



**International  
Standard**

**ISO 10302-1**

**Acoustics — Measurement of  
airborne noise emitted and  
structure-borne vibration induced  
by small air-moving devices —**

**Part 1:  
Airborne noise measurement**

*Acoustique — Mesurage du bruit aérien émis et des vibrations de  
structure induites par les petits équipements de ventilation —*

*Partie 1: Mesurage du bruit aérien*

**Second edition  
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## Foreword

ISO (the International Organization for Standardization) is a worldwide federation of national standards bodies (ISO member bodies). The work of preparing International Standards is normally carried out through ISO technical committees. Each member body interested in a subject for which a technical committee has been established has the right to be represented on that committee. International organizations, governmental and non-governmental, in liaison with ISO, also take part in the work. ISO collaborates closely with the International Electrotechnical Commission (IEC) on all matters of electrotechnical standardization.

The procedures used to develop this document and those intended for its further maintenance are described in the ISO/IEC Directives, Part 1. In particular, the different approval criteria needed for the different types of ISO document should be noted. This document was drafted in accordance with the editorial rules of the ISO/IEC Directives, Part 2 (see [www.iso.org/directives](http://www.iso.org/directives)).

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This document was prepared by Technical Committee ISO/TC 43, *Acoustics*, Subcommittee SC 1, *Noise*.

This second edition cancels and replaces the first edition (ISO 10302-1:2011), which has been technically revised.

The main changes are as follows:

- In [Clause 3](#), the most terms were editorially improved with no technical changes, and their cross-references to the main body were also clarified.
- In [Clause 4](#), the allowable fan static pressure range, 750 Pa for a full-size plenum, was extended up to 1,500 Pa for a half-size plenum and 3,000 Pa for a quarter-size plenum.
- In [Clause 7](#), for the selection of points of operation, in addition to the existing Method A (conventional method), Method B (alternative method) was introduced.
- In [Clause 11](#), Note was amended to clarify the reference to [Annex D](#).
- In [Annex A](#), to be consistent to the definition of micro-fan ([3.1.2](#)), the abscissa of [Figure A.1](#) and related descriptions were amended.

A list of all parts in the ISO 10302 series can be found on the ISO website.

Any feedback or questions on this document should be directed to the user's national standards body. A complete listing of these bodies can be found at [www.iso.org/members.html](http://www.iso.org/members.html).

## Introduction

This document shows in detail methods for determining and reporting the airborne noise emissions of small air-moving devices (AMDs) used primarily for cooling electronic equipment, such as that for information technology and telecommunications.

To provide compatibility with measurements of acoustical noise emitted by such equipment, this document uses the noise emission descriptors and sound power measurement methods of ISO 7779. The descriptor of overall airborne noise emission of the AMD under test is the A-weighted sound power level. The one-third-octave-band sound power level is the detailed descriptor of the noise emission. Octave-band sound power levels may be provided in addition to the one-third-octave-band sound power levels.

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# Acoustics — Measurement of airborne noise emitted and structure-borne vibration induced by small air-moving devices —

## Part 1: Airborne noise measurement

### 1 Scope

This document specifies methods for measuring the airborne noise emitted by small air-moving devices (AMDs), such as those used for cooling electronic, electrical, and mechanical equipment where the sound power level of the AMD is of interest.

Examples of these AMDs include propeller fans, tube-axial fans, vane-axial fans, centrifugal fans, motorized impellers, and their variations.

This document describes the test apparatus and methods for determining the airborne noise emitted by small AMDs as a function of the volume flow rate and the fan static pressure developed by the AMD on the test apparatus. It is intended for use by AMD manufacturers, by manufacturers who use AMDs for cooling electronic equipment and similar applications, and by testing laboratories. It provides a method for AMD manufacturers, equipment manufacturers and testing laboratories to obtain comparable results. Results of measurements made in accordance with this document are expected to be used for engineering information and performance verification, and the methods can be cited in purchase specifications and contracts between buyers and sellers. The ultimate purpose of the measurements is to provide data to assist the designers of electronic, electrical or mechanical equipment which contains one or more AMDs.

Based on experimental data, a method is given for calculating the maximum volume flow rate of the scaled plenum up to which this document is applicable.

### 2 Normative references

The following documents are referred to in the text in such a way that some or all of their content constitutes requirements of this document. For dated references, only the edition cited applies. For undated references, the latest edition of the referenced document (including any amendments) applies.

ISO 3741, *Acoustics — Determination of sound power levels and sound energy levels of noise sources using sound pressure — Precision methods for reverberation test rooms*

ISO 3744, *Acoustics — Determination of sound power levels and sound energy levels of noise sources using sound pressure — Engineering methods for an essentially free field over a reflecting plane*

ISO 3745, *Acoustics — Determination of sound power levels and sound energy levels of noise sources using sound pressure — Precision methods for anechoic rooms and hemi-anechoic rooms*

ISO 5801, *Fans — Performance testing using standardized airways*

ISO 7779:2018, *Acoustics — Measurement of airborne noise emitted by information technology and telecommunications equipment*

ISO/IEC Guide 98-3, *Uncertainty of measurement — Part 3: Guide to the expression of uncertainty in measurement (GUM:1995)*

ANSI/ASA S2.32, *Methods for the experimental determination of mechanical mobility — Part 2: Measurements using single-point translational excitation*

JBMS-72-1:2010, *Acoustics — Method for the measurement of airborne noise emitted and structure-borne vibration induced by small air-moving devices — Part 1: Airborne noise measurement*

### 3 Terms and definitions

For the purposes of this document, the terms and definitions given in ISO 7779 apply.

ISO and IEC maintain terminology databases for use in standardization at the following addresses:

- ISO Online browsing platform: available at <https://www.iso.org/obp>
- IEC Electropedia: available at <https://www.electropedia.org/>

#### 3.1 General definitions

##### 3.1.1

##### **air-moving device**

##### **AMD**

##### **fan**

device for moving air which utilizes a rotating impeller driven by an electric motor with electronic or mechanical command

Note 1 to entry: An air-moving device has at least one inlet opening and at least one outlet opening. The openings can have elements for connection to ductwork or to other parts of the airflow path.

Note 2 to entry: Tests can be run with a particular frame, motor, and rotor, but with different accessories (e.g. finger guards). For the purposes of this document, each such configuration is referred to as an air-moving device.

Note 3 to entry: Within some industries, including information technology, the unmodified term “fan” means “axial flow air-moving device”, and the unmodified term “blower” means “centrifugal air-moving device”. In this document, the term “fan” is used to mean “air-moving device” and does not necessarily imply axial flow. Modifiers (such as axial, centrifugal or mixed flow) are added as necessary to distinguish between types.

##### 3.1.2

##### **micro-fan**

*air-moving device* (3.1.1) which has a maximum volume flow rate less than or equal to 0,015 m<sup>3</sup>/s

Note 1 to entry: Micro-fans are a subset of fans under test according to this document.

Note 2 to entry: ISO 5801 limits the range of applicability to Reynolds numbers of 12 000 or higher. This Reynolds number corresponds to the lower limit of volume flow rate of approximately 0,01 m<sup>3</sup>/s. Since lower volume fans are of interest for many cooling applications, the methodology of JBMS-72-1:2010, Annex A<sup>1)</sup> is used to measure the *p-q* curve of a micro-fan.

#### 3.2 Acoustical definitions

##### 3.2.1

##### **sound power level**

$L_W$   
ten times the logarithm to the base 10 of the ratio of the sound power,  $P$ , to a reference value,  $P_0$ , expressed in decibels

$$L_W = 10 \lg \frac{P}{P_0}$$

1) The English version of JBMS-72-1:2010, Annex A is freely available from <https://hyojunka.jbmia.or.jp/hyojun2/upload-v3/archive/JBMS-72-1-1.pdf>.

where the reference value,  $P_0$ , is 1 pW

Note 1 to entry: If a specific frequency weighting as specified in IEC 61672-1<sup>[8]</sup> and/or specific frequency bands are applied, this should be indicated by appropriate subscripts; e.g.  $L_{WA}$  denotes the A-weighted sound power level.

### 3.2.2

#### frequency range of interest

range extending from the 100 Hz one-third-octave band to the 10 kHz one-third-octave band

Note 1 to entry: The centre frequencies of these one-third-octave bands are defined in ISO 266<sup>[1]</sup>.

Note 2 to entry: For small, low-noise fans to be measured (i.e., micro-fans), depending on the size of applicable plenum, the radius of the test hemisphere may be reduced to less than 1 m, but not less than 0,5 m (see 8.2.1). However, a radius less than 1 m could itself impose limits on the frequency range over which tests are performed. For details, reference is made to ISO 7779:2018, B.1.

### 3.2.3

#### insertion loss of test plenum

$\Delta L$

sound power level (3.2.1) difference due to the presence of test plenum, defined as follows:

$$\Delta L_W = L_{W,out} - L_{W,in}$$

where

$L_{W,out}$  is the sound power level, in decibels, of a sound source determined when installed outside the test plenum;

$L_{W,in}$  is the sound power level, in decibels, of a sound source determined when installed inside the test plenum.

Note 1 to entry: The insertion loss of the test plenum is expressed in decibels.

## 3.3 Aerodynamic definitions

### 3.3.1

#### test plenum

structure on to which the air-moving device under test is mounted for acoustical noise emission measurements

Note 1 to entry: The plenum provides a flow resistance to the air-moving device, but permits sound from the air-moving device to radiate freely into the test room with only minimal attenuation. Thus, the sound power radiated by the air-moving device can be determined from acoustical measurements made outside the test plenum.

### 3.3.2

#### AMD aerodynamic performance curve

*p-q* curve

presentation of fan static pressure as a function of volume flow rate under *standard air conditions* (3.3.6) and constant operating voltage and frequency

Note 1 to entry: For the purpose of this document, a qualifier, “aerodynamic”, before “performance curve” is inserted to distinguish from acoustical noise emission characteristics against volume flow rate.

Note 2 to entry: The presentation is derived in accordance with ISO 5801 or Annex A, which complement each other. The method for small air-moving devices of volume flow rate up to 0,015 m<sup>3</sup>/s is specified in Annex A.

Note 3 to entry: For convenience, in this document, the term “*p-q* curve” is used.

### 3.3.3

#### point of operation

point on the *AMD aerodynamic performance curve* (3.3.2) corresponding to a particular volume flow rate

Note 1 to entry: The point of operation is controlled during a test by adjusting the “slider” on the test plenum exit port assembly.

