

---

---

**Iron ores for shaft direct-reduction  
feedstocks — Determination of the  
reducibility index, final degree of  
reduction and degree of metallization**

*Minerais de fer pour charges utilisées dans les procédés par réduction  
directe — Détermination de l'indice de réductibilité, du degré final de  
réduction et du degré de métallisation*

STANDARDSISO.COM : Click to view the PDF of ISO 11258:2007



**PDF disclaimer**

This PDF file may contain embedded typefaces. In accordance with Adobe's licensing policy, this file may be printed or viewed but shall not be edited unless the typefaces which are embedded are licensed to and installed on the computer performing the editing. In downloading this file, parties accept therein the responsibility of not infringing Adobe's licensing policy. The ISO Central Secretariat accepts no liability in this area.

Adobe is a trademark of Adobe Systems Incorporated.

Details of the software products used to create this PDF file can be found in the General Info relative to the file; the PDF-creation parameters were optimized for printing. Every care has been taken to ensure that the file is suitable for use by ISO member bodies. In the unlikely event that a problem relating to it is found, please inform the Central Secretariat at the address given below.

STANDARDSISO.COM : Click to view the full PDF of ISO 11258:2007



**COPYRIGHT PROTECTED DOCUMENT**

© ISO 2007

All rights reserved. Unless otherwise specified, no part of this publication may be reproduced or utilized in any form or by any means, electronic or mechanical, including photocopying and microfilm, without permission in writing from either ISO at the address below or ISO's member body in the country of the requester.

ISO copyright office  
Case postale 56 • CH-1211 Geneva 20  
Tel. + 41 22 749 01 11  
Fax + 41 22 749 09 47  
E-mail [copyright@iso.org](mailto:copyright@iso.org)  
Web [www.iso.org](http://www.iso.org)

Published in Switzerland

## Contents

Page

Foreword.....	iv
Introduction .....	v
1 Scope .....	1
2 Normative references .....	1
3 Terms and definitions.....	1
4 Principle.....	2
5 Sampling, sample preparation and preparation of test portions.....	2
6 Apparatus .....	2
7 Test conditions .....	3
8 Procedure .....	4
9 Expression of results .....	5
10 Test report .....	7
11 Verification .....	8
Annex A (normative) Flowsheet of the procedure for the acceptance of test results .....	11
Annex B (informative) Derivation of equation for reducibility .....	12
Annex C (informative) Derivation of equation for degree of metallization from $R_{90}$ .....	14

## Foreword

ISO (the International Organization for Standardization) is a worldwide federation of national standards bodies (ISO member bodies). The work of preparing International Standards is normally carried out through ISO technical committees. Each member body interested in a subject for which a technical committee has been established has the right to be represented on that committee. International organizations, governmental and non-governmental, in liaison with ISO, also take part in the work. ISO collaborates closely with the International Electrotechnical Commission (IEC) on all matters of electrotechnical standardization.

International Standards are drafted in accordance with the rules given in the ISO/IEC Directives, Part 2.

The main task of technical committees is to prepare International Standards. Draft International Standards adopted by the technical committees are circulated to the member bodies for voting. Publication as an International Standard requires approval by at least 75 % of the member bodies casting a vote.

Attention is drawn to the possibility that some of the elements of this document may be the subject of patent rights. ISO shall not be held responsible for identifying any or all such patent rights.

ISO 11258 was prepared by Technical Committee ISO/TC 102, *Iron ore and direct reduced iron*, Subcommittee SC 3, *Physical testing*.

This second edition cancels and replaces the first edition (ISO 11258:1999), which has been revised to homogenise with other physical test standards prepared.

STANDARDSISO.COM : Click to view the full PDF of ISO 11258:2007

## Introduction

This International Standard concerns one of a number of physical test methods that have been developed to measure various physical parameters and to evaluate the behaviour of iron ores, including reducibility, disintegration, crushing strength, apparent density, etc. This method was developed to provide a uniform procedure, validated by collaborative testing, to facilitate comparisons of tests made in different laboratories.

The results of this test should be considered in conjunction with other tests used to evaluate the quality of iron ores as feedstocks for direct reduction processes.

This International Standard may be used to provide test results as part of a production quality control system, as a basis of a contract, or as part of a research project.

