve.

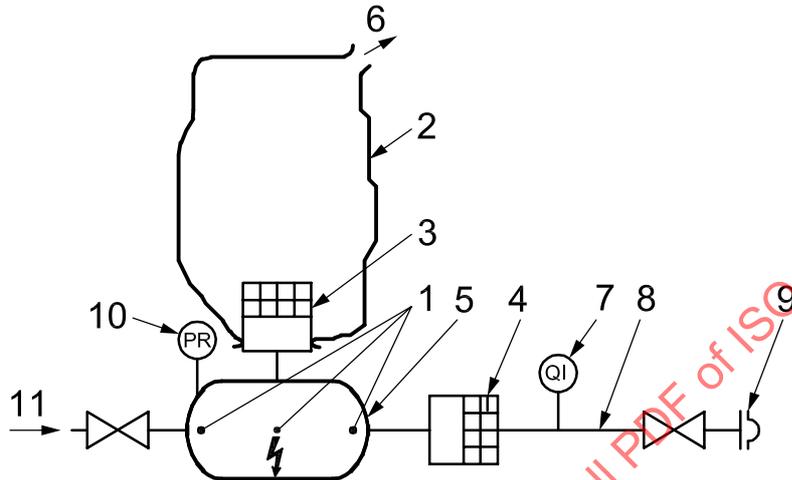
Pre-volume flame arresters shall be tested using the original configuration or equivalent full-scale model configuration.

Pre-volume applications using end-of-line types shall be enclosed in a plastic bag, as shown in Figure 3.

Pre-volume applications using in-line types shall be connected to the actual pipe work or equipment on the protected side, or to pipe work simulating the actual length, diameter and volume.

Flame transmission shall be indicated by the following:

- a) for end-of-line types, by the ignition of the mixture in the plastic bag (2); a flame detector is optional;
- b) for in-line types, by the flame detector (7).



**Key**

- 1 ignition sources
- 2 plastic bag ( $\varnothing \geq 1,2$  m; length  $\geq 2,5$  m; foil thickness  $\geq 0,05$  mm)
- 3 end-of-line flame arrester
- 4 in-line flame arrester
- 5 explosion-pressure-resistant containment (vessel or closed pipe work)
- 6 mixture outlet
- 7 flame detector for indication
- 8 original or simulated pipe work with mixture outlet and shut-off valve
- 9 bursting diaphragm
- 10 pressure transducer for recording
- 11 mixture inlet with shut-off valve

**Figure 3 — Test apparatus for pre-volume flame arrester for deflagration test**

If the enclosure has more than one outlet, all flame arresters shall be used and tested simultaneously.

Fill the enclosure and the plastic bag or pipe with a mixture as specified in 6.8.2. Disconnect the mixture supply and ignite separately at three positions inside the enclosure: one as close as possible to the flame arrester, one at the most likely position of an ignition source and one as far away from the flame arrester as possible.

Carry out two tests for each position resulting in a total of six tests. No flame transmission shall occur in any of the tests.

All types and sizes shall be tested.

### 7.3.3 Detonation test

#### 7.3.3.1 General

If the largest and smallest nominal sizes of a design series are satisfactorily tested for detonations, the two intermediate nominal sizes in accordance with 7.2 may be considered acceptable without testing. Each nominal size larger than 1 000 mm shall be tested.

Detonation flame arresters tested for unstable detonations with restriction (see 7.3.3.5) are classified as Type 1.

Detonation flame arresters tested for unstable detonations without restriction (see 7.3.3.4) are classified as Type 2.

Detonation flame arresters tested for stable detonations with restriction (see 7.3.3.3) are classified as Type 3.

Detonation flame arresters tested for stable detonations without restriction (see 7.3.3.2) are classified as Type 4.

Type 1 detonation flame arresters are also suitable for use as Type 2, Type 3 and Type 4 without additional testing.

Type 2 detonation flame arresters are also suitable for use as Type 4 without additional testing.

Type 3 detonation flame arresters are also suitable for use as Type 4 without additional testing.

#### 7.3.3.2 Stable detonation without restriction

The test apparatus is shown in Figure 4.

The pipe diameter  $D$  shall have the same size as the flame arrester connection.

The pipe on the unprotected side shall have a length  $L_u$  sufficient to develop a stable detonation and shall have a blind flange or an explosion-pressure-resistant containment (vessel or closed pipe work) fitted with an ignition source. The pipe may also contain a flame accelerator to reduce the pipe length for stable detonation conditions.

The pipe on the protected side shall have a length  $L_p$  of  $10 \times D$ , but not less than 3 m. The blind flange or other closure shall resist the shock pressures during testing.

For measuring flame velocities and detonation pressures, four flame detectors and a pressure transducer (limiting frequency  $\geq 100$  kHz) shall be fitted to the pipe on the unprotected side. The position of the flame detectors and the pressure transducer shall be in accordance with Figure 4.

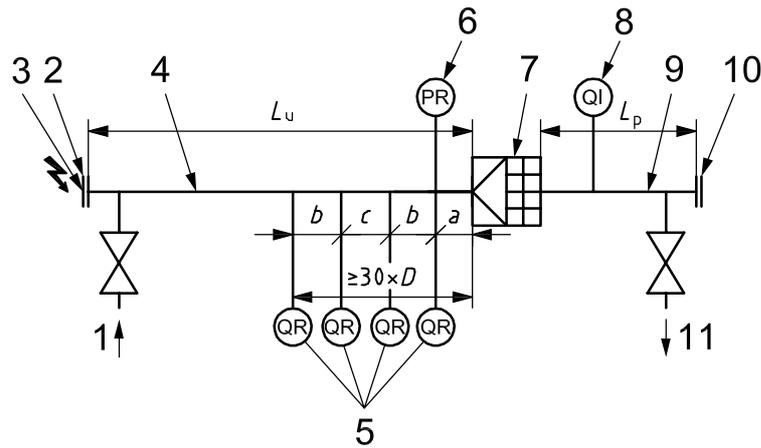
One flame detector shall be fitted to the pipe on the protected side to indicate flame transmission.

The apparatus shall be filled with a test mixture as specified in 6.8.2, and at a pressure of  $p_{TB}$  when  $p_{TB} \geq p_0$ . Under these conditions, five tests shall be carried out.

In each test, the flame velocities from the two pairs of flame detectors (see Figure 4) shall be constant, i.e. the difference between the two flame velocities shall not exceed 10 % of the lower value.

The velocities shall be  $\geq 1\,600$  m/s for hydrocarbon-air mixtures (IIA, IIB1, IIB2 and IIB3) and  $\geq 1\,900$  m/s for hydrogen-air mixtures (IIB and IIC).

The pressure time record shall indicate a stable detonation shock wave.