### 3.3.4

#### overall static efficiency

$\eta_{o,s}$

<for air-moving device of interest>volume flow rate multiplied by the fan static pressure and divided by the input electrical power

Note 1 to entry: The overall static efficiency,  $\eta_{o,s}$ , expressed as a percentage, is given by

$$\eta_{o,s} = \frac{p_{s,f} q_V}{P_{\text{input}}} \times 100$$

where

$p_{s,f}$  is the fan static pressure, in pascals;

$q_V$  is the volume flow rate, in cubic metres per second;

$P_{\text{input}}$  is the motor input power, in watts (true power, not including reactive component), supplied at the terminals of the electric drive motor.

Note 2 to entry: The air-moving device is defined to include the motor, impeller and frame; therefore, the overall static efficiency includes both the electromechanical efficiency of the motor and the aerodynamic efficiency of the impeller and frame.

### 3.3.5

#### standard air density

density under *standard air conditions* (3.3.6)

Note 1 to entry: The value is 1,20 kg/m<sup>3</sup>.

### 3.3.6

#### standard air conditions

<for aerodynamic performance measurement> specified meteorological conditions

Note 1 to entry: For the purposes of this document, the conditions are: 20 °C temperature; 50 % relative humidity; and 1,013 × 10<sup>5</sup> Pa ambient pressure.

## 4 Limitations of measurement

This method is useful up to the maximum volume flow rate,  $q_{V,\text{max}}$ , as a function of nominal air volume,  $V$ , of the plenum used and up to a fan static pressure of 750 Pa.

Based on experimental data and modelled results, the allowable fan static pressure range is extended up to at least 750 Pa for a full-size plenum, 1 500 Pa for a half-size plenum and 3 000 Pa for a quarter-size plenum.

NOTE 1 For static pressures above 750 Pa, the integrity of the plenum and the measurement can be impacted by the thickness of the polyester film, the size of the plenum, and the construction of the mounting plate and the outlet port. A thinner polyester film and a larger plenum size will result in increased strain on the polyester film. If a fan is operating at a static pressure above 750 Pa, closely monitor for leaks, particularly around the mounting panel and outlet port. See References [14] and [15] for details.

$$q_{V,\text{max}} = \frac{q_{V,0}}{V_0} V \quad (1)$$

where

- $q_{V,max}$  is the maximum volume flow rate of the scaled plenum, in cubic metres per second;
- $q_{V,0}$  is the maximum volume flow rate of the full-size plenum, in cubic metres per second,  $q_{V,0} = 1 \text{ m}^3 / \text{s}$ ;
- $V_0$  is the nominal air volume of the full-size plenum defined in [Clause 6](#), in cubic metres,  $V_0 = 1,3 \text{ m}^3$ ;
- $V$  is the nominal air volume of the scaled plenum, in cubic metres.

NOTE 2 The value of the interior air volume of a full-size plenum of  $1,3 \text{ m}^3$  is rounded up from  $1,296 \text{ m}^3 = 1,2 \text{ m}$  (width)  $\times 1,2 \text{ m}$  (depth)  $\times 0,9 \text{ m}$  (height).

NOTE 3 It is noted that the “nominal air volume” means approximate air volume calculated from the outer dimensions of the plenum. For instance, in case of 1/4 sized plenum, the nominal air volume of the plenum, excluding the leg height, becomes  $V = b \cdot l \cdot h = 0,3 \text{ m} \times 0,3 \text{ m} \times 0,225 \text{ m} = 0,020 25 \text{ m}^3$ , where  $b$  is width,  $l$  is depth, and  $h$  is height.

For the purposes of this document, it is recommended that the smallest plenum possible be applied, provided that the maximum volume flow rate of the fan is within the limit of [Formula \(1\)](#).

The method defined in this document, by reference to ISO 7779, provided for determination of sound power levels in a qualified environment, shall use either a comparison method in a reverberation test room based on ISO 3741, or a direct method in essentially free-field conditions over a reflecting plane based on ISO 3744 or ISO 3745. The method specified in this document can be applied to air-moving devices (AMDs) which radiate: a) broad-band noise; b) narrow-band noise; or c) noise that contains discrete frequency components.

The method specified in this document permits the determination of acoustical noise emission levels for an individual unit under test. If these levels are determined for several units of the same production series, the results may be used to determine a statistical value for the production series.

**CAUTION — Vibration, flow disturbances, insertion loss and other phenomena can alter radiated sound power in the actual application; therefore, the results of measurements made in accordance with this document can differ from the results obtained when AMDs are installed in equipment.**

NOTE 4 This document does not describe measurement of the structure-borne noise generated by AMDs.

## 5 Design and performance requirements for test plenum

### 5.1 General

The design specified is intended to meet the limits stated for maximum volume flow rate and maximum fan static pressure. The design provides an acoustically transparent, adjustable flow resistance to the AMD.

NOTE 1 See [5.5](#) for requirements for confirming acoustical transparency in accordance with this document.

The reference design of the plenum is specified in [5.2](#) to [5.6](#) and shown in [Figure 1](#) to [Figure 8](#). Also addressed in these subclauses and elsewhere in this document are permitted variations from this design, primarily the option of reducing the linear dimensions of the frame and some dimensions of other parts, while maintaining geometric proportions, in the range from full to quarter scale. Such a reduction reduces the maximum permitted volume flow rate of AMDs to be tested in direct proportion to the reduction in volume of the plenum [see [Formula \(1\)](#)], i.e. by the linear scale raised to the third power.

NOTE 2 These variations can better accommodate the use of smaller or quieter fans as well as test chambers with doors too narrow for the reference design plenum.

Permitted variations have been shown to yield standard deviations of reproducibility within the range of [Table 1](#). The degree to which other deviations from the reference design affect the uncertainty of the determination of sound power levels of AMDs is not known.

## 5.2 Test plenum: main assembly

The test plenum shall consist of an airtight chamber constructed with a frame covered with an airtight acoustically transparent polyester film, a mounting panel, and an adjustable exit port assembly as shown in [Figure 1](#). The plenum shall conform to the requirements specified in [5.2.1](#) to [5.2.6](#).

**5.2.1 Plenum size:** [Figure 1](#) shows the dimensions of the full-size plenum.

**5.2.2 Covering:** Isotropic polyester film of nominal thickness 25 µm to 50 µm. Batten strips may be used to protect the covering (see [Figure 1](#) and [Figure 2](#)).

**5.2.3 Frame:** Suitable material with nominal size of 50 mm × 50 mm that provides structural integrity for the plenum. Corner gussets are recommended for wood framing and may be needed for other materials (see [Figure 3](#)). Frame linear dimensions including the thickness of the framing members shall be in scale with the plenum size.

**5.2.4 Frame material:** Experience has shown that either a hardwood, such as birch, or aluminium tubing provides sufficient strength, stiffness and durability and complies with the acoustical performance requirements outlined in [5.5](#).

**5.2.5 Vibration isolation:** The test plenum feet or support should provide vibration isolation of the plenum from the floor, for any size of plenum. The intent is to break the vibration-transmission path between the plenum and the floor. Whichever method is chosen, the 0,1 m overall leg height should be maintained for the full-size plenum (see [Figure 1](#) and [Figure 3](#)). The 0,1 m leg height shall be in scale with the plenum size.

**5.2.6 Taps for fan static pressure:** The pressure ring shall be mounted immediately behind the mounting panel. The ring should be sized to match the perimeter of the mounting panel (see [Figure 4](#)). The perimeter dimensions of the pressure ring shall be in scale with the plenum size. The tubing diameter and taps do not scale but remain constant.

## 5.3 Mounting panel assembly

The mounting panel assembly shall comprise some kind of adapter plate sealed and attached to a reinforced rubber sheet which, in turn, is sealed and attached to the test plenum frame through the use of aluminium retaining strips (see [Figure 1](#), [Figure 4](#), and [Figure 5](#)). The adapter plate is used to mount the fan securely to the rubber panel. It may take the form of that shown in [Figure 5](#), which is well suited to axial-flow fans, or some other form more suitable to the particular air-moving device under test. The adapter plate should not cause any disturbance to the air flow and should not cause any additional sound radiation other than that from the air-moving device itself.

The mounting panel assembly (comprising adapter plate and flexible panel) may be replaced by a single damped plate with comparable cut-outs (but no adapter plate) of specified material without significantly affecting the airborne sound measurements.

The specification on the plate stock is mobility level (reference: 1 m/N·s) of -45 dB from 25 Hz to 5 000 Hz when measured in the middle of a plate of dimension 1,0 m<sup>2</sup> with no fan-mounting hole and with the plate freely suspended by two corners. The mobility level measurement shall be made in accordance with ANSI/ASA S2.32.

The tolerance on mobility levels is ±8 dB from 25 Hz to 100 Hz, ±4 dB from 100 Hz to 200 Hz and ±2 dB from 200 Hz to 5 000 Hz. These tolerance limits ensure that the plate has sufficient damping to prevent excitation of the frame. Such replacement panels are sometimes used in connection with fan vibration measurements (which are addressed in ISO 10302-2<sup>[6]</sup>). Using the same mounting panel for sound and vibration measurements may improve the efficiency of combined tests. If the reference design mounting panel is replaced, on the basis of impedance testing of the plate material, this shall be stated in the test report.

The opening of the adapter plate shall conform to the recommendations of the AMD manufacturer. The openings in the clamp frame and rubber panel shall be larger than the opening in the adapter plate to minimize disturbance of the airflow. The length, width, and thickness of the aluminium retainer strip as well as the length and width of the reinforced rubber mounting panel shall be in scale with the plenum size. The other dimensions, including the panel thickness, do not scale.

#### 5.4 Adjustable exit port assembly

The adjustable exit port assembly shall comprise a fixed aperture plate and a slider (movable sliding plate) to provide a continuously variable exit port of area from 0,0 m<sup>2</sup> to 0,2 m<sup>2</sup> for the full-size plenum (see [Figure 6](#) to [Figure 8](#)). The exit port maximum area shall be in scale with the square of the linear scale of the plenum.

NOTE The point of operation of the AMD is controlled during a test by adjusting the position of the slider on the exit port assembly.

#### 5.5 Insertion loss of test plenum

For the purpose of this document, adequacy of the test plenum is evaluated by means of insertion loss of the test plenum (see [3.2.3](#)).

Within the frequency range of interest (see [3.2.2](#)), the one-third-octave-band insertion loss of the test plenum shall be not greater than  $(0_{-2}^{+3})$  dB and is recommended to be not greater than  $(0 \pm 1,5)$  dB, when determined in accordance with the procedure specified in steps a) to c).