STANDARDSISO.COM : Click to view the full PDF of ISO 11258:2007

[STANDARDSISO.COM](https://standardsiso.com) : Click to view the full PDF of ISO 11258:2007

# Iron ores for shaft direct-reduction feedstocks — Determination of the reducibility index, final degree of reduction and degree of metallization

**CAUTION** — This International Standard may involve hazardous materials, operations and equipment. This standard does not purport to address all of the safety issues associated with its use. It is the responsibility of the user of this International Standard to establish appropriate safety and health practices and determine the applicability of regulatory limitations prior to its use.

## 1 Scope

This International Standard specifies a method to provide a relative measure for evaluating the extent and ease to which oxygen can be removed from iron ores, when reduced under conditions resembling those prevailing in shaft direct-reduction processes. It specifies the determination of the reducibility, final degree of reduction and degree of metallization.

This International Standard is applicable to lump ores and hot-bonded pellets.

## 2 Normative references

The following referenced documents are indispensable for the application of this International Standard. For dated references, only the edition cited applies. For undated references, the latest edition of the referenced document (including any amendments) applies.

ISO 2597-1:2006, *Iron ores — Determination of total iron content — Part 1: Titrimetric method after tin(II) chloride reduction*

ISO 3082:2000<sup>1)</sup>, *Iron ores — Sampling and sample preparation procedures*

ISO 5416:2006, *Direct reduced iron — Determination of metallic iron — Bromine-methanol titrimetric method*

ISO 9035:1989, *Iron ores — Determination of acid-soluble iron(II) content — Titrimetric method*

ISO 9507:1990, *Iron ores — Determination of total iron content — Titanium(III) chloride reduction methods*

ISO 11323:2002, *Iron ore and direct reduced iron — Vocabulary*

## 3 Terms and definitions

For the purposes of this document, the terms and definitions given in ISO 11323 apply.

---

1) Under revision to incorporate ISO 10836, *Iron ores — Method of sampling and sample preparation for physical testing*

## 4 Principle

The test portion is isothermally reduced in a fixed bed, at 800 °C, using a reducing gas consisting of H<sub>2</sub>, CO, CO<sub>2</sub> and N<sub>2</sub> and is weighed continuously or at specified time intervals until 90 min of reduction is reached. The rate of reduction is calculated at the oxygen/iron ratio of 0,9 and the final degree of reduction is calculated from the oxygen mass loss after 90 min ( $R_{90}$ ). The degree of metallization is calculated either by an equation based on  $R_{90}$  or by chemical analysis of the reduced product.

## 5 Sampling, sample preparation and preparation of test portions

### 5.1 Sampling and sample preparation

Sampling of a lot and preparation of a test sample shall be in accordance with ISO 3082.

The size range for pellets shall be 50 % – 16,0 mm + 12,5 mm and 50 % – 12,5 mm + 10,0 mm.

The size range for lump ores shall be 50 % – 20,0 mm + 16,0 mm and 50 % – 16,0 mm + 10,0 mm.

A test sample of at least 2,5 kg, on a dry basis, of the sized material shall be obtained.

Oven-dry the test sample to constant mass at 105 °C ± 5 °C and cool it to room temperature before preparation of the test portions.

NOTE Constant mass is achieved when the difference in mass between two subsequent measurements becomes less than 0,05 % of the initial mass of the test sample.

### 5.2 Preparation of test portions

Collect each test portion by taking ore particles at random.

NOTE Manual methods of division recommended in ISO 3082, such as riffing, can be applied to obtain the test portions.

At least 5 test portions, each of approximately 500 g (± the mass of 1 particle) shall be prepared from the test sample: 4 test portions for testing and 1 for chemical analysis.

Weigh the test portions to the nearest 1 g and register the mass of each test portion on its recipient label.

## 6 Apparatus

### 6.1 General

The test apparatus shall comprise:

- a) ordinary laboratory equipment, such as an oven, hand tools, a time-control device and safety equipment;
- b) a reduction-tube assembly;
- c) a furnace, equipped with a balance for permitting the mass loss of the test portion to be read at any time during the test;
- d) a system to supply the gases and regulate the flow rates;
- e) a weighing device.

Figure 1 shows an example of the test apparatus.