**Key**

- 1 mixture inlet
- 2 explosion-pressure-resistant containment (vessel or closed pipe work) or blind flange
- 3 ignition source
- 4 unprotected pipe (length  $L_u$ ; diameter  $D$ )
- 5 flame detectors for recording of the flame velocity measurement
- 6 pressure transducer for recording
- 7 detonation flame arrester
- 8 flame detector for indication
- 9 protected pipe (length  $L_p$ ; diameter  $D$ )
- 10 blind flange or other closure
- 11 mixture outlet

$a = (200 \pm 50) \text{ mm}$

$b \geq 3 \times D$ , but  $b \geq 100 \text{ mm}$

$c \geq 500 \text{ mm}$

**Figure 4 — Test apparatus for detonation flame arrester for detonation without restriction**

Until the arrival of a stable detonation shock wave, the pressure (see item 6 in Figure 4) shall remain constant at  $p_{TB}$ . If not, a longer pipe or turbulence promoting equipment may be used.

The average value  $p_{md}$  of the detonation pressure shall be calculated from the area integral below the pressure-time trace, starting at the maximum pressure peak and covering a time interval of  $200 \mu\text{s}$ . The ratio  $p_{md}/p_{TB}$ , with regard to mixture and pipe size, shall correspond to the values given in Table 7 with a maximum deviation of  $\pm 20 \%$ .

NOTE When  $p_{md}/p_{TB}$  exceeds the quoted values of Table 7 by more than 20 % and flame transmission occurs, the detonation might still be overdriven and it is advisable that a longer pipe or turbulence promoting equipment be used.

Table 7 — Ratio  $p_{md}/p_{TB}$ 

Explosion group	Ratio $p_{md}/p_{TB}$ for pipe diameter $D$			
	mm			
	$D \leq 80^a$	$80 < D \leq 150$	$150 < D < 1\ 000$	$D \geq 1\ 000$
IIA	10	12	14	16
IIB1	9	11	13	14
IIB2	9	11	13	15
IIB3	10	12	14	16
IIB	8	10	10	12
IIC	8	8	8	8

<sup>a</sup> If for pipe diameters  $\leq 80$  mm the quoted pressure ratio is not achieved, tests shall be carried out using a gas-air mixture of a lower safe gap to qualify the arrester as a detonation flame arrester.

In addition, deflagration tests shall be carried out where the basic test set-up shall be in accordance with Figure 4, with  $L_p = 50 \times D$ , as follows:

- a) five deflagration tests with  $L_u/D = 5$ , and
- b) five deflagration tests with
  - $L_u/D = 50$  for IIA, IIB1, IIB2 and IIB3, or
  - $L_u/D = 30$  for IIB and IIC.

The ignition source for these deflagration tests shall be a spark plug fitted in the centre of the blind flange. For these deflagration tests, flame velocity measurement is not required.

The initial pressure, deflagration and stable detonation pressure, the values of  $p_{md}/p_{TB}$  and also any flame velocities recorded during the tests shall be reported.

A stable detonation flame arrester (Type 4) shall prevent flame transmission in any of these stable detonation and deflagration tests.

### 7.3.3.3 Stable detonation with restriction

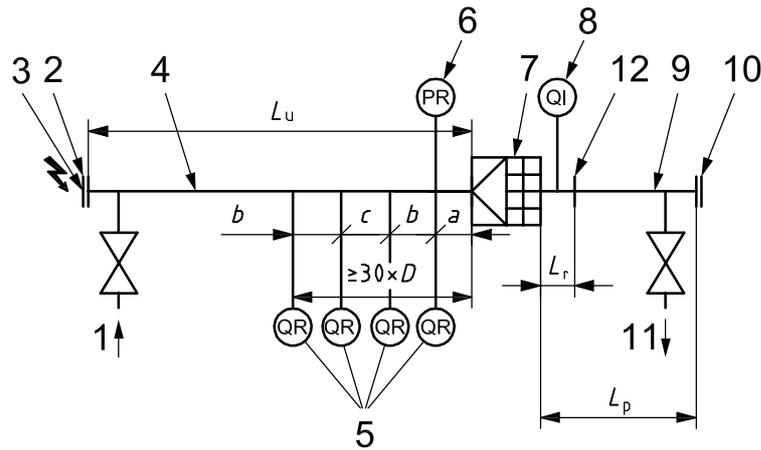
The test apparatus is shown in Figure 5.

The pipe diameter  $D$  shall have the same size as the flame arrester connection.

The pipe on the unprotected side shall have a length  $L_u$  sufficient to develop a stable detonation and shall have a blind flange or an explosion-pressure-resistant containment (vessel or closed pipe work) fitted with an ignition source. The pipe may also contain a flame accelerator to reduce the pipe length for stable detonation conditions.

The pipe on the protected side shall have a length  $L_p$  of  $54 \times D$ . A restriction shall be fitted at  $L_r/D = 4$ . The restriction shall consist of a blind flange with a central bore. The central bore shall have 2,5 % of the cross sectional area of the pipe. The closed pipe end and the restriction shall resist the shock pressures during testing.

For measuring flame velocities and detonation pressures, four flame detectors and a pressure transducer (limiting frequency  $\geq 100$  kHz) shall be fitted to the pipe on the unprotected side. The position of the flame detectors and the pressure transducer shall be in accordance with Figure 5.



**Key**

- 1 mixture inlet
- 2 explosion-pressure-resistant containment (vessel or closed pipe work) or blind flange
- 3 ignition source
- 4 unprotected pipe (length  $L_u$ ; diameter  $D$ )
- 5 flame detectors for recording the flame velocity
- 6 pressure transducer for recording
- 7 detonation flame arrester
- 8 flame detector for indication
- 9 protected pipe (length  $L_p$ ; diameter  $D$ )
- 10 blind flange or other closure
- 11 mixture outlet
- 12 restriction ( $L_r = 4 \times D$ )

$a = (200 \pm 50) \text{ mm}$

$b \geq 3 \times D$ , but  $b \geq 100 \text{ mm}$

$c \geq 500 \text{ mm}$

**Figure 5 — Test apparatus for detonation flame arrester for detonation with restriction**

One flame detector shall be fitted to the pipe on the protected side to indicate flame transmission.

The apparatus shall be filled with a test mixture as specified in 6.8.2, and at a pressure of  $p_{TB}$  when  $p_{TB} \geq p_0$ . Under these conditions, five tests shall be carried out.

In each test, the flame velocities from the two pairs of flame detectors (see Figure 5) shall be constant, i.e. the difference between the two flame velocities shall not exceed 10 % of the lower value.

The velocities may be greater but not less than 1 600 m/s for hydrocarbon-air mixtures (IIA, IIB1, IIB2 and IIB3) and 1 900 m/s for hydrogen-air mixtures (IIB and IIC).

The pressure time record shall indicate a stable detonation shock wave.

Until the arrival of a stable detonation shock wave, the pressure (see item 6 in Figure 5) shall remain constant at  $p_{TB}$ . If not, a longer pipe or turbulence promoting equipment may be used.