- a) The sound power levels of a sound source (e.g. a loudspeaker) shall be determined twice: once with the source inside the test plenum and once with the source outside the plenum, but at the same location in the test room. If insertion loss measurements are made in a free field over a reflecting plane, the hemispherical microphone array should be centred on the sound power source.
- b) Measurement uncertainties can arise if the loudspeaker sound power source is moved relative to reflective surfaces (floor and mounting panel) between the two sound power determinations. Accordingly, install the sound power source on the floor. Remove the mounting panel and rotate the plenum by 90° so that the face normally covered by the mounting panel is parallel to the floor and the exit port is on the top surface. The plenum can then be lowered or raised vertically to cover or expose the sound power source without causing movement of the source.
- c) The source shall be mounted to ensure that solid body radiation from the sound power source which is transmitted into the test plenum frame or covering is minimized.

The exit port slider shall be closed during the insertion loss test.

#### 5.6 Instrumentation for static pressure measurement

The fan static pressure developed inside the test plenum by the AMD shall be measured using a pressure ring (shown in [Figure 4](#)). This pressure ring has four taps spaced 90° apart as shown, facing towards the centre of the discharge of the AMD (in the plane of the ring). The pressure ring should be mounted on the frame that supports the mounting panel. A pressure line can be brought out of the box by drilling a small, smooth, burr-free hole through the frame. The fan static pressure should be read on a calibrated pressure meter.

The manometer or other pressure measuring device used shall have a resolution of 1 % or finer (e.g. 0,5 %) of maximum fan static pressure.

## 6 Installation

### 6.1 Installation of test plenum in test room

The test plenum shall be installed on the floor of a test room, which has been qualified for sound power level determinations in accordance with ISO 7779:2018, Clause 6 or Clause 7, respectively.

### 6.2 Direction of airflow

The AMD should preferably be tested when discharging into the test plenum. Exceptions to this airflow direction can be made to avoid undesirable flow conditions. For example, centrifugal fans or motorized impellers without scrolls can be tested with the plenum on the inlet.

### 6.3 Mounting of air-moving device

The AMD shall be mounted on and sealed to the mounting panel assembly specified in 5.3 (either the rubber sheet with adapter plate and clamp frame or the single damped panel). Additional vibration-isolated supports, which shall not interfere with the propagation of airborne sound, shall be provided as necessary to maintain the mounting plane parallel with the face of the test plenum; in particular, such supports can be required when testing centrifugal fans, especially at low static pressures. In all cases, the mounting panel assembly shall remain plane with the face of the plenum. For large AMDs, auxiliary support can be required to prevent the weight of the device from bending or twisting the mounting panel. Such auxiliary support shall not interfere with the propagation of airborne sound and shall be vibration-isolated from the air-moving device.

The AMD should be tested for each of its configurations (see Note 2 to 3.1.1).

In some cases, AMDs operating under conditions which keep the plenum exit port completely open can cause the polyester film panels to flutter or vibrate, creating unwanted noise. In such cases, steps should be taken to minimize noise due to fluttering or vibration. For example, the mounting panel assembly with the AMD can be detached from the rest of the plenum and the latter moved out of the way. The mounting panel assembly should be maintained planar and suspended above the floor of the test room at the same location as specified in 6.1.

## 7 Operation of air-moving device

### 7.1 Input power

#### 7.1.1 Alternating current (AC) air-moving devices

The AMD shall be operated at each rated power line frequency, and within  $\pm 1,0$  % of either:

- a) the rated voltage (if any is stated); or
- b) the mean voltage of a stated voltage range (e.g. 220 V for a stated range of 210 V to 230 V).

For power having more than two phases, phase-to-phase voltage variations shall not exceed 1 % of the rated voltage.

NOTE Though the test procedure of Clause 7 is similar to those of ISO 7779, the tolerance of voltage given here is much tighter than that in ISO 7779 (i.e., 5 % of the rated voltage).

#### 7.1.2 Direct current (DC) air-moving devices

The AMD shall be operated within  $\pm 1$  % of the rated nominal voltage.

Additional tests may be run at other voltages (e.g. rated maximum, rated minimum).

## 7.2 Points of operation (AC and DC air-moving devices)

### 7.2.1 Required points of operation

For the selection of points of operation, there are the following 2 methods.

Method A of [7.2.2](#) is, so called conventional method, which defines points of operation as a function of the maximum flow rate of the AMD of interest.

Method B of [7.2.3](#) is alternative method, which defines points of operation as a point at the intersection of the  $p$ - $q$  curve of the AMD and the system impedance curve.

In conformity to this document, the requirements of at least, either [7.2.2](#) and/or [7.2.3](#) are to be fully satisfied.

### 7.2.2 Method A (conventional method)

#### 7.2.2.1 Required points of operation

The AMD shall be tested at three points of operation for each of the required line frequencies and voltages given in [7.1](#). These points of operation correspond to

- a) the adjustable exit port (slider) completely open,
- b) 80 % of maximum volume flow rate on the  $p$ - $q$  curve, and
- c) 20 % of maximum volume flow rate on the  $p$ - $q$  curve.

The actual static pressure reading at each point of operation shall be recorded.

NOTE 1 In this document,  $p$ - $q$  curve measurement is a prerequisite for acoustical noise measurement. So the “maximum volume flow rate” means the point on the  $p$ - $q$  curve (see [3.3.2](#)), which corresponds to the condition of static pressure equal to 0. For instance, when the maximum volume flow rate of a fan under test is read as 0,01 m<sup>3</sup>/s from the  $p$ - $q$  curve, 80 % of maximum volume flow rate means 0,01 m<sup>3</sup>/s × 0,8 = 0,008 m<sup>3</sup>/s.

NOTE 2 Within the framework of this document, a clear distinction is made between “slider completely open” and “maximum flow rate”. In the previous edition and other conventional standards this was not the case. Condition a) above, “slider completely open”, was referred to as the “maximum flow rate” or “free delivery” condition. However, air-flow resistance by the plenum influences the actual point of operation. For example, the three smooth lines near the abscissa in [Figure 9](#) indicate the system impedance curves of the quarter-scale, half-scale and full-scale plenum respectively, with slider completely open.

#### 7.2.2.2 Additional points of operation

Additional tests may be run at other points of operation, including the point of maximum overall static efficiency, to establish the sound power level versus volume flow rate curve. Some AMDs (e.g. small tubular fans) can be unstable when operated near the maximum overall static efficiency point. Tests should not be conducted at unstable points of operation.

### 7.2.3 Method B (alternative method)

#### 7.2.3.1 Required points of operation

The AMD shall be tested at point of operation at the intersection of the  $p$ - $q$  curve of the AMD and the system impedance curve<sup>2)</sup> of the candidate system (i.e. a functional unit which is expected to install the AMD), for each of the required line frequencies and voltages given in [7.1](#). These test points correspond to the actual points of operation of the candidate system.

2) System impedance curve can be referred to system resistance curve.

### 7.2.3.2 Additional points of operation

Optionally, the points of operations specified in [7.2.2.1](#) can be added.

### 7.2.4 Procedure

Points of operation shall be established as in steps a) to c).

- a) The fan static pressure at the designated percentage volume flow rates shall be read from the AMD aerodynamic performance curve ( $p$ - $q$  curve) determined (prior to acoustical noise measurement) in accordance with ISO 5801 or [Annex A](#), as applicable, with the same direction of airflow.
- b) If the ambient atmospheric density during the noise test differs by more than 1 % from that recorded in accordance with ISO 5801 or [Annex A](#), as applicable, the fan static pressure shall be corrected as follows:

$$p_{s,2} = p_{s,1} \left( \frac{273 + t_1}{273 + t_2} \right) \frac{p_{amb,2}}{p_{amb,1}} \quad (5)$$

where

- $p_{s,2}$  is the fan static pressure to be set on the test plenum during acoustical noise measurement, in pascals;
  - $t_2$  is the air-flow temperature during acoustical noise measurement, in degrees Celsius;
  - $p_{amb,2}$  is the atmospheric pressure during acoustical noise measurement, in kilopascals;
  - $p_{s,1}$  is the fan static pressure during volume flow rate measurement, in pascals;
  - $t_1$  is the air-flow temperature during volume flow rate measurement, in degree Celsius;
  - $p_{amb,1}$  is the atmospheric pressure during volume flow rate measurement, in kilopascals.
- c) The slider shall be adjusted to obtain a reading of the fan static pressure,  $p_{s,2}$ , within  $\pm 1$  % of the maximum fan static pressure, determined with a pressure-measuring instrument satisfying the requirements of [5.6](#).

The fan and the fan static pressure shall be allowed to stabilize at each point of operation.

If measurements are made at the maximum overall static efficiency point, care should be taken when adjusting the plenum for this point of operation. Some AMDs have three or more values of volume flow rate corresponding to the same fan static pressure in the region of maximum overall static efficiency. Only the point with the highest volume flow rate is the maximum overall static efficiency point. To obtain this point of operation, start from free delivery and increase the static pressure until the point of operation is reached.

If an AMD is unstable (e.g. unsteady speed or pressure) at one of the recommended points of operation, decrease the fan static pressure until stability is achieved and use the new point of operation thus reached. The instability shall be reported and the alternative point of operation shall be described.

NOTE The AMD aerodynamic performance curve obtained according to ISO 5801 or [Annex A](#) can differ from the performance on the test plenum. This difference is assumed to be equivalent to that typical of normal AMD applications, and no corrections for test plenum differences are necessary.

## 8 Measurement procedures

### 8.1 General

Sound power levels shall be determined in accordance with ISO 7779. ISO 7779:2018, Clause 6 permits the use of a comparison method in a reverberation test room, based on ISO 3741. ISO 7779:2018, Clause 7

permits sound power determination in an essentially free field over a reflecting plane based on ISO 3744 and ISO 3745. If a method specified in ISO 7779:2018, Clause 7 is used, one of the sets of microphone positions described in [8.2](#) is required.

NOTE When using the method of ISO 7779:2018, Clause 7, sound power levels can be influenced by air density. This document follows ISO 7779:2018 for the corrections. For some cases requiring consideration of the influence of air density, [Annex B](#) gives supplementary information.

## 8.2 Microphone positions for measurements in an essentially free field over a reflecting plane

### 8.2.1 General

For the purposes of this document, the measurement surfaces for determining sound power level shall be hemispherical, selected from those specified in ISO 3744 and ISO 3745. The radius shall not be smaller than 0,5 m (see Note 2 to [3.2.2](#)).