**6.2 Reduction tube**, made of non-scaling, heat-resistant metal to withstand temperatures higher than 800 °C and resistant to deformation. The internal diameter shall be 75 mm ± 1 mm. A removable perforated plate, made of non-scaling, heat-resistant metal to withstand temperatures higher than 800 °C, shall be mounted in the reduction tube to support the test portion and to ensure uniform gas flow through it. The perforated plate shall be 4 mm thick, with its diameter 1 mm less than the internal diameter of the tube. The holes in the plate shall be 2 mm to 3 mm in diameter at a pitch center distance of 4 mm to 5 mm.

Figure 2 shows an example of a reduction tube.

**6.3 Furnace**, having a heating capacity and temperature control able to maintain the entire test portion, as well as the gas entering the bed, at 800 °C ± 5 °C.

**6.4 Porcelain balls**, having a size range between 10,0 mm and 12,5 mm, and of sufficient quantity to form a double-layer bed on the perforated plate.

**6.5 Balance**, capable of weighing the reduction-tube assembly, including the test portion, to an accuracy of 1 g. The balance shall have an appropriate device to suspend the reduction-tube assembly.

**6.6 Gas-supply system**, capable of supplying the gases and regulating gas flow rates. It shall be ensured that a frictionless connection between the gas-supply system and the reduction tube does not affect the weight loss determination during reduction.

**6.7 Weighing device**, capable of weighing the test sample and test portions to an accuracy of 1 g.

## 7 Test conditions

### 7.1 General

Volumes and flow rates of gases are as measured at a reference temperature of 0 °C and at a reference atmospheric pressure of 101,325 kPa (1,013 25 bar).

### 7.2 Reducing gas

#### 7.2.1 Composition

The reducing gas shall consist of:

CO	30 % ± 1 % (volume fraction)
CO <sub>2</sub>	15 % ± 1 % (volume fraction)
H <sub>2</sub>	45 % ± 1 % (volume fraction)
N <sub>2</sub>	10 % ± 1 % (volume fraction)

#### 7.2.2 Purity

Impurities in the reducing gas shall not exceed:

O <sub>2</sub>	0,1 % (volume fraction)
H <sub>2</sub> O	0,2 % (volume fraction)

### 7.2.3 Flow rate

The flow rate of the reducing gas, during the entire reducing period, shall be maintained at 50 L/min  $\pm$  0,5 L/min.

### 7.3 Heating and cooling gas

Nitrogen (N<sub>2</sub>) shall be used as the heating and cooling gas. Impurities shall not exceed 0,1 % (volume fraction).

The flow rate of N<sub>2</sub> shall be maintained at 25 L/min until the test portion reaches 800 °C and at 50 L/min during the temperature-equilibration period. During cooling, it shall be maintained at 25 L/min.

### 7.4 Temperature of the test portion

The temperature of the entire test portion shall be maintained at 800 °C  $\pm$  5 °C during the entire reducing period and, as such, the reducing gas shall be preheated before entering the test portion.

## 8 Procedure

### 8.1 Number of determinations for the test

Carry out the test as many times as required by the procedure in Annex A.

### 8.2 Chemical analysis before reduction

Take, at random, one of the test portions prepared in 5.2 and use it for the determination of the iron(II) oxide content ( $w_1$ ) in accordance with ISO 9035 and total iron content ( $w_2$ ) in accordance with ISO 2597-1 or ISO 9507.

### 8.3 Reduction

Take, at random, another test portion prepared in 5.2 and record its mass ( $m_0$ ). Place it in the reduction tube (6.2) and level its surface.

NOTE 1 In order to achieve a more uniform gas flow, a double-layer bed of porcelain balls sized between 10,0 mm and 12,5 mm may be placed between the perforated plate and the test portion.

Close the top of the reduction tube. Connect the thermocouple, ensuring that its tip is in the centre of the test portion.

Insert the reduction tube into the furnace (6.3) and suspend it centrally from the balance (6.5), ensuring that there is no contact with the furnace wall or heating elements.

Connect the gas-supply system (6.6).