The average value  $p_{md}$  of the detonation pressure shall be calculated from the area integral below the pressure-time trace, starting at the maximum pressure peak and covering a time interval of 200  $\mu$ s. The ratio  $p_{md}/p_{TB}$ , with regard to mixture and pipe size shall correspond to the values given in Table 7, with a maximum deviation of  $\pm 20$  %.

NOTE When  $p_{md}/p_{TB}$  exceeds the quoted values of Table 7 by more than 20 % and flame transmission occurs, the detonation might still be overdriven and it is advisable that a longer pipe or turbulence promoting equipment be used.

In addition, deflagration tests shall be carried out, where the basic test set-up shall be in accordance with Figure 5, with  $L_U = 4 \times D$  and  $L_P = 54 \times D$ , as follows:

- a) five deflagration tests with  $L_U/D = 5$ , and
- b) five deflagration tests with
  - $L_U/D = 50$  for IIA, IIB1, IIB2 and IIB3, or
  - $L_U/D = 30$  for IIB and IIC.

The ignition source for these deflagration tests shall be a spark plug fitted in the centre of the blind flange. For these deflagration tests, flame velocity measurement is not required.

The initial pressure, deflagration and stable detonation pressure, the values of  $p_{md}/p_{TB}$  and also any flame velocities recorded during the tests shall be reported.

A stable detonation flame arrester (Type 3) shall prevent flame transmission in any of these stable detonation and deflagration tests.

#### 7.3.3.4 Unstable detonation without restriction

The test apparatus is shown in Figure 4.

The pipe diameter  $D$  shall have the same size as the flame arrester connection.

The pipe on the unprotected side shall have a length  $L_U$  sufficient to develop an unstable detonation and shall have a blind flange or an explosion-pressure-resistant containment (vessel or closed pipe work) fitted with an ignition source. The ignition source may be mounted to the wall of the unprotected pipe. The pipe may also contain a flame accelerator to reduce the pipe length for unstable detonation conditions.

The pipe length and configuration on the unprotected side and the location of the ignition source shall, after ignition, produce an unstable detonation at the detonation flame arrester.

The pipe on the protected side shall have a length  $L_P$  of  $10 \times D$ , and not less than 3 m. The blind flange or other closure shall resist the shock pressures during testing.

Four flame detectors and a pressure transducer shall be fitted to the pipe on the unprotected side to record flame velocities and pressures respectively. One flame detector shall not be more than 200 mm from the flame arrester connection. One flame detector shall be fitted to the pipe on the protected side to indicate flame transmission.

For the purposes of this International Standard, a characteristic of an unstable detonation is  $p_{mu}$  of not less than  $2,5 \times p_{md}$  for pipe diameters  $< 100$  mm, and  $3 \times p_{md}$  for pipe diameters  $\geq 100$  mm. Values of  $p_{md}$  shall be taken from Table 7 with regard to  $p_{TB}$ .

NOTE The unprotected side pipe length and configuration for these tests can be found by varying the distance between the ignition source and the flame arrester until the recorded flame velocities reach a maximum (above those of stable detonations). The distribution of more than four flame detectors along the pipe will make it easier to find the transition point. Direct initiation, e.g. by solid detonators, or long accelerator sections should be avoided.

The apparatus shall be filled with a test mixture as specified in 6.8.2, at a pressure  $p_{TB}$  when  $p_{TB} \geq p_0$ .

Under these conditions, five tests shall be carried out.

In addition, deflagration tests shall be carried out, where the basic test set-up shall be in accordance with Figure 4, with  $L_p = 50 \times D$ , as follows:

- a) five deflagration tests with  $L_u/D = 5$ , and
- b) five deflagration tests with
  - $L_u/D = 50$  for IIA, IIB1, IIB2 and IIB3, or
  - $L_u/D = 30$  for IIB and IIC.

The ignition source for these deflagration tests shall be a spark plug fitted in the centre of the blind flange. For these deflagration tests, flame velocity measurement is not required.

The initial pressure, deflagration and unstable detonation pressures and also any flame velocities shall be reported.

An unstable detonation flame arrester (Type 2) shall prevent flame transmission in any of these deflagration and unstable detonation tests.

#### 7.3.3.5 Unstable detonation with restriction

The test apparatus is shown in Figure 5.

The pipe on the protected side shall have a length  $L_p$  of  $54 \times D$ . A restriction shall be fitted at  $L_r/D = 4$ . The restriction shall consist of a blind flange with a central bore. The central bore shall have 2,5 % of the cross sectional area of the pipe. The closed pipe end and the restriction shall resist the shock pressures during testing.

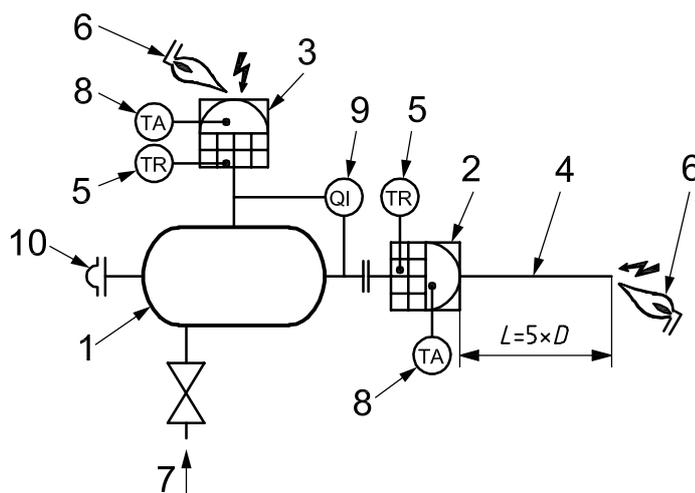
The test procedure for unstable detonation testing as well as the characteristic of an unstable detonation shall be in accordance with 7.3.3.4.

In addition, additional deflagration tests shall be carried out completely in accordance with 7.3.3.3.

An unstable detonation flame arrester (Type 1) shall prevent flame transmission in any of these deflagration and unstable detonation tests.

#### 7.3.4 Short time burning test

The test apparatus is shown in Figure 6 for an in-line and end-of-line flame arrester.



### Key

- 1 explosion-pressure-resistant containment (vessel or closed pipe work)
- 2 in-line flame arrester
- 3 end-of-line flame arrester
- 4 outlet pipe
- 5 temperature sensor for recording for tests only
- 6 pilot flame
- 7 mixture inlet
- 8 integrated temperature sensor for alarm
- 9 flame detector for indication
- 10 bursting diaphragm

**Figure 6 — Test apparatus for short time burning test**

A flow meter shall be used to measure the mixture flow rates. The flame arrester shall be fitted with a temperature sensor for the test only. This sensor shall be mounted close to the surface of the flame arrester element on the protected side close to the centre of the cross sectional area of the flow.