NOTE 1 In ISO 7779, measurement surfaces in forms other than hemispherical are specified for an essentially free field over a reflecting plane. However, for the purpose of sound power level determination using the test plenum mounted in such an acoustical environment, this document permits only hemispherical measurement surfaces.

One of the sets of microphone positions in either [8.2.2](#) or [8.2.3](#) should be used, but the radius shall not be smaller than 0,5 m (see Note 2 to [3.2.2](#)). In any case, the origin of the co-ordinates is located at the vertical projection of the centre of the mounting opening on the reflecting plane. If a test plenum geometrically smaller than that in [Figure 1](#) is used, a radius of between 2 m and the geometrically scaled radius shall be used.

NOTE 2 These sets of microphone positions reduce interference effects caused by reflections from the plane and can avoid intake or exhaust air streams.

### 8.2.2 Fixed points on a hemisphere

The locations of 10 positions associated with equal areas on the surface of the hemisphere are numbered from 1 to 10 in [Figure 10](#). The coordinates  $(x, y, z)$  are given in [Table 2](#) and [Figure 10](#).

NOTE For convenience, [Table 2](#) and [Figure 10](#) show co-ordinates of fixed positions on the hemispherical measurement surface.

### 8.2.3 Coaxial circular paths in five or more parallel planes

Instead of fixed positions, circular paths consisting of coaxial circular paths according to ISO 3744 shall be used. See [Figure 11](#), so that the annular areas of the hemisphere associated with each are equal.

## 8.3 Preparations for measurements

Steps a) to g) shall be taken in preparation for noise emission measurements on each AMD.

- a) Record the name, model number, serial number, dimensions, nameplate data and complete description of the AMD under test.
- b) Obtain the AMD aerodynamic performance curve in accordance with ISO 5801 or [Annex A](#), as applicable.
- c) Check the calibration of the microphone(s) in conformity with ISO 7779.
- d) Measure the background noise levels in the test room in conformity with ISO 7779.
- e) Measure the ambient temperature, relative humidity, and ambient pressure.
- f) If a method requiring the use of a reference sound source (RSS) is to be used, measure the sound pressure levels produced by the RSS.

- g) Zero the manometer or other pressure-measuring device used for measuring the fan static pressure in the test plenum.

#### 8.4 Operational test of air-moving device

Steps a) to h) shall be taken in carrying out the noise emission measurements on each AMD configuration.

- a) Allow the AMD under test to warm up for a sufficient period of time before proceeding with the acoustical test to allow the temperature to stabilize. If this time is unknown, the equipment shall be operated for at least 30 min before the acoustical test.
- b) Mount the AMD on the test plenum in accordance with [6.3](#).
- c) Adjust the voltage (and frequency when AC powered) in accordance with [7.1](#).
- d) Adjust the slider to obtain the desired point of operation in accordance with [7.2](#).
- e) Determine the sound power level in conformity with ISO 7779:2018, Clause 6 or Clause 7, as applicable. A-weighted sound power levels and one-third-octave-band sound power levels are required; octave-band sound power levels are optional.
- f) Record the data in conformity with [Clause 10](#).
- g) Repeat steps d) to f) for each point of operation.
- h) Repeat steps c) to g) for each voltage as required.

In some tests of small centrifugal fans on a full-scale plenum, discrete tones not normally present in the spectrum of the fan appeared; these apparently coincided with plenum resonance frequencies. This phenomenon has not been widely noted, but if unexpected tones appear during testing, the possible cause should be explored.

#### 9 Measurement uncertainty

The uncertainty of results obtained from measurements in accordance with this document shall be evaluated, preferably in accordance with ISO/IEC Guide 98-3. If reported, the expanded uncertainty together with the corresponding coverage probability as defined in ISO/IEC Guide 98-3 shall be given. Guidance on the determination of the expanded uncertainty is given in [Annex E](#).

If, in a laboratory performing measurements in accordance with this document, current knowledge is still insufficient to fully apply ISO/IEC Guide 98-3, the values given in [Table 1](#) are recommended for provisional use in test reports.

**Table 1 — Estimated values of the standard deviation of reproducibility of sound power levels of air-moving devices determined in accordance with ISO 10302-1**

Octave-band centre frequency Hz	One-third-octave-band centre frequency Hz	Standard deviation of reproducibility, $\sigma_{R0}$ dB
125	100 to 160	4,0
250	200 to 315	2,5
500 to 4 000	400 to 6 300	1,5
8 000	8 000	2,5
	10 000	3,0
A-weighted		1,5

NOTE 1 For the plenum between full and half size, these estimates are based on interlaboratory comparisons (Reference [12]) on tube-axial and forward-curved centrifugal fans in the range of volume flow rate from 0,016 m<sup>3</sup>/s to 0,456 m<sup>3</sup>/s, conducted in 14 laboratories (including both reverberation and hemi-anechoic chambers) following the guidelines provided by ISO 5725:1986<sup>3)</sup>[3]. For a smaller plenum, down to one-quarter size, the measurement uncertainty is assumed to be similar for the purposes of this document.

NOTE 2 The standard deviation of reproducibility data given in Table 1 is assumed to reflect the cumulative effects of all sources of uncertainty in measurements in accordance with this document, excluding variations in the sound power level from specimen to specimen. It does not, however, cover any systematic bias, which might occur between sound power levels determined with different measurement methods.

NOTE 3 The standard deviation of repeatability for the same specimen and the same laboratory measurement conditions can be considered to be considerably smaller than the corresponding standard uncertainties on which the values in Table 1 are based.

## 10 Information to be recorded

The following information shall be recorded, when applicable, for all measurements made in accordance with the requirements of this document.

At each point of operation, record the following data and other information required by ISO 7779:

- a) actual input voltage, in volts;
- b) fan static pressure, in pascals, with data resolutions of at least  $\pm 1\%$  of measured value, or 2,5 Pa, whichever is the larger;
- c) slider location or exit port open area (optional);
- d) rotational frequency, rounded to the nearest 5 min<sup>-1</sup>;
- e) input electrical power, in watts, if required;
- f) line frequency, in hertz, when AC powered;
- g) A-weighted sound power level determined in conformity with ISO 7779:2018, Clause 6 or Clause 7, as applicable, and rounded to the nearest 0,1 dB (reference: 1 pW);
- h) one-third-octave-band sound power levels (reference: 1 pW) determined in conformity with ISO 7779:2018, Clause 6 or Clause 7, as applicable, and rounded to the nearest 0,1 dB;
- i) octave-band sound power levels (reference: 1 pW) determined in conformity with ISO 7779:2018, Clause 6 or Clause 7, as applicable, and rounded to the nearest 0,1 dB (optional).

## 11 Information to be reported

Data should be presented using forms similar to those given in Annex C. The report shall contain at least the following information:

- a) a statement that the AMD has been tested in conformity with this document and that sound power levels have been determined in conformity with ISO 7779 (the method used for determinations of sound power levels shall be stated);
- b) manufacturer, product name (if any), manufacturer's part number, serial number (if any), dimensions (length, width, depth, hub diameter, impeller diameter), all other nameplate data, and a complete description of the AMD under test;
- c) the AMD aerodynamic performance curve, or the reference points of operation used;

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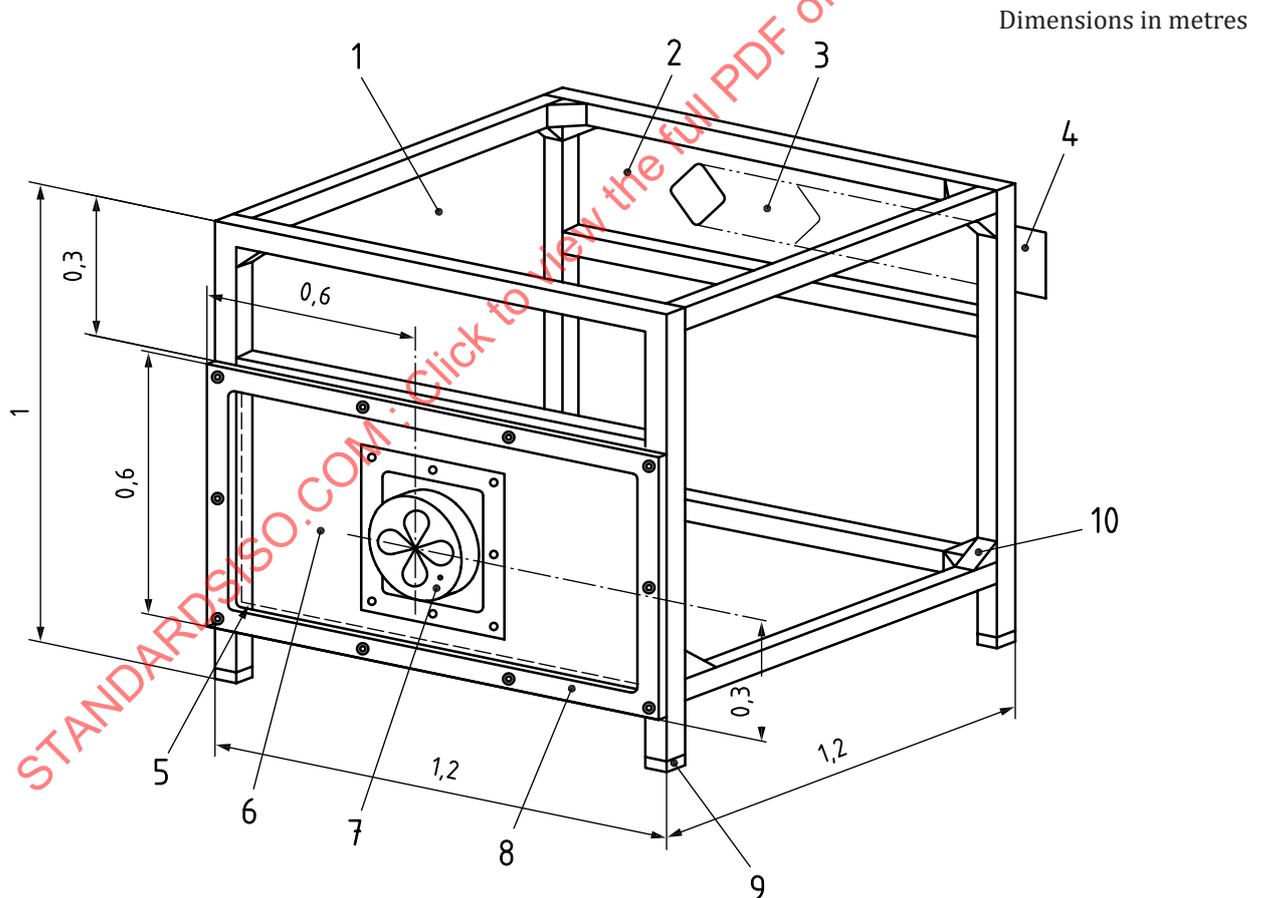
3) ISO 5725:1986 was withdrawn and replaced by ISO 5725-1 to ISO 5725-6.