Pass a flow of N<sub>2</sub> through the test portion at a rate of at least 25 L/min  $\pm$  0,5 L/min and commence heating. When the temperature of the test portion approaches 800 °C, increase the flow rate to 50 L/min  $\pm$  0,5 L/min. Continue heating while maintaining the flow of the N<sub>2</sub> until the mass of the test portion is constant and the temperature is constant at 800 °C  $\pm$  5 °C for 10 min.

NOTE 2 In the case of lump ores, the temperature of the test portion should be raised to 800° C over more than 60 min to reduce decrepitation.

**DANGER — Carbon monoxide and the reducing gas, which contains carbon monoxide, are toxic and therefore hazardous. Testing shall be carried out in a well ventilated area or under a hood. Precautions should be taken for the safety of the operator in accordance with the safety codes of each country.**

Record the mass of the test portion ( $m_1$ ) and immediately introduce the reducing gas at a flow rate of 50 L/min  $\pm$  0,5 L/min to replace the N<sub>2</sub>. Record the mass of the test portion ( $m_t$ ) at least every 3 min for the first 15 min, and thereafter at 10 min intervals. After 90 min of reduction, record the mass of the test portion ( $m_2$ ), turn off the power and replace the reducing gas by N<sub>2</sub> at a flow rate of 25 L/min. The flow of N<sub>2</sub> should be continued until the test portion is below 50 °C.

#### 8.4 Chemical analysis after reduction

Pulverise the entire reduced material and determine its total iron content ( $w_t$ ) in accordance with ISO 2597-1 or ISO 9507, and its metallic iron content ( $w_0$ ) in accordance with ISO 5416.

NOTE If desired, the mass percentage of combined carbon in the reduced test portion can be determined by applying ISO 9686:2006, *Direct reduced iron — Determination of carbon and/or sulfur — High-frequency combustion method with infrared measurement*.

### 9 Expression of results

#### 9.1 Calculation of the final degree of reduction ( $R_{90}$ )

The final degree of reduction,  $R_{90}$ , expressed as a percentage by mass, is calculated from the following equation 2):

$$R_{90} = \left( \frac{0,111 w_1}{0,430 w_2} + \frac{m_1 - m_2}{m_0 \times 0,430 w_2} \times 100 \right) \times 100$$

where

$m_0$  is the mass, in grams, of the test portion;

$m_1$  is the mass, in grams, of the test portion immediately before starting the reduction;

$m_2$  is the mass, in grams, of the test portion, after 90 min of reduction;

$w_1$  is the iron(II) oxide content, expressed as a percentage by mass, of the test portion prior to the test, determined in accordance with ISO 9035. It is calculated from the iron(II) content by multiplying it by the oxide conversion factor FeO/Fe(II) = 1,286;

$w_2$  is the total iron content, expressed as a percentage by mass, of the test portion prior to the test, determined in accordance with ISO 2597-1 and ISO 9507.

Record the result to one decimal place.

#### 9.2 Calculation of the reducibility indices $\frac{dR}{dt} (R=40)$ and $\frac{dR}{dt} (R=90)$

##### 9.2.1 Reduction curve

Prepare the reduction curve by plotting the degree of reduction  $R_t$  against time  $t$ , using the following equation:

$$R_t = \left( \frac{0,111 w_1}{0,430 w_2} + \frac{m_1 - m_t}{m_0 \times 0,430 w_2} \times 100 \right) \times 100$$

where

$m_t$  is the mass, in grams, of the test portion, after reduction time  $t$ .

Using the reduction curve, obtain and express the reducibility indices to 2 decimal places.

2) The derivation of the formula is given in Annex B.

**9.2.2 Reducibility index for 40 % reduction**

Read off, from the reduction curve, the time, in minutes, to attain degrees of reduction of 30 % and 60 %.

The reducibility index  $\frac{dR}{dt (R=40)}$  for 40 % reduction (O/Fe = 0,9), expressed as the rate of reduction, in %/min, is calculated from the following equation <sup>3)</sup>:

$$\frac{dR}{dt (R=40)} = \frac{33,6}{t_{60} - t_{30}}$$

where

- $t_{30}$  is the time, in minutes, to attain a degree of reduction of 30 %;
- $t_{60}$  is the time, in minutes, to attain a degree of reduction of 60 %;
- 33,6 is a constant.