The tests shall be carried out using a test mixture as specified in Table 3. First, the critical flow rate  $\dot{V}_c$  shall be calculated from the open area  $A_0$  of the surface of the flame arrester element on the unprotected side and from the size and number of apertures per unit area. Assuming a uniform velocity of 75 % of a burning velocity  $v_1$  of the mixture across this area, calculate a critical flow rate  $\dot{V}_c$  according to Equation (2):

$$\dot{V}_c = 0,75 \times A_0 \times v_1 \quad (2)$$

where

$$v_1 = 0,5 \text{ m/s for IIA1 and IIA;}$$

$$v_1 = 0,8 \text{ m/s for IIB1, IIB2, IIB3 and IIB;}$$

$$v_1 = 3 \text{ m/s for IIC.}$$

For non-measurable flame arrester elements, the critical flow rate  $\dot{V}_c$  may be obtained by using the same principle. The free area  $A_0$  of the flame arrester element surface can be estimated according to Equation (3):

$$A_0 = R_U \times A_t \quad (3)$$

The tests shall be carried out with a continuously operated pilot flame or spark. Ignite the mixture until the flame has stabilized on the surface of the flame arrester element. After flame stabilization, continue burning for the burning time  $t_{BT}$  specified by the manufacturer ( $1 \text{ min} \leq t_{BT} \leq 30 \text{ min}$ ). Record the temperature indicated by the test temperature sensor after that time and stop the flow. No flame transmission shall occur during the tests or when the flow is stopped.

Carry out this test procedure with flow rates  $\dot{V}_c$ ,  $0,5 \dot{V}_c$  and  $1,5 \dot{V}_c$ . In each of these tests, the flame arrester shall be at ambient temperature at the beginning. If  $\dot{V}_c$  results in the highest temperature reading of the three tests, then  $\dot{V}_m = \dot{V}_c$ . If not, carry out two further tests with flow rates 50 % and 150 % of the flow rate which gave the highest reading in the first three tests.  $\dot{V}_m$  will be the flow rate that results in the highest temperature reading in all five tests. When determining the flow rate  $\dot{V}_m$ , flame arrester elements may be replaced between the tests. If the flame arrester elements have been replaced, a final test shall be carried out with the flow rate  $\dot{V}_m$ , using the original flame arrester element, without modification, that was used for the deflagration and/or detonation test.

In any of the tests, the integrated temperature sensor(s) (8) shall produce a signal that may be used to activate counter measures within a burning time of 50 % of the manufacturer's specified burning time,  $t_{BT}$ , where  $\frac{t_{BT}}{2} \leq 15 \text{ min}$ .

A flame transmission is indicated by the flame detector (9). No flame transmission shall occur during the tests or when the flow is stopped. The burn time without flash back shall be recorded as the burning time,  $t_{BT}$ , expressed in minutes.

If the largest and smallest nominal sizes of a design series are satisfactorily tested, the intermediate nominal sizes may be considered acceptable without testing, but these flame arresters shall be marked with the shortest burning time,  $t_{BT}$ , found in the experimental tests.

Each size of in-line flame arresters greater than 1 000 mm shall be tested.

### 7.3.5 Endurance burning test

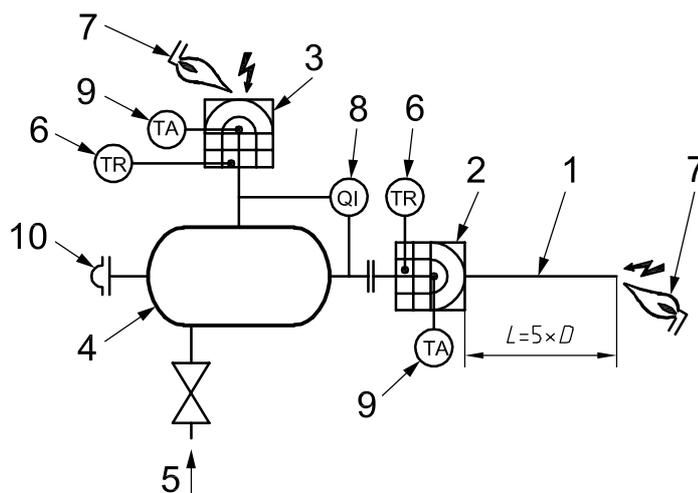
The test apparatus is shown in Figure 7 for an in-line and end-of-line flame arrester.

A flow meter shall be used to measure the mixture flow rate. The flame arrester shall be fitted with two temperature sensors for the test only.

One temperature sensor (item 6 in Figure 7) shall be mounted on the protected side. The location of this temperature sensor shall be left to the discretion of the test laboratory.

Another temperature sensor (item 9 in Figure 7) shall be fitted to the unprotected side to detect the stabilized flame (start of burning load).

The tests shall be carried out using a mixture as specified in Table 4.



### Key

- 1 outlet pipe
- 2 in-line flame arrester
- 3 end-of-line flame arrester
- 4 explosion-pressure-resistant containment (vessel or closed pipe work)
- 5 mixture inlet
- 6 temperature sensor for recording for tests only
- 7 pilot flame or spark igniter
- 8 flame detector for indication
- 9 test temperature sensor for alarm to detect stabilized flame
- 10 bursting diaphragm

**Figure 7 — Test apparatus for endurance burning test**

First, the critical flow rate  $\dot{V}_c$  shall be calculated from the open area  $A_0$  of the surface of the flame arrester element on the unprotected side and from the size and number of apertures per unit area. Assuming a uniform velocity of 75 % of a burning velocity  $v_1$  of the mixture across this area, calculate a critical flow rate  $\dot{V}_c$  according to Equation (2) in 7.3.4.

For non-measurable flame arrester elements, the critical flow rate  $\dot{V}_c$  may be obtained by using the same principle. The free area  $A_0$  of the flame arrester element surface can be estimated according to Equation (3) in 7.3.4.

The tests shall be carried out with a continuously operated pilot flame or spark. Ignite the mixture until the flame has stabilized on the surface of the flame arrester element.

Carry out the following preliminary testing for critical flow rates.

After flame stabilization, continue burning until the protected side temperature sensor indicates a temperature rise of 20 K and then stop the flow. Record the time from stabilization of the flame to the 20 K temperature increase.

Carry out this test procedure with flow rates  $\dot{V}_c$ ,  $0,5\dot{V}_c$  and  $1,5\dot{V}_c$ . In each of these tests, the flame arrester shall be at ambient temperature at the start.

If  $\dot{V}_C$  results in the shortest time to 20 K temperature increase, then  $\dot{V}_m = \dot{V}_C$ . If not, carry out two further tests with flow rates 50 % and 150 % of the flow rate which gave the shortest time in the first three tests.  $\dot{V}_m$  will be the flow rate that results in the shortest time in all five tests. When determining the flow rate  $\dot{V}_m$ , flame arrester elements may be replaced between the tests.

The endurance burn test shall be carried out with the flow rate  $\dot{V}_m$ , using the original flame arrester element, without modification, that was used for the deflagration and/or detonation test. Maintain the mixture composition and the flow rate  $\dot{V}_m (\pm 5 \%)$  until a stable temperature is established at the temperature sensor on the protected side. The temperature rise on the protected side shall then not exceed 10 K in 10 min. The flow of the mixture shall be stopped when a stable temperature is established, but not before 2 h of burning.