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- d) A-weighted sound power level,  $L_{WA}$  (reference: 1 pW), in decibels, rounded to the nearest 1 dB for each point of operation, corresponding to each voltage “– if there is possibility of post data processing for calculation of statistical upper limit, A-weighted sound power level data of each sample shall have a resolution of 0,1 dB or finer);

NOTE For the purpose of declaring statistical values of sound power levels of AMDs, the A-weighted sound power level can be stated either in decibels rounded to the nearest 1 dB, or in bels rounded to the nearest 0,1 B. If statistical values are used, this should be made explicit in the report. [Annex D](#) gives sample specification formats, only for a single AMD.

- e) the sound power levels,  $L_W$ , rounded to the nearest 1 dB (reference: 1 pW) in one-third-octave bands and, optionally, in octave bands, for each point of operation;
- f) detailed description of operating conditions of the AMD under test as recorded in accordance with [Clause 9](#) (voltage, frequency, fan static pressure, corresponding volume flow rate, input power, and rotational frequency);
- g) temperature in degrees Celsius, relative humidity as a percentage, ambient pressure in kilopascals, and any other information that can be pertinent to the particular AMD under test;
- h) the associated expanded measurement uncertainties of A-weighted sound power levels determined according to the procedure used shall be reported (see [Clause 9](#)), with results rounded to the nearest 0,1 dB – in addition, information can be given on the basis of [Annex E](#).

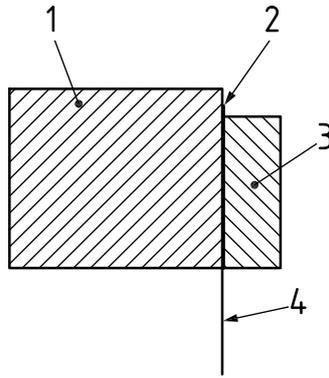


### Key

- 1 polyester film (covers all areas, including bottom, except mounting panel and exit port)
- 2 adjustable exit port assembly
- 3 slider opening
- 4 slider
- 5 piezometer pressure ring behind panel

- 6 mounting panel assembly
- 7 fan
- 8 retainer
- 9 vibration isolation
- 10 gusset

Figure 1 — Test plenum (full size)

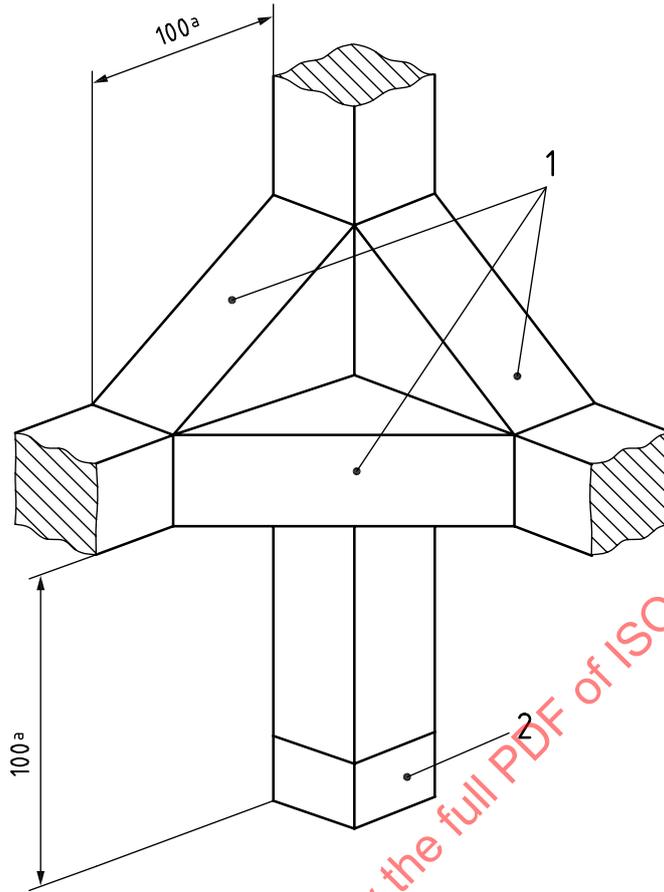


**Key**

- 1 frame
- 2 adhesive (holds polyester film)
- 3 external batten, screwed on (holds polyester film against adhesive)
- 4 polyester film

Figure 2 — Test plenum — Film attachment detail

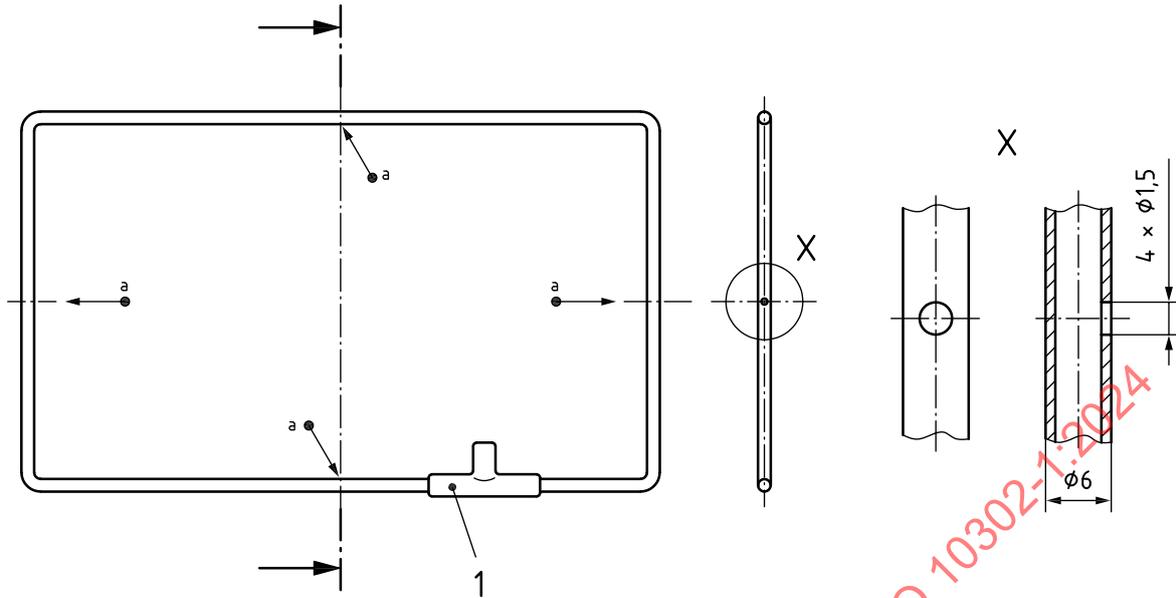
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**Key**

- 1 braces, all corners, screwed and glued
- 2 vibration isolator (on each leg)
- a Typical dimension.

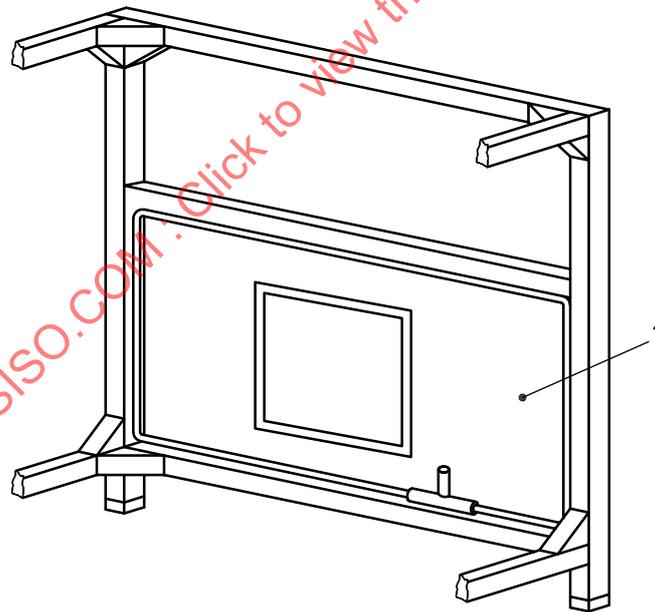
**Figure 3 — Test plenum — Gusset and vibration isolation**



**Key**

- 1 pressure line (as required)
- a Tap locations.