**9.2.3 Reducibility index for 90 % reduction**

Read off, from the reduction curve, the time, in minutes, to attain degrees of reduction of 80 % and 95 %.

The reducibility index  $\frac{dR}{dt (R=90)}$  for 90 % reduction (O/Fe = 0,15), expressed as the rate of reduction, in %/min, is calculated from the following equation:

$$\frac{dR}{dt (R=90)} = \frac{13,9}{t_{95} - t_{80}}$$

where

- $t_{80}$  is the time, in minutes, to attain a degree of reduction of 80 %;
- $t_{95}$  is the time, in minutes, to attain a degree of reduction of 95 %;
- 13,9 is a constant.

**9.3 Calculation of the degree of metallization (M)**

**9.3.1 Determination of the degree of metallization from chemical analysis (M)**

The degree of metallization, *M*, expressed as a percentage by mass, is calculated from the following equation:

$$M = \frac{w_0}{w_t} \times 100$$

where

- $w_0$  is the metallic iron content, expressed as a percentage by mass, of the reduced test portion;
- $w_t$  is the total iron content, expressed as a percentage by mass, of the reduced test portion.

Express the result to one decimal place.

---

3) The derivation of the formula is given in Annex C.

### 9.3.2 Determination of the degree of metallization from $R_{90}$ ( $M_R$ )

During the preparation of the reduced test portion for chemical analysis, some reoxidation can occur. If the iron(II) oxide content before reduction ( $w_1$ ) is less than 2 %, the chemical analysis can be avoided and the degree of metallization  $M_R$ , expressed as a percentage by mass, can be calculated directly from  $R_{90}$  using the following equation 4):

$$M_R = 1,43 \times R_{90} - 43$$

Express the result to one decimal place.

### 9.4 Repeatability for $R_{90}$ and acceptance of test results

Follow the procedure in Annex A by using the repeatability values for  $R_{90}$  given in Table 1. The results shall be reported to one decimal place.

Table 1 — Repeatability ( $r$ ) for  $R_{90}$

Type of iron ore	$r$ %, absolute
Pellets	2,0
Lump ores	3,5

## 10 Test report

The test report shall include the following information:

- a reference to this International Standard, i.e. ISO 11258:2007;
- all details necessary for the identification of the sample;
- the name and address of the test laboratory;
- the date of the test;
- the date of the test report;
- the signature of the person responsible for the test;
- details of any operation and any test conditions not specified in this International Standard or regarded as optional, as well as any incident which may have had an influence on the results;
- the reducibility indices  $\frac{dR}{dt} (R=40)$  and  $\frac{dR}{dt} (R=90)$  ;
- the degree of metallization,  $M$  or  $M_R$ ;
- the final degree of reduction,  $R_{90}$ ;
- the total iron and iron(II) contents of the test portion before reduction.

---

4) The derivation of this formula is given in Annex C.

## 11 Verification

Regular checking of the apparatus is essential to assure test-result reliability. The frequency of checking is a matter for each laboratory to determine.