The flame detector (8) shall indicate any flame transmission. No flame transmission shall occur during the tests or when the flow is stopped.

All types and nominal sizes shall be tested.

Modifications that do not change the flame arrester element and are part of the housing to which the flame arrester element is fitted do not require retesting, e.g. flame arresters with integrated pressure and/or vacuum valves.

## 7.4 Limits for use

### 7.4.1 General

The general limits for use are as indicated below.

- a) The operational temperature  $T_0$  shall be limited as follows:
  - $20 \text{ °C} \leq T_0 \leq 60 \text{ °C}$  when testing is at atmospheric conditions ( $T_{TB} \leq 60 \text{ °C}$ );
  - $T_0 \leq T_{TB}$  where  $T_{TB} \leq 150 \text{ °C}$  (see 6.8.1, paragraph 4).
- b) The operational pressure  $p_0$  shall be limited as follows:
  - 1) for flame arresters with measurable element:
    - end-of-line flame arresters with or without pressure and/or vacuum valve on the protected side:
 
$$(0,8 \times 10^5 \text{ Pa}) \leq p_0 \leq (1,1 \times 10^5 \text{ Pa})$$
 when testing is at atmospheric pressure ( $p_{TB} \approx 10^5 \text{ Pa}$ );
   
 — in-line flame arresters:
 
$$p_0 \leq p_{TB}$$
 where  $p_{TB} \leq 1,6 \times 10^5 \text{ Pa}$ ;
  - 2) for flame arresters with non-measurable element:
    - $p_0 \leq 0,9 \times p_{TB}$  where  $p_{TB} \leq 1,6 \times 10^5 \text{ Pa}$ .

Use shall be limited to gas-air mixtures with an MESG equal to or greater than that tested.

### 7.4.2 In-line flame arrester

#### 7.4.2.1 General

For an in-line flame arrester, the pipe diameter on the protected side shall be no less than the pipe diameter on the unprotected side.

For an in-line flame arrester, the pipe diameter on the unprotected side shall be no greater than the flame arrester connection.

#### 7.4.2.2 In-line deflagration flame arrester

The use of in-line deflagration flame arresters tested in accordance with 7.3.2.2 shall be limited to the following conditions:

- a) the ratio of pipe length (between the potential ignition source and the flame arrester) and pipe diameter shall not exceed the tested ratio  $L_u/D$ ;
- b) at least 10 % of the cross sectional area of the pipe shall be open at the ignition source;
- c) pipe branches and valves on the unprotected side shall be installed as close as possible to the in-line deflagration flame arrester.

#### 7.4.3 Pre-volume flame arrester

The use of pre-volume flame arresters shall be limited to enclosures, contents and pipe work on the unprotected side as used or simulated in the test.

#### 7.4.4 Detonation flame arrester

Detonation flame arresters may be used for open and closed pipe work on the unprotected side.

Detonation flame arresters tested at  $p_{TB}$  are suitable for operational pressures  $p_0 \leq p_{TB}$  in the same or smaller pipe size when the application is limited to mixtures with an MESG equal to or greater than that tested.

Unstable detonation flame arresters (Type 1 and Type 2) are designed and tested for stopping deflagrations and stable and unstable detonations; there are no limits imposed on their installation.

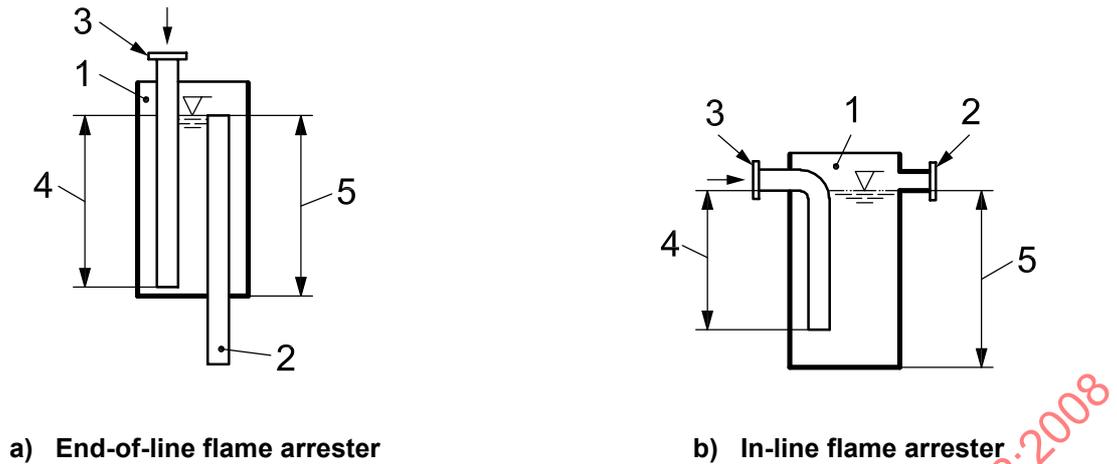
Stable detonation flame arresters (Type 3 and Type 4) are designed and tested for stopping deflagrations and stable detonations; they shall only be used in combination with additional protection measures. This fact and suitable additional measures shall be addressed in the instructions for use (see 11.1).

## 8 Specific requirements for liquid product detonation flame arresters

### 8.1 Liquid seals

A flame arrester consisting of a liquid seal formed by the liquid product may be an end-of-line flame arrester [see Figure 8 a)] or an in-line flame arrester [see Figure 8 b)].

The housings for liquid seals suitable for emptying operations shall incorporate a safety device that prevents loss of the sealing liquid.



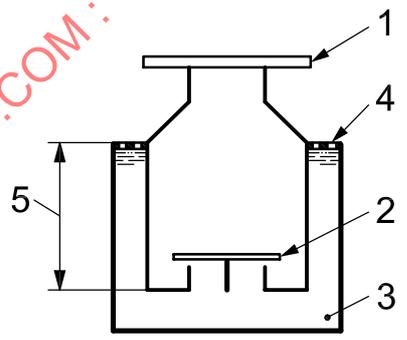
**Key**

- 1 housing
- 2 overflow pipe/outlet pipe
- 3 immersion pipe
- 4 immersion depth
- 5 filling height

**Figure 8 — Liquid product detonation flame arrester**

**8.2 Foot valves**

There shall be an end-of-line flame arrester incorporating a non-return valve (foot valve) in an immersion cup, providing an immersion depth of not less than that specified by the manufacturer. A screen or perforated plate shall protect the valve seal from solid particles (see Figure 9).