**a) Detail**

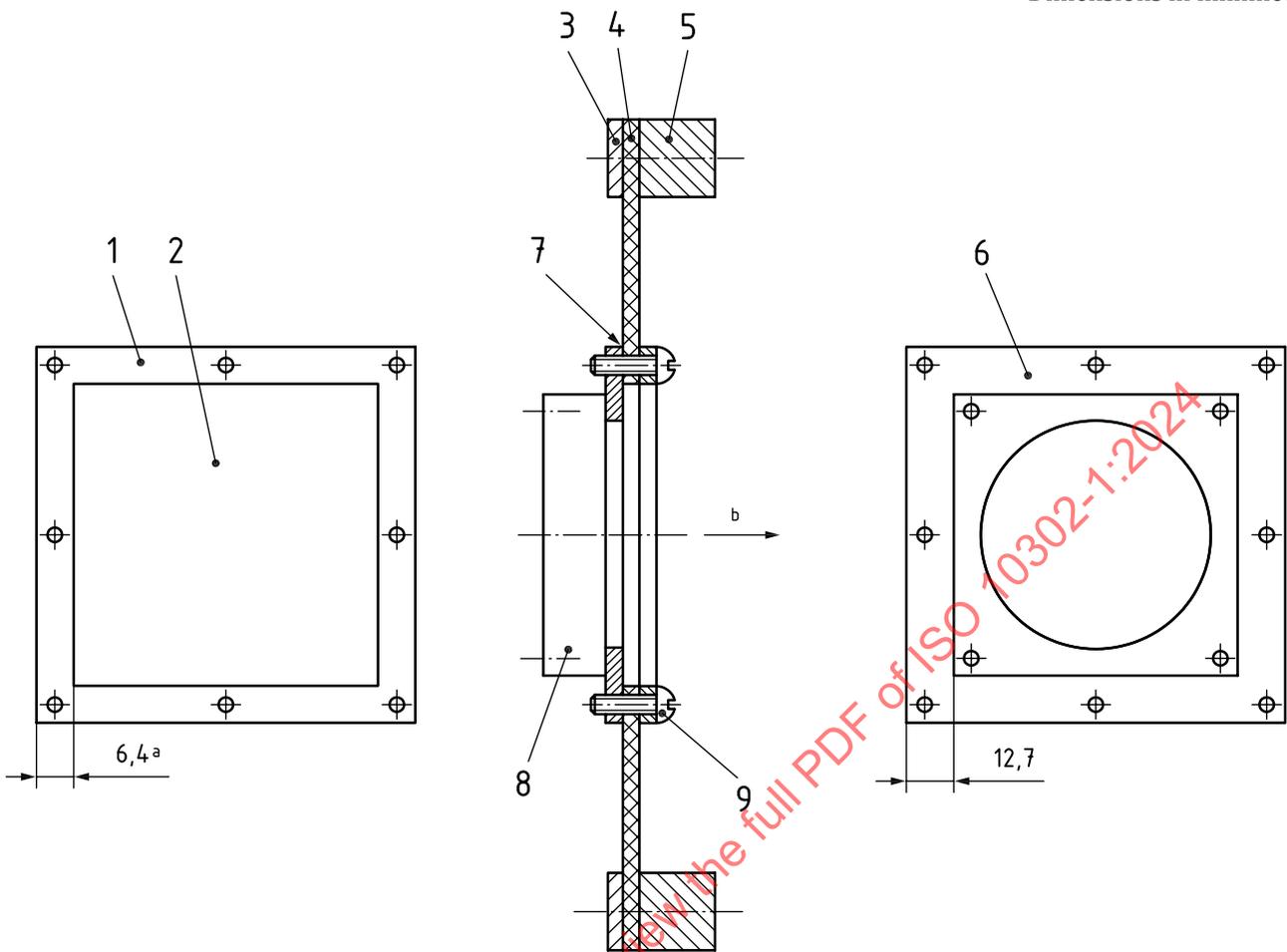


**Key**

- 1 rear side of mounting panel assembly

**b) Location**

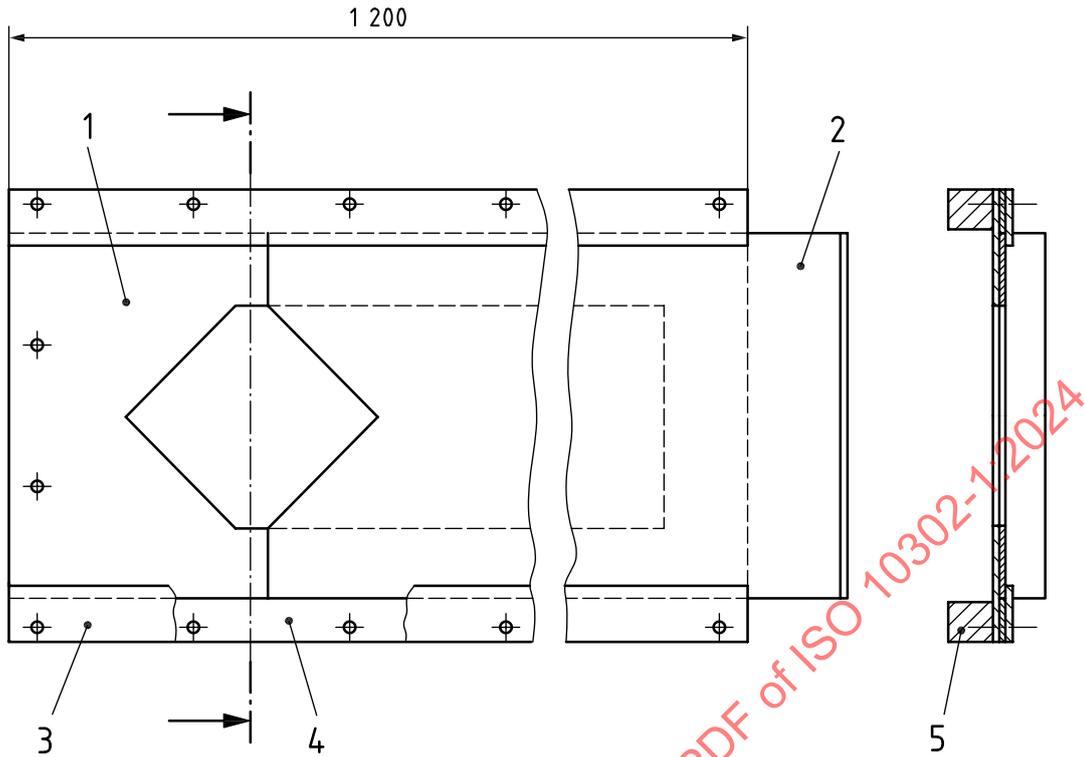
**Figure 4 — Test plenum — Pressure ring**



**Key**

- 1 clamp frame (3,2 mm thick aluminium)
- 2 cut-out
- 3 retainer aluminium strip with screw every 150 mm nom.
- 4 reinforced rubber panel, 5 kg/m<sup>2</sup> nom. loaded rubber
- 5 test plenum frame (ref.)
- 6 adapter plate (3,2 mm thick aluminium)
- 7 sealant
- 8 fan
- 9 screws or studs
- a Typical minimum.
- b Airflow.

**Figure 5 — Mounting panel assembly**

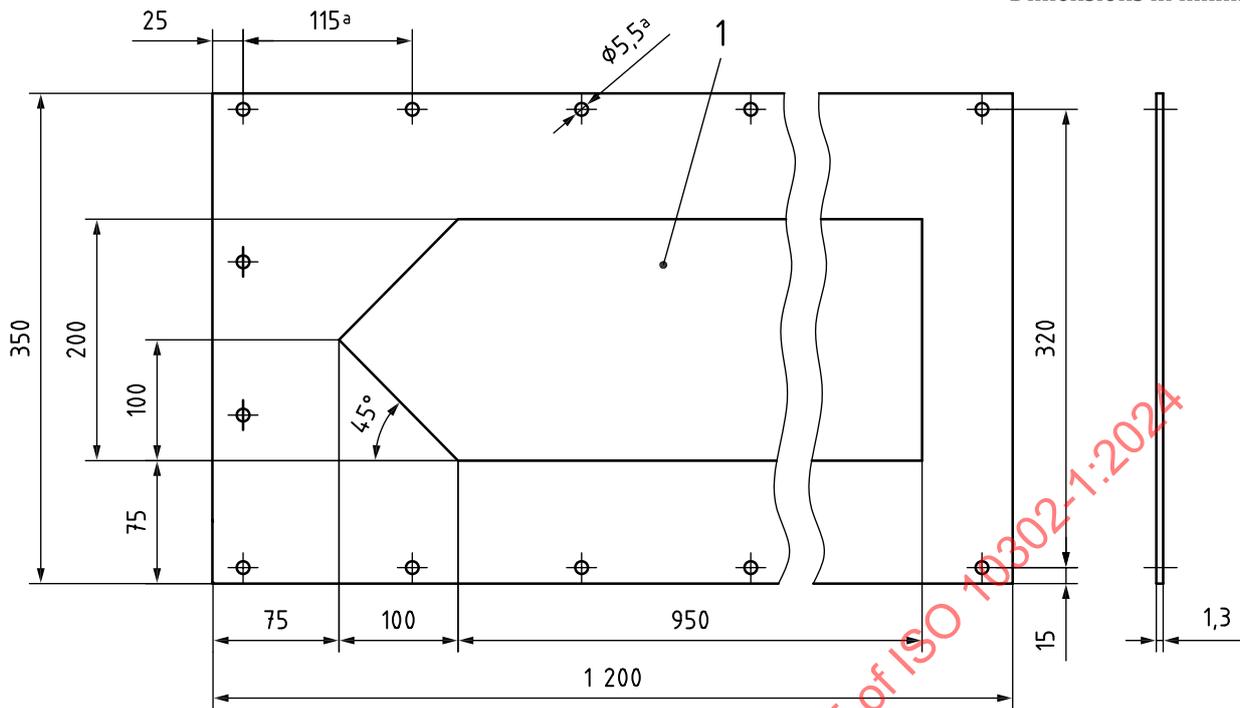


**Key**

- 1 aperture plate (see [Figure 7](#))
- 2 slider (see [Figure 8](#))
- 3 retainer (steel, 50 mm × 1,3 mm)
- 4 spacer and bearing (plastics, 30 mm × 1,6 mm)
- 5 frame (ref.)