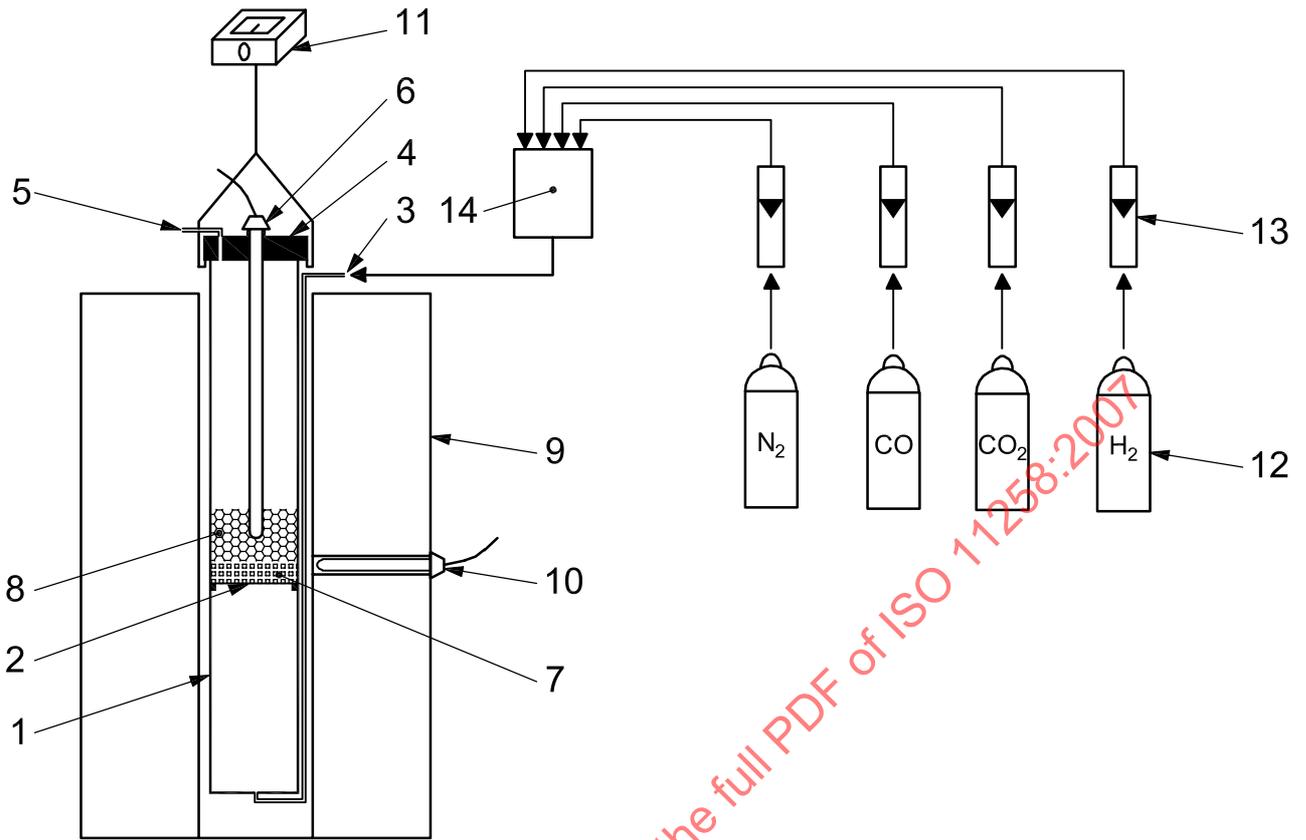
The conditions of the following items shall be checked:

- weighing device;
- reduction tube;
- temperature control and measurement devices;
- balance;
- gas flowmeters;
- purity of gases;
- recording system;
- time-control device.

It is recommended that internal reference material be prepared and used periodically to check test repeatability.

Appropriate records of verification activities shall be maintained.

STANDARDSISO.COM : Click to view the full PDF of ISO 11258:2007



**Key**

**Reduction tube**

- 1 reduction-tube wall
- 2 perforated plate
- 3 gas inlet
- 4 lid
- 5 gas outlet
- 6 thermocouple for measuring the reduction temperature
- 7 porcelain ball layer
- 8 test portion