**Key**

- 1 valve housing
- 2 valve disc
- 3 immersion cup
- 4 perforated plate or screen
- 5 immersion depth

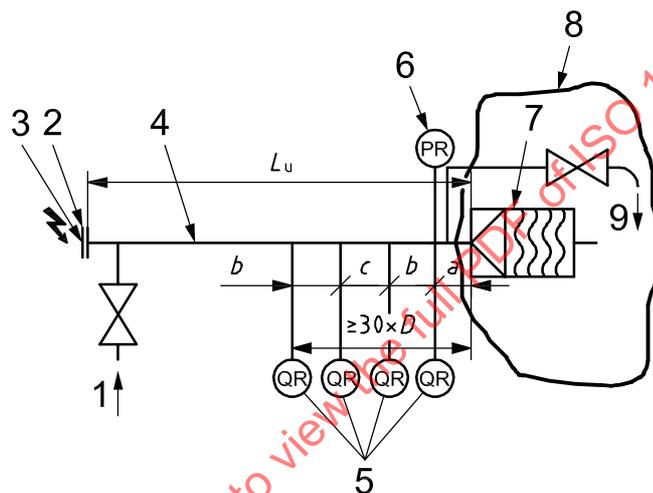
**Figure 9 — End-of-line flame arrester incorporating a non-return valve (foot valve)**

### 8.3 Flame transmission test

Liquid product detonation flame arresters shall be tested under atmospheric conditions for detonations only. The flame arrester shall be filled either with the liquid to be used in operation, or alternatively with gasoline having a boiling range from 100 °C to 140 °C. These liquids may also be used in tests for group IIB mixtures. The filling height shall be recorded (see Figures 8 and 9).

In-line and end-of-line flame arresters shall be tested in accordance with the test procedure given in 7.3.3.2, and if necessary in accordance with 7.3.3.4, but using the test apparatus shown in Figure 10. On the basis of the operational conditions for these flame arresters, only three stable detonation tests shall be carried out.

The flame arrester test shall be carried out in the orientation required in service.



#### Key

- 1 mixture inlet
- 2 explosion-pressure-resistant containment (vessel or closed pipe work)
- 3 ignition source
- 4 unprotected pipe (length  $L_u$ , diameter  $D$ ) with bypass
- 5 flame detectors for recording the flame velocity measurement
- 6 pressure transducer for recording
- 7 liquid product detonation flame arrester
- 8 plastic bag ( $\varnothing \geq 1,2$  m; length  $\geq 2,5$  m; foil thickness  $\geq 0,05$  mm)
- 9 mixture outlet (bypass)

$$a = (200 \pm 50) \text{ mm}$$

$$b \geq 3 \times D, \text{ but } b \geq 100 \text{ mm}$$

$$c \geq 500 \text{ mm}$$

**Figure 10 — Test apparatus for liquid product detonation flame arresters**

## 8.4 Limits for use

If a liquid product detonation flame arrester is satisfactorily tested for detonations, it may be considered acceptable for deflagrations without further testing. The operation pressure for the product-air mixture shall be limited to test pressure.

NOTE The operation pressure for the liquid flow is not limited by flame arresting requirements.

Liquid product detonation flame arresters suitable for emptying operations shall have the flow rate restricted so that the pressure drop of the safety device that prevents loss of sealing liquid does not exceed the static pressure given by the immersion depth (see 8.1). For filling operations, there are no such limitations.

## 9 Specific requirements for dynamic flame arresters (high velocity vent valves)

### 9.1 General

Dynamic flame arresters shall be tested for flame transmission (see 9.2) and for endurance burning (see 9.3). All types and sizes shall be tested.

The set pressure and closing pressure of the dynamic flame arrester shall be specified.

For any type, testing shall be carried out at the lowest and highest settings and closing pressures intended for approval.

For the tests described in 9.2 and 9.3 below, the completion of the undamped oscillation test in accordance with Clause A.4 is required to provide  $L_M$ ,  $D_M$  and  $V_M$ .

### 9.2 Flame transmission test

The test apparatus is shown in Figure 11. The pipe length  $L_m$  between the explosion-pressure-resistant containment and the dynamic flame arrester shall not exceed  $L_M$ . The volume  $V_M$  of the explosion-pressure-resistant containment and the pipe diameter  $D_M$  shall be as used in Clause A.4.

A temperature sensor for testing shall be attached to the dynamic flame arrester as close as possible to the stabilized flame. Ignition shall be maintained by a pilot flame. The pilot flame shall burn propane and provide a stabilized flame. The pilot flame shall be positioned as close as possible to the mixture outlet to atmosphere, visually not more than 20 mm away measured horizontally (see Figure 12). If the pilot flame is blown out, the testing shall be started over again.

A gas-air mixture as specified in 6.8.2 shall be fed into the explosion-pressure-resistant containment.

The flow rate into the containment shall be increased in ten steps.

The step width depends on the dynamic flame arrester characteristic, as follows:

- for a dynamic flame arrester with  $\dot{V}_{CL} > 0$ , the step width shall be  $0,1 \times \dot{V}_{CL}$  with a starting point of  $0,1 \times \dot{V}_{CL}$ ;
- for a dynamic flame arrester with  $\dot{V}_{CL} = 0$ , the step width shall be 10 % of the flow rate of the fully open dynamic flame arrester; this value of the step width shall also be taken as the starting point.

The duration of each test step shall be chosen depending on the dynamic flame arrester action, as specified below.

- a) If at some point during the sequence of tests the dynamic flame arrester turns into an open position while steadily relieving, the test duration shall be a minimum of 5 min and shall also achieve a stationary pressure in the containment. After that, the inflow to the containment shall be stopped (e.g. by a shut-off valve), thereby forcing the dynamic flame arrester to close.
- b) If the dynamic flame arrester varies periodically between the closed and open position associated with a varying pressure in the containment, the test duration shall be a minimum of 5 min and shall furthermore cover a minimum of five closing actions before the next flow rate step is adjusted.

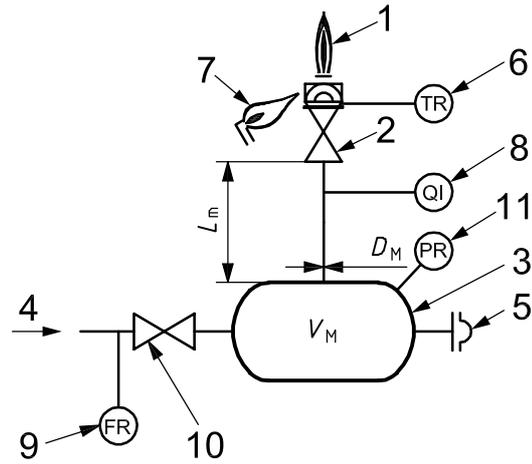
If the flow rate readings vary due to the opening and closing cycles [see case b) above], the appropriate time averaged flow rate shall be recorded.

This procedure shall be carried out with the dynamic flame arrester in the upright position and repeated with the dynamic flame arrester inclined 10 degrees to the vertical orientation.

No flame transmission shall occur during these tests.