**Figure 6 – Adjustable exit port assembly**

Dimensions in millimetres

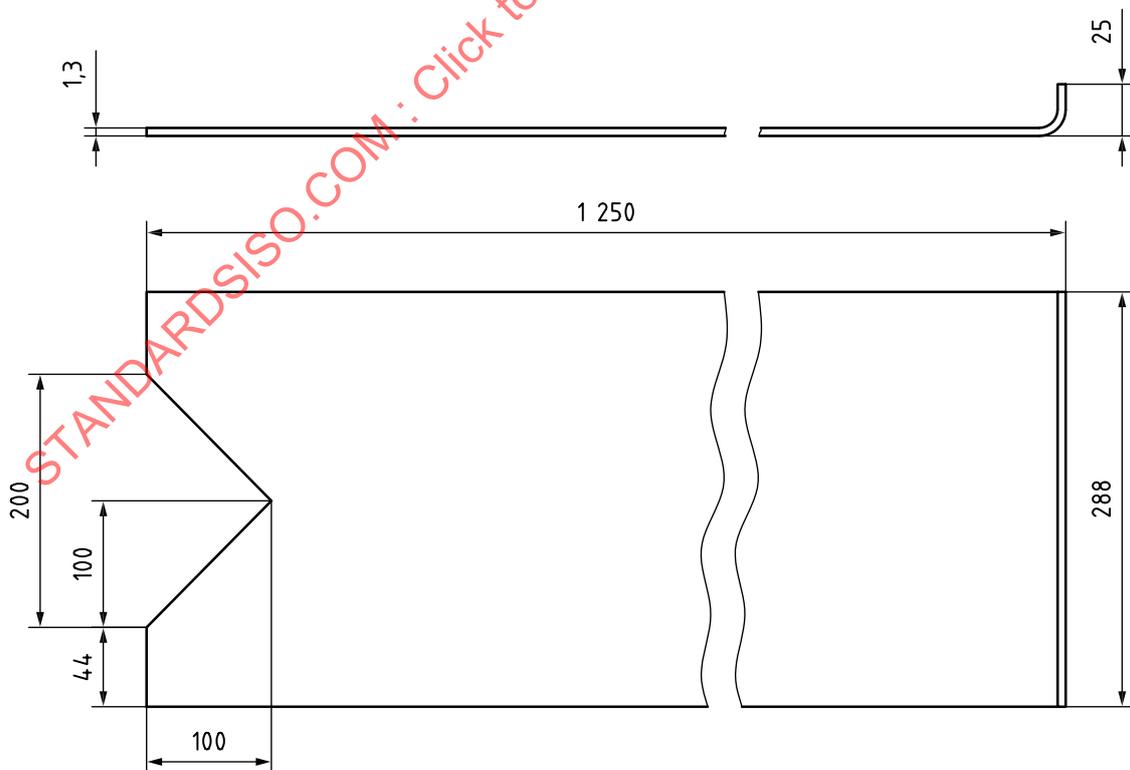


**Key**

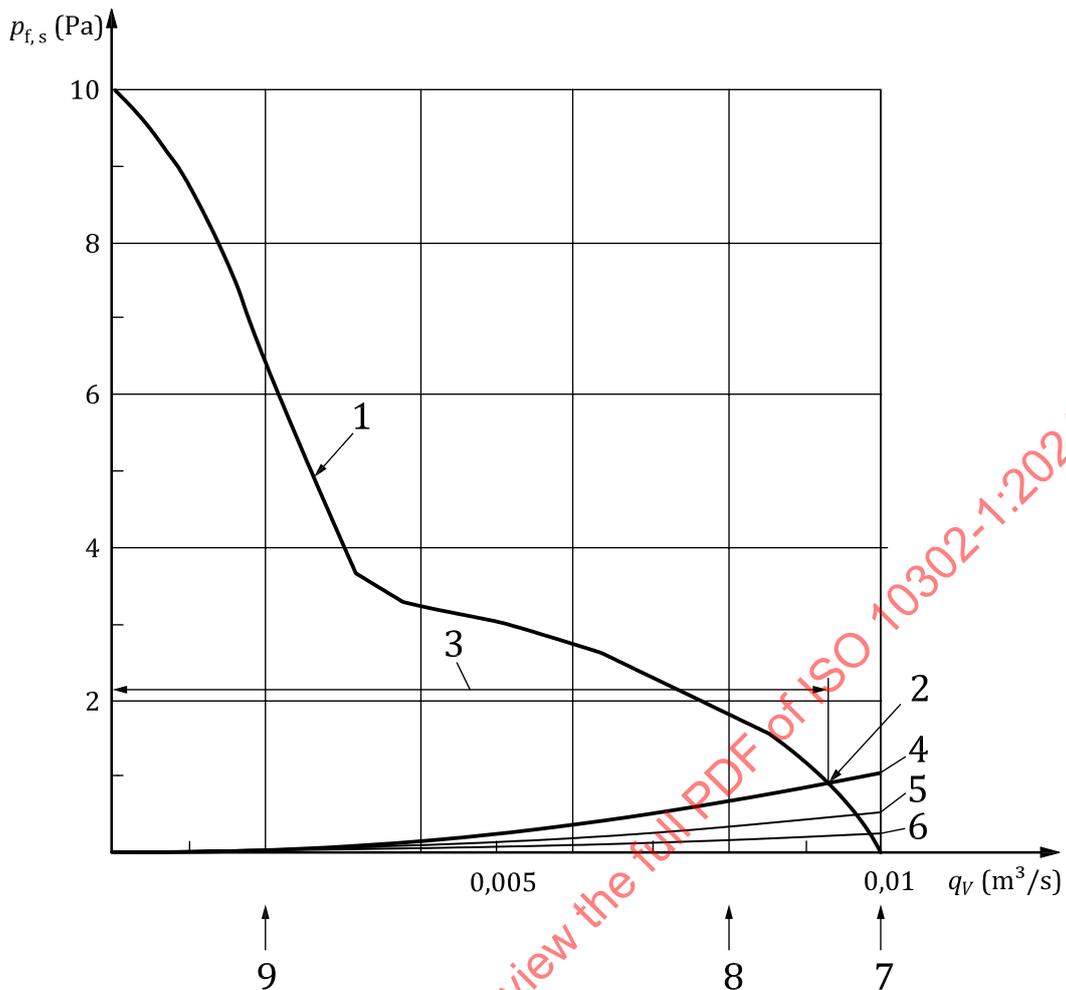
- 1 cut-out
- a Typical value.

**Figure 7 — Adjustable exit port assembly — Aperture plate (stainless steel)**

Dimensions in millimetres



**Figure 8 — Adjustable exit port assembly — Slider (stainless steel)**



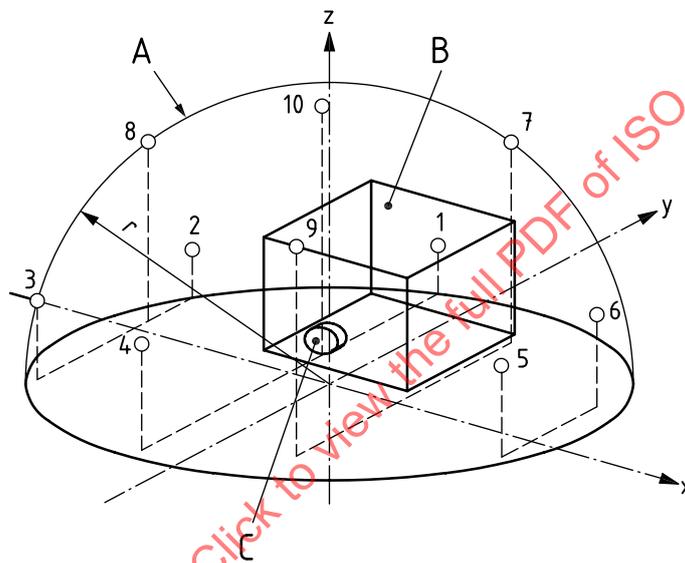
**Key**

- 1 example of  $p$ - $q$  curve with maximum volume flow rate =  $0,01 \text{ m}^3/\text{s}$ ; maximum static pressure =  $10 \text{ Pa}$
- 2 point of operation for quarter-size plenum, which is the cross-point of the  $p$ - $q$  curve and the system impedance curve of the plenum
- 3 adjustable region of volume flow rate by slider
- 4 system impedance curve of quarter-size plenum
- 5 system impedance curve of half-size plenum
- 6 system impedance curve of full-size plenum
- 7 point of operation a) (i.e., maximum volume flow rate)
- 8 point of operation b) (i.e., 80 % of maximum volume flow rate)
- 9 point of operation c) (i.e., 20 % of maximum volume flow rate)

**Figure 9 — Schematic correlation between  $p$ - $q$  curve versus system impedance curves (not to scale)**

Table 2 — Co-ordinates of hemispherical measurement surface for sources emitting discrete tones (10 measurement heights)

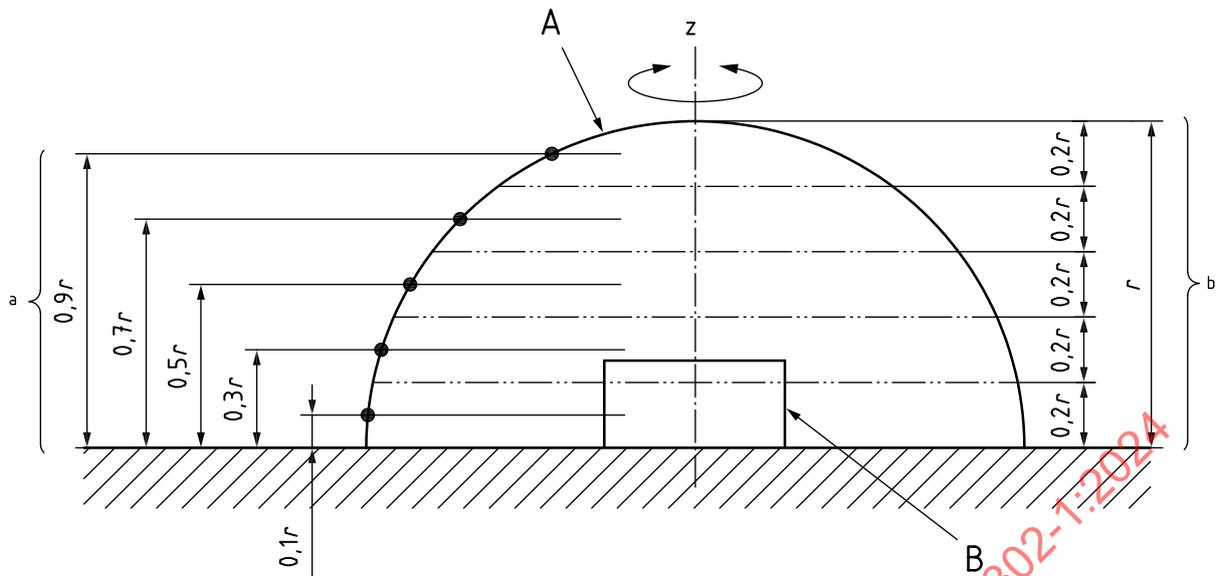
Measurement position No.	$x/r$	$y/r$	$z/r$
1	-0,16	0,96	0,22
2	-0,78	0,60	0,20
3	-0,78	-0,55	0,31
4	-0,16	-0,90	0,41
5	0,83	-0,32	0,45
6	0,83	0,40	0,38
7	0,26	0,65	0,71
8	-0,74	0,07	0,67
9	0,26	-0,50	0,83
10	-0,10	0,10	0,99



**Key**

- 1,2,3,4,5,6,7,8,9,10 microphone positions
- A measurement surface
- B plenum box
- C air-moving device mounting location
- $r$  radius of hemisphere

Figure 10 — Hemispherical surface — 10 measurement points



**Key**

- A measurement surface
- B reference box
- $r$  radius of hemisphere
- $z$  axis of rotation of microphone traversing mechanism
- $a$  Elevation of microphone traverses.
- $b$  Height of corresponding areas of hemisphere.

NOTE The paths are selected so that the annular area of the hemisphere associated with each path is the same.

**Figure 11 — Coaxial circular five or more paths in parallel planes for microphone traverses in an essentially free field over a reflecting plane**

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## Annex A (normative)

### Micro-fan $p$ - $q$ curve measurement method

#### A.1 Scope

In the main body of this document, the acquisition of the  $p$ - $q$  curve of the fan under test is a prerequisite for airborne noise emission measurement. For this purpose, the methods of ISO 5801 based on measurement by using the air chamber are cited.