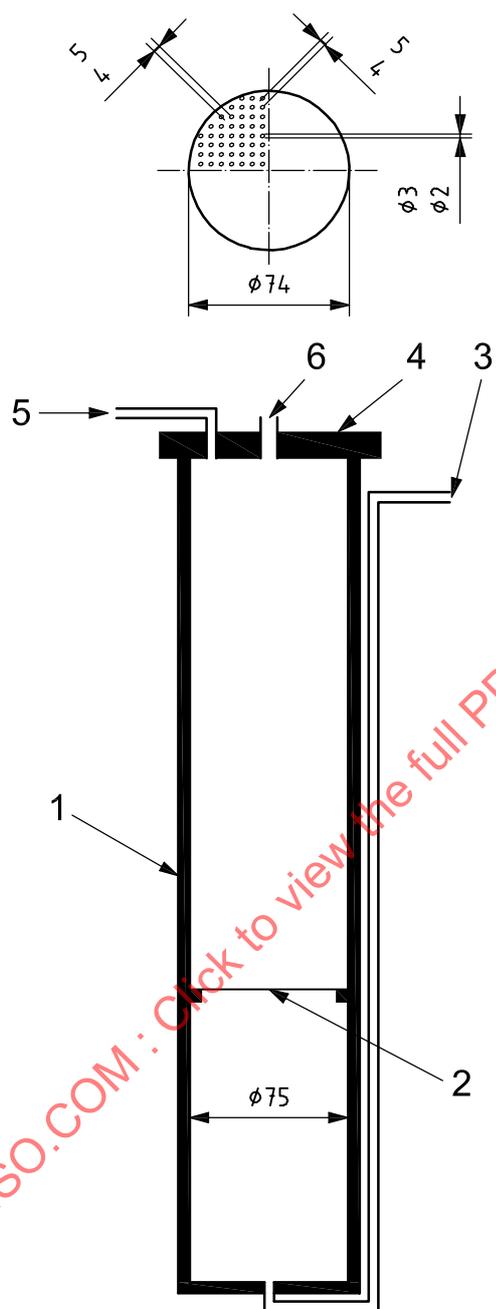
**Furnace**

- 9 electrically heated furnace
- 10 thermocouple for temperature regulation of furnace
- 11 balance

**Gas-supply system**

- 12 gas cylinders
- 13 gas flowmeters
- 14 mixing vessel

**Figure 1 — Example of test apparatus (schematic diagram)**



**Key**

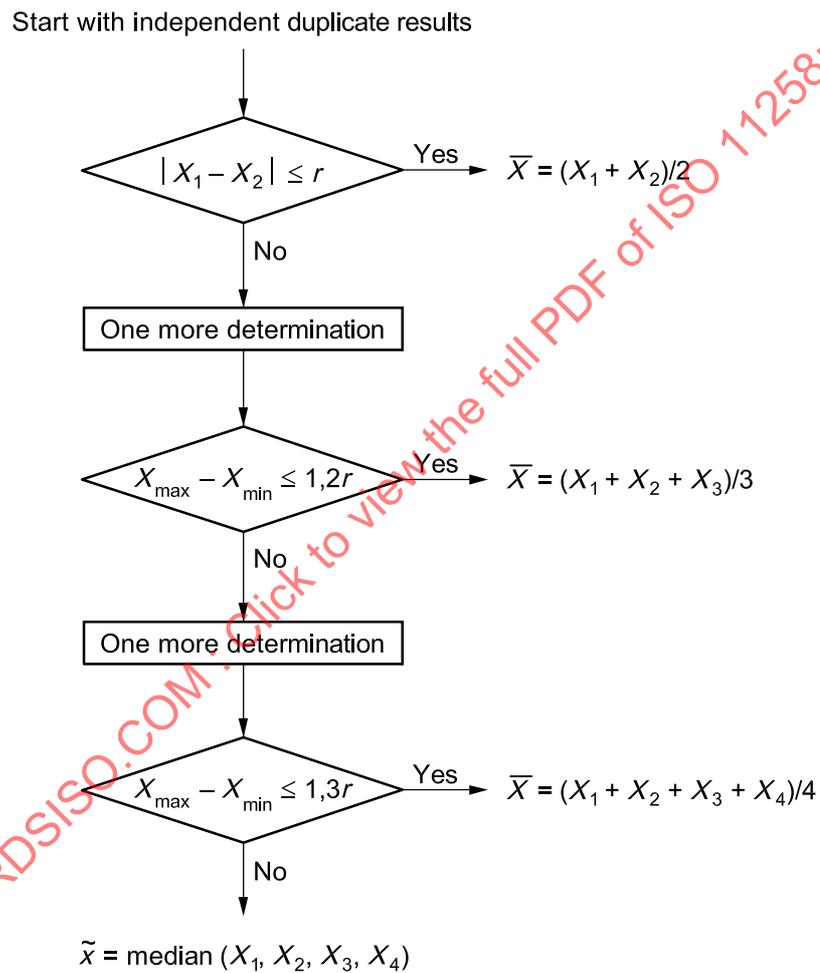
- 1 reduction-tube wall
- 2 perforated plate
- 3 opening for gas inlet
- 4 lid
- 5 opening for gas outlet
- 6 opening for thermocouple insertion

NOTE Dimensions not specified in the apparatus clause are shown for information only.

**Figure 2 — Example of reduction tube (schematic diagram)**

## Annex A (normative)

### Flowsheet of the procedure for the acceptance of test results



$r$ : see Table 1