### 9.3 Endurance burning test

The test apparatus is shown in Figure 11. The pipe length  $L_m$  between the explosion-pressure-resistant containment and dynamic flame arrester shall not exceed  $L_M$ . A temperature sensor for testing shall be attached to the dynamic flame arrester as close as possible to the stabilized flame. Ignition shall be maintained by a pilot flame. The pilot flame shall burn propane and provide a stabilized pilot flame. The pilot flame shall be positioned as close as possible to the mixture outlet to atmosphere, not more than 20 mm away measured horizontally (see Figure 12).



**Key**

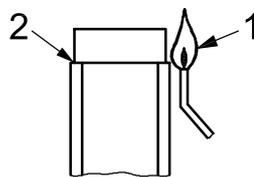
- 1 flame
- 2 dynamic flame arrester
- 3 explosion-pressure-resistant containment with the volume  $V_M$  in  $m^3$
- 4 mixture inlet
- 5 bursting diaphragm
- 6 temperature sensor for recording (for tests only)
- 7 pilot flame
- 8 flame detector for indication
- 9 flow meter for recording
- 10 shut-off valve
- 11 pressure sensor for recording

$D_M$  diameter of the pipe on the protected side in accordance with Clause A.4

$L_m$  pipe length upstream of the dynamic flame arrester

$V_M$  volume of the explosion-pressure-resistant containment

**Figure 11 — Test apparatus for dynamic flame arresters**



**Key**

- 1 pilot flame
- 2 mixture outlet to atmosphere

**Figure 12 — Positioning of pilot flame and mixture outlet in endurance burning test for dynamic flame arrester**

Using a gas-air mixture as specified in Table 3, the pressure in the pressure resistant containment shall be increased to force the dynamic flame arrester open and then shall be maintained at 10 % above the established closing pressure. The corresponding flow rate  $\dot{V}_0$  shall be recorded. If no stabilized burning is possible under these conditions, the mixture shall be gradually enriched until the flame is stabilized. Without changing that mixture composition, the flow shall be increased in increments of 20 % of  $\dot{V}_0$ , and after each increment, the flow shall be maintained until the temperature rise is less than 10 K/min, but for a minimum of 5 min.

When the temperature starts to decrease, the corresponding flow  $\dot{V}_E$  is the maximum flow that shall be used in this test. The flow shall then be reduced in increments of 10 % of  $\dot{V}_0$  and after each step shall be maintained until the temperature change is less than 10 K/min, but for a minimum of 5 min. Flow rates for which the corresponding temperature has been recorded need not be repeated, and tests need not be made at flow rates below  $\dot{V}_0$ . Upon completion, the flow rate yielding the highest temperature shall be recorded as  $\dot{V}_m$  and the burning at that rate shall be continued until the change of temperature indicated by the test temperature sensor does not exceed 10 K in 10 min.

For enriched mixtures, the concentration of fuel shall be gradually reduced as far as possible towards the initial value (see Table 3) keeping the flame stabilized. The flow shall be stopped and no flame transmission shall occur.

#### 9.4 Limits for use

The use of a dynamic flame arrester shall be limited to ambient temperatures. The pipe length on the protected side shall not exceed  $L_m$ , as successfully tested in 9.2 and 9.3, and the diameter shall not be less than  $D_M$ , while the minimum gaseous volume (ullage space) available at any time in the protected tank shall not be less than  $V_M$ .

### 10 Specific requirements for hydraulic flame arresters

#### 10.1 Equipment

Hydraulic flame arresters are in-line flame arresters. An example is shown schematically in Figure 13. They consist of a mixture inlet (3), a container (1) with a water seal (12), one or more immersion pipe(s) (2) and a mixture outlet (16). The design and construction shall ensure that the immersion depth is always constant within  $\pm 5$  mm.

Hydraulic flame arresters shall include the following features:

- a) a level indicator with an optical display (4) for the immersion depth at rest ( $Z_R$ ) and the operational immersion depth ( $Z_0$ );
- b) automatic equipment (5) to maintain the water level above the minimum operational immersion depth ( $Z_{0min}$ );
- c) a temperature sensor (8) for the water seal;
- d) an integrated temperature sensor (7) above the water seal (12) to indicate a stabilized flame.

## 10.2 Flame transmission test

### 10.2.1 General

Hydraulic flame arresters shall be tested for short time burning, deflagration and stable detonation in succession. Before ignition, mixtures shall be at ambient conditions on the unprotected side. Each test shall be carried out with the minimum immersion depth at rest ( $Z_{Rmin}$ ) and with the minimum operational immersion depth ( $Z_{0min}$ ) specified by the manufacturer. The flow rate of the mixture shall be recorded with a sensor (9) at the inlet, and flame transmission shall be detected with a flame detector (18) in the inlet pipe.

### 10.2.2 Short time burning test

The test apparatus is as shown in Figure 13, with the mixture outlet pipe (6) removed if necessary.

The ignition source (14) shall be positioned ( $100 \pm 20$ ) mm above the water seal (12). The test shall be carried out for not less than 5 min with a water seal temperature  $\geq 10$  °C, at which time the temperature shall remain  $\leq 30$  °C.

The safe volume flow rate  $\dot{V}_{max}$  shall be determined for the minimum immersion depth at rest ( $Z_{Rmin}$ ) and the minimum operational immersion depth ( $Z_{0min}$ ) at which no flame transmission occurs. Four tests shall be carried out with  $\dot{V}_{max}$ . No flame transmission shall occur in any of the tests.

### 10.2.3 Deflagration test

The test apparatus is as shown in Figure 13, with the mixture outlet pipe (6) in place and equipped with two flame detectors (18) in a straight part of the pipe close to the mixture outlet (16) (see also Figure 2).

The maximum diameter  $D$  of the mixture outlet pipe (6) shall be used for all tests for which the hydraulic flame arrester is acceptable. The ignition source (13) shall be positioned at the open end of the mixture outlet pipe (6).

Tests shall be carried out by using a test mixture as specified in 6.8.2.

The deflagration test shall be carried out at the minimum immersion depth at rest ( $Z_{Rmin}$ ) and minimum operational immersion depth ( $Z_{0min}$ ) with the mixture flow rate at  $\dot{V}_{max}$ , as determined in 10.2.2. The test shall be carried out with the following lengths of mixture outlet pipe (6):

—  $L_u = 50 \times D$ ;

—  $L_u = 100 \times D$ .

Carry out three tests on each length.

If flame transmission takes place, the flow shall be reduced to a level where no flame transmission occurs. This reduced flow shall then be recorded as  $\dot{V}_{max}$ .

### 10.2.4 Detonation test

The test apparatus is as shown in Figure 13, with the mixture outlet pipe (6) in place and equipped with four flame detectors (15) in the straight part of the pipe close to the outlet (16) (see also Figure 4). All tests shall be carried out with the mixture outlet pipe (6) with the maximum diameter  $D$  for which the hydraulic flame arrester shall be used.

The mixture outlet pipe (6) shall have a blind flange equipped with an ignition source (13). The mixture outlet pipe (6) shall have sufficient length to develop a stable detonation (see 7.3.3.2 for further details).

Tests shall be carried out by using a test mixture as specified in 6.8.2.

Carry out three detonation tests with the mixture at rest and with the minimum immersion depth at rest ( $Z_{Rmin}$ ), and with the minimum operational immersion depth ( $Z_{0min}$ ) for which the hydraulic flame arrester is acceptable.

No flame transmission shall occur in any of the tests.

### 10.3 Limits for use

The use of a hydraulic flame arrester shall be limited to the following conditions:

- a) the flow rate does not exceed the safe value  $\dot{V}_s = 0,9 \times \dot{V}_{max}$ ;
- b) the operational immersion depth is kept above the tested minimum value  $Z_{0min}$ ;
- c) the mixture on the unprotected side is at ambient temperature and pressure.

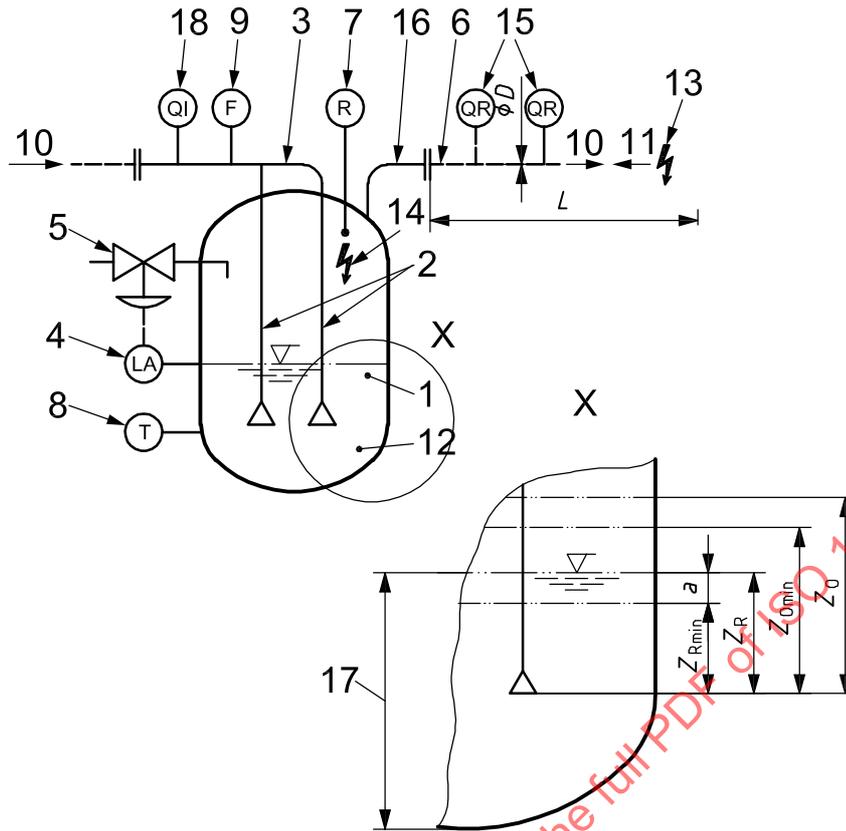
Failure of any of the features listed under points a) to d) in 10.1 shall operate an alarm and stop the gas flow.

If any temperature recorded in accordance with points c) and/or d) in 10.1 exceeds or falls below the specified limits, or if the minimum operational immersion depth  $Z_{0min}$  falls below the specified level, or if the volume flow exceeds  $\dot{V}_s$ , the flow shall be stopped within 30 s.

If for operational reasons the mixture flow cannot be stopped, it shall be inerted.

The immersion depth at rest  $Z_R$  and the operational immersion depth  $Z_0$  shall not be less than the manufacturer's recommended safety margin and greater than the minimum water seal immersion depth at rest  $Z_{Rmin}$  and the minimum operational water seal immersion depth  $Z_{0min}$  at which the maximum volume flow  $\dot{V}_{max}$  has been established.

The operational immersion depth  $Z_0$  shall be maintained by automatic control of the water supply [see item (5) in Figure 13] to ensure that the minimum operational immersion depth  $Z_{0min}$  is not reached.



**Key**

- 1 container for the hydraulic flame arrester medium
- 2 gas or vapour mixture immersion pipe(s)
- 3 gas or vapour mixture inlet
- 4 water seal level indicator with an optical display
- 5 automatic water seal level control
- 6 mixture outlet pipe (length  $L$ ; diameter  $D$ )
- 7 temperature sensor for alarm to indicate a stabilized flame above the water seal
- 8 water seal temperature sensor
- 9 mixture volume flow sensor
- 10 direction of mixture flow
- 11 direction of flame propagation
- 12 water seal
- 13 ignition source for flame transmission tests
- 14 ignition source for stabilized burning tests
- 15 flame detector for recording flame velocity
- 16 mixture outlet
- 17 filling height
- 18 flame detector to indicate flame transmission

$a = (25 \pm 3) \text{ mm}$

**Figure 13 — Test apparatus for hydraulic flame arrester**

## 11 Information for use

### 11.1 Instructions for use

The manufacturer shall provide the following minimum written instructions and information:

- a) the information marked on the flame arrester and an explanation of its meaning;
- b) information concerning the classification of the flame arrester as outlined in Clause 5;
- c) all details of the operational requirements, including the specific limits in accordance with 7.4, 8.4, 9.4 and 10.3, as appropriate; the maximum operational temperature and pressure shall be given;
- d) static flame arresters classified as safe for endurance burning shall include a warning that safe use is limited to hydrocarbons, and that extension to other chemicals may require testing with these specific chemicals;
- e) short time burning flame arresters and hydraulic flame arresters shall include a warning that additional external safety equipment is required; all data that are necessary to characterize the integrated temperature sensor used for the stabilized burning test shall be documented; if the user equips the flame arrester with his own temperature sensor, this sensor shall fulfil these requirements as a minimum;
- f) a full description of installation and maintenance procedures; maintenance shall include cleaning instructions and the procedure to be followed after deflagration, detonation or stabilized burning conditions have taken place;
- g) the user should be aware of the high stresses exerted on the fixing points of the flame arrester and on the unprotected side of the piping especially in the case of a detonation (high pressure shock wave); stresses from adjoining pipe work shall be limited to acceptable levels by appropriate installation, selection of material and construction;
- h) stable detonation flame arresters shall only be used in combination with additional protection measures, e.g. flame arresters and/or explosion isolation systems in series, as well as measures for concentration control and for ignition source control; the integral safety of the combined installation shall be assessed, taking account of any hazardous area classification and of the likelihood of possible ignition sources (see Annex D for guidance);
- i) for end-of line deflagration arresters, a minimum distance shall be given for any external installation that might impair flame or flow.

### 11.2 Marking

#### 11.2.1 Flame arrester

##### 11.2.1.1 General information

The flame arrester shall be marked with the following information:

- a) name and address of the manufacturer;
- b) designation of series;
- c) serial number;
- d) year of construction [if not incorporated in point c)];
- e) the number of this International Standard;