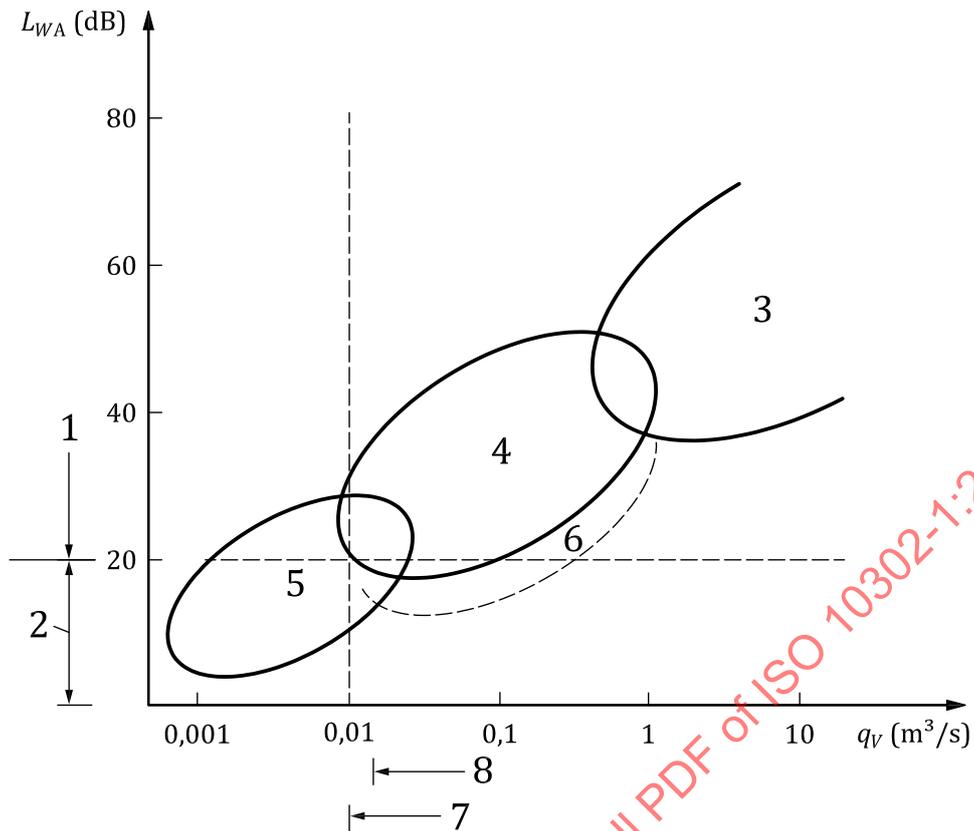
According to ISO 5801, the applicability of the methods is limited to the condition with a Reynolds number of approximately 12 000 or higher (see [3.1.2](#), Note 2 to entry). This lowest Reynolds number corresponds to the lower limit of volume flow rate of approximately 0,001 5 m<sup>3</sup>/s.

Actual fans are becoming smaller and smaller and are violating the Reynolds number assumption. Therefore, a complementary method to ISO 5801 is required for these fans. In this document, these fans are referred to as micro-fans (see [3.1.2](#)).

This annex specifies a new methodology for  $p$ - $q$  curve measurement of micro-fans, by reference to JBMS-72-1:2010, Annex A<sup>4)</sup>. Experimental data show that this method is useful to, at least, a maximum volume flow rate of 0,015 m<sup>3</sup>/s. See [Figure A.1](#).

---

4) Since there is no exact plan to update JBMS-72-1 anymore, ECMA plans to publish a Technical Report on “Method for measurement of airborne noise emitted by microfans in 2024”.



**Key**

- 1 lower limit of measurement by conventional method with 1 m radius (limit due to conventional microphone)
  - 2 range in which new measurement method is required
  - 3 approximate region intended for industrial fans
  - 4 approximate region intended for IT equipment fans
  - 5 approximate region of micro-fans
  - 6 approximate region of extremely low noise fans
  - 7 approximate lower limit of measurement by conventional method based on ISO 5801
  - 8 approximate upper limit of volume flow rate 0,015 m<sup>3</sup>/s, in accordance with JBMS-72-1:2010, Annex A
- $L_{WA}$  A-weighted sound power level, in decibels (reference: 1 pW)
- $q_V$  volume flow rate, in cubic metres per second

**Figure A.1 — Schematic correlation of applicability of this annex and corresponding noise emissions (not to scale)**

## Annex B (informative)

### Effects of air density

There are four principal effects of air density, a) to d), that require consideration in measurements of the sound power levels of aerodynamic sources such as fans.

- a) Changes in air density or ambient pressure produce changes in microphone sensitivity. Follow the manufacturer's instructions to ensure that the microphone is calibrated for ambient pressure.
- b) The sound power of the source,  $P$ , is determined from the value of the sound pressure using the expression in a free field:

$$P \propto \frac{p^2}{\rho c}$$

where

$p^2$  is the mean-squared value of the sound pressure in pascal squared;

$\rho$  is the density of air in kg per cubic metres;

$c$  is the speed of sound in metres per second.

If the free field over a reflecting plane method of ISO 7779 is used, then any correction for this effect should be made according to ISO 7779.

If the comparison reverberation test room method is used from ISO 7779, no explicit correction is necessary because the correction is inherently included in the comparison method. The use of the direct method of ISO 3741 is not permitted by this document.

- c) The sound power radiated by many aerodynamic sources, e.g. axial fans and centrifugal fans, is proportional to air density.
- d) If the atmospheric density differs significantly from standard air density (see [3.3.5](#)) so as to change the rotational frequency of the AMD appreciably, an error due to this change may be introduced. In such a case, other quantities (e.g. motor current, electrical input power and overall static efficiency) may also change from their values under standard air density. This document does not provide for correction of the data to rotational frequencies of the AMD other than those existing during the measurements.

**Annex C**  
(informative)

**Data formats for presentation**

**C.1 General**

This annex gives sample data formats for reporting of acoustical noise emission of AMDs according to this document. The contents are based on the requirements stated in [Clause 11](#), but the others (e.g. sequences of each item, horizontal line spacing of spectrum graphs, and number of pages) are arbitrary and completely informative in nature.

In case of conflict, [Clause 11](#) takes precedence over this annex.

**C.2 Example**

The following pages show one example.

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Air-moving device acoustical noise emission test report

Manufacturer:

Model: Part/serial number:

Nameplate data:

Manufacture date:

Description:

The data presented in this report have been determined in conformity with the requirements of ISO 10302-1.

Method of sound power determination: [Reverberation test room/Essentially free field over a reflecting plane]

Test voltage: [DC/AC] Test frequency (if AC powered)

Rating data				Measurement data	
Points of operation	Electrical power W	Reference volume flow rate m <sup>3</sup> /s	Reference fan static pressure Pa	Rotational frequency min <sup>-1</sup>	L <sub>WA</sub> (reference value 1 pW) dB
Adjustable exit port (slider) completely open					
80 % Of maximum volume flow rate					
20 % Of maximum volume flow rate					

Test environmental conditions:

Temperature: °C

Relative humidity: %

Air density: kg/m<sup>3</sup>

Ambient pressure: kPa

Prepared by:

Date:

Organization performing test:

Document number:

Air-moving device noise emission test report

NOTE [Table C.1](#) and [Table C.2](#) are alternative.

**Table C.1 — Data table according of Method A (conventional method) of [7.2.2](#)**

Rating data				Measurement data	
Points of operation	Electrical power W	Reference volume flow rate m <sup>3</sup> /s	Reference fan static pressure Pa	Rotational frequency min <sup>-1</sup>	$L_{WA}$ (reference value 1 pW) dB
Adjustable exit port (slider) completely open					
80 % of maximum volume flow rate					
20 % of maximum volume flow rate					
the point of maximum overall static efficiency (optional)					

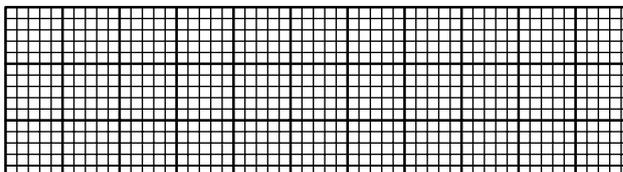
**Table C.2 — Data table according of Method B (alternative method) of [7.2.3](#)**

Rating data				Measurement data	
Points of operation	Electrical power W	Reference volume flow rate m <sup>3</sup> /s	Reference fan static pressure Pa	Rotational frequency min <sup>-1</sup>	$L_{WA}$ (reference value 1 pW) dB
At point of operation at the intersection of the <i>p-q</i> curve of the AMD and the system impedance curve of the candidate system					
The adjustable exit port (slider) completely open (optional)					
80 % of maximum volume flow rate (optional)					
20 % of maximum volume flow rate (optional)					

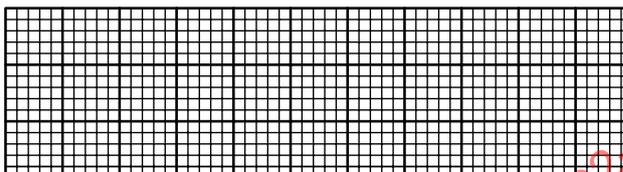
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Aerodynamic performance

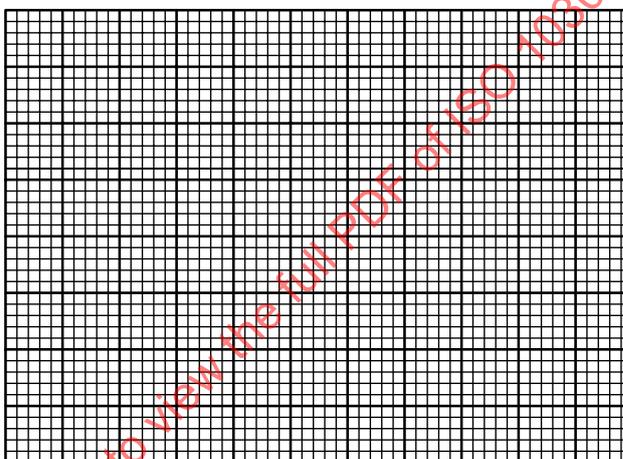
$L_{WA}$  reference  
value 1 pW  
dB



Rotational frequency  
 $\text{min}^{-1}$



Fan static pressure  
Pa



Volume flow rate under standard air condition ( $\text{m}^3/\text{s}$ )

Model: \_\_\_\_\_

Part/serial number: \_\_\_\_\_

Test voltage: \_\_\_\_\_

Power line frequency (if applicable): \_\_\_\_\_

Date: \_\_\_\_\_

Other information: \_\_\_\_\_